

**Application for Letter of Map Revision
(LOMR)
Bella Vista Ranch Phase 1
City of Reno, Nevada**

**Prepared for:
Centex Homes, Nevada**

**Prepared by:
QUAD KNOPF**

**January, 2008
Job No. N0432**



1/9/08



Quad Knopf

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1.0 INTRODUCTION

This narrative has been prepared to accompany an application for a Letter of Map Revision (LOMR) for Bella Vista Ranch Phase 1. Bella Vista Ranch is bounded on the east by Mira Loma Road, the west and south by the Damonte Ranch and Double Diamond Ranch developments, and the north by the Butler Ranch, a privately owned ranch. Bella Vista Ranch is located north of the new flood control detention facilities on Damonte Ranch, part of the regional flood control facilities. The development consists of a medium- to high-density single family residential area with lot sizes generally less than 1/8 acre. The property lies within the City of Reno's jurisdiction and within the Southeast Truckee Meadows Master Plan area Figure 1 shows a vicinity map for this area.

The Southeast Truckee Meadows Specific Plan area lies within the Steamboat Creek hydrologic basin. In addition to Steamboat Creek, flows from two branches of Whites Creek and flows from the Virginia Range affect this area. Regional detention facilities and major channel systems provide conveyance and control of 100-year storm waters. The area covered by this study is found on Panels 3178 and 3179 of FIRM Number 32031C3178 E, Washoe County, Nevada and Incorporated Areas. Both panels will be modified by this LOMR. The most recent floodplain adjustments were done under "An application for Letter of Map Revision (LOMR) for the Damonte Ranch/Double Diamond Ranch Regional Flood Control Improvements" (September 2004), FEMA Case No. 05-09-0105P. It was approved by FEMA in October 2005 (see panels 3186 and 3187 in Appendix E). Additionally, FEMA has recently issued a Conditional Letter of Map Revision (CLOMR) for Damonte Ranch Phase V and Bella Vista Ranch Phase 1 dated August 8, 2007 (Quad Knopf, 2007). Quad Knopf presently has a LOMR for Damonte Ranch V in review with FEMA under Case No. 07-09-1677R (Quad Knopf, 2007).

A number of hydrologic and hydraulic analysis reports are available for this area and the surrounding development. These reports are listed in the reference section.

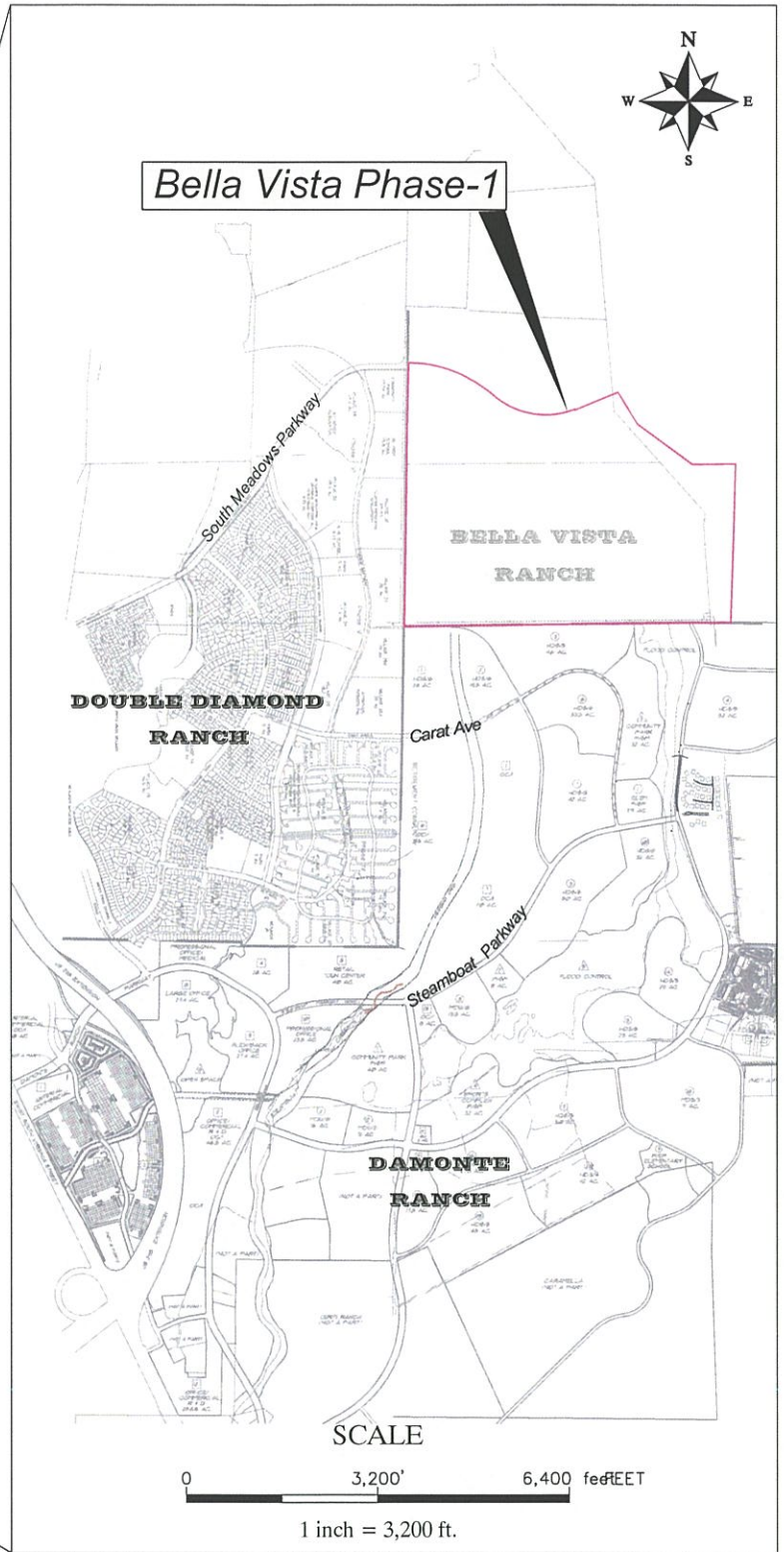
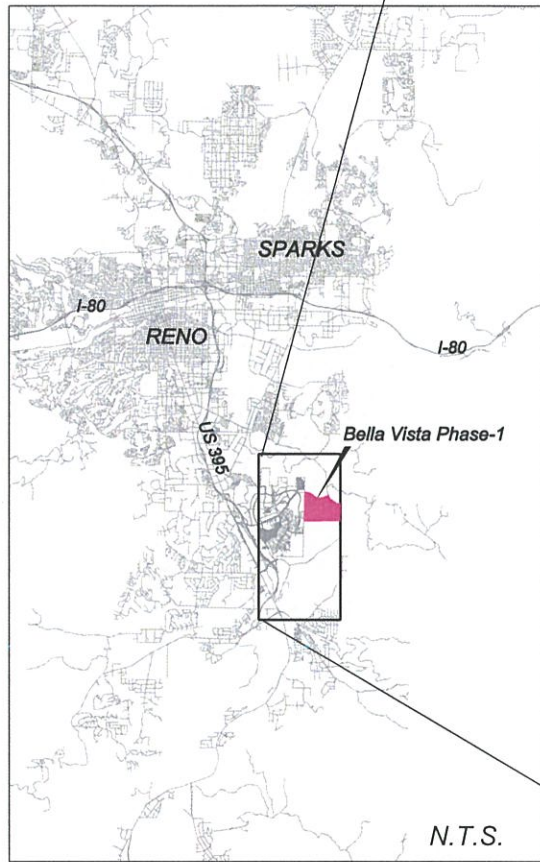
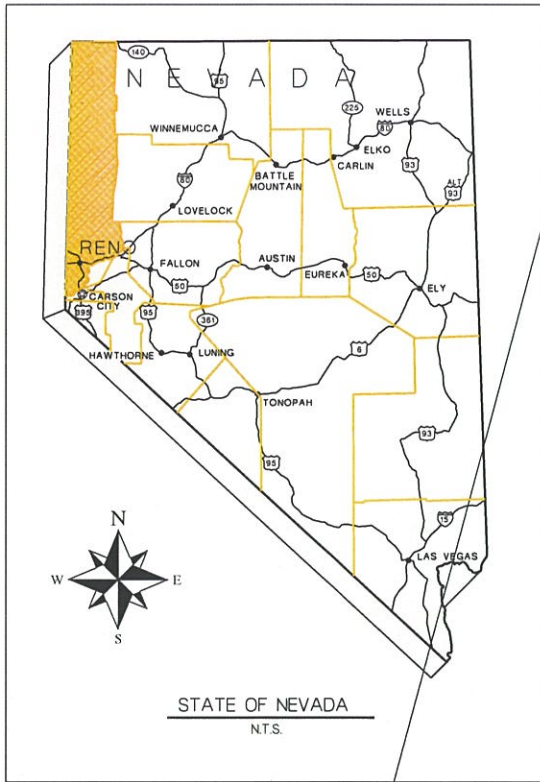


FIGURE 1
Vicinity Map
Bella Vista Phase-1 LOMR
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Date: January 2008



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2.0 EXISTING AND DEVELOPED CONDITIONS

2.1 Existing Conditions

As mentioned earlier, the most recent floodplain adjustments (Figure 2) were done under Damonte Ranch/Double Diamond Ranch Regional Flood Control Improvements (FEMA Case No. 05-09-0105P), although another revision is currently under review (FEMA Case No. 07-09-1677R, Quad Knopf, 2007.) Steamboat Creek high flows will be split at the Damonte Diversion Structure. Approximately 4154 cfs, or 52% of the 100-year flood flow, will continue northward in the existing Steamboat Creek channel, and 3838 cfs, or 48% of the flow, will be diverted eastward through regional detention basin, wetlands and ponds, then northward to the where it crosses Damonte Ranch property line and sheet flows into the realigned Steamboat Creek Channel. The proposed model from Damonte Phase V (DRph5.dat) from the LOMR case currently under review by FEMA will be used as the existing condition model for the Bella Vista Phase 1. Results of the model are contained in the Appendix C. Figure 3, Damonte V Hydrologic Workmap, illustrates the area covered in the LOMR presently under review. Flows from the Realigned Steamboat Creek Channel (RSCC) through Bella Vista Phase 1 will be returned to sheet flow condition prior to reaching the Butler Ranch, in order to maintain existing flow conditions on the Butler Ranch, shown as watershed subbasin D5 in Figure 4.

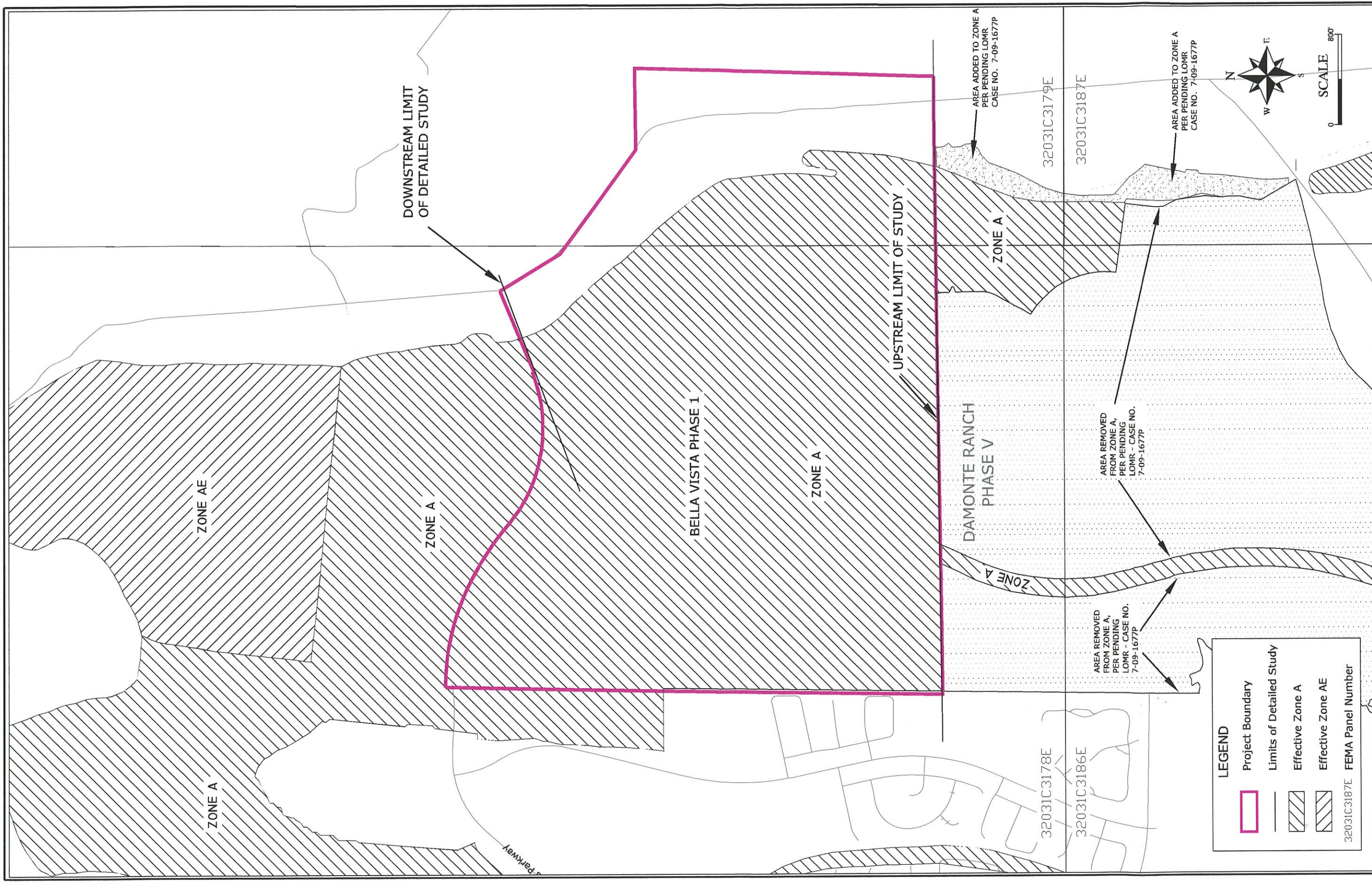
2.2 Developed Conditions

Bella Vista Ranch Phase 1 is located north of the new flood control channels and detention facilities on Damonte Ranch and south of the Butler Ranch, a privately owned ranch (Figure 1). The proposed condition model (DRph5+BV1.dat) is contained in Appendix C. Bella Vista Ranch Phase 1 is a medium-to high-density single family residential development with lot sizes generally less than 1/8 acre. RSCC has been improved to contain flood flows up to and including the design event, the 100-year, 24-hour storm, through the Bella Vista Ranch Phase 1 property. RSCC turns east just downstream from where it enters into Bella Vista Ranch from Damonte Ranch to its historic alignment along the toe of the Virginia Range.

New channels and storm drains have been constructed to convey the storm waters from the Bella Vista Ranch development to the RSCC. The West Boundary Channel discharges into an existing regional flood control channel south of South Meadows Parkway. The East-West Channel carries interior drainage from the southerly portion of Phase 1 and discharges into the RSCC upstream of South Meadows Parkway. An underground storm drain beginning at the intersection of Veterans Parkway and South Meadows Parkway carries flows from the northerly portion of Phase 1 and discharges into the RSCC where South Meadows Parkway currently terminates.

WHERE?

Fig 4



LEGEND

- Project Boundary
- Limits of Detailed Study
- Effective Zone A
- Effective Zone AE

FEMA Panel Number

N
W E S

SCALE
0 800'

Sheet 1 of 1 Quad Knopf Job # N0432 Date: Jan 2008	FIGURE 2 Existing Conditions FEMA Zone Map Bella Vista Phase-1 LOMR <small>Centex Homes</small>	Revisions: Scale: 1" = 800' CI: detailed contours = NA File Name: LOMR_Fig2-Plat1-Plat3.dwg Drawn By: GH Designed By: RH	9600 Prototype Ct. Reno, Nevada 89521 TEL: (775) 324-1212 FAX: (775) 324-2311 WEB: www.quadknopf.com N0432 Quad Knopf
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3.0 HYDROLOGIC ANALYSIS

The hydrologic analyses for the Bella Vista Ranch Phase 1 project have been performed using the Corps of Engineers HEC-1 computer program (U.S. Army Corps of Engineers, 1998) and current effective models accepted by FEMA. The modeling analyses included with this report are for the existing condition (Damonte Ranch Phase V development; file name DRph5.dat) and the developed condition (Damonte Ranch Phase V development and Bella Vista Ranch Phase 1 development; file name DRph5+BV1.dat). The outputs from these models are included in Appendix C and in electronic format on a CD also located in Appendix C. The hydrologic workmaps and regional watershed map, Figures 3, 4 and 5, respectively, display the basin configuration used in the models. Refer to Nimbus Engineers (2004) for the watershed parameters used in the models. It should be noted that 100-year flood flows mentioned here are based on updated HEC-1 models, which contain the *As-Built UPDATE* for Damonte Ranch/Double Diamond Ranch Regional Flood Control Improvements, described in Appendix B.

The City of Reno requires mitigation of the increase in volume resulting from the 100-year, 72-hour storm event for development in the vicinity of Damonte and Bella Vista Ranches. Per information in the CLOMR (Quad Knopf, 2007), the pre-development 100-year, 72-hour model generated 101 acre-feet on the project site. The post-development model generated 121 acre-feet, an increase of 20 acre-feet from development of the Bella Vista Phase 1 project. The models are contained in the CLOMR (Quad Knopf, 2007).

3.1 On-site Hydrologic Analysis

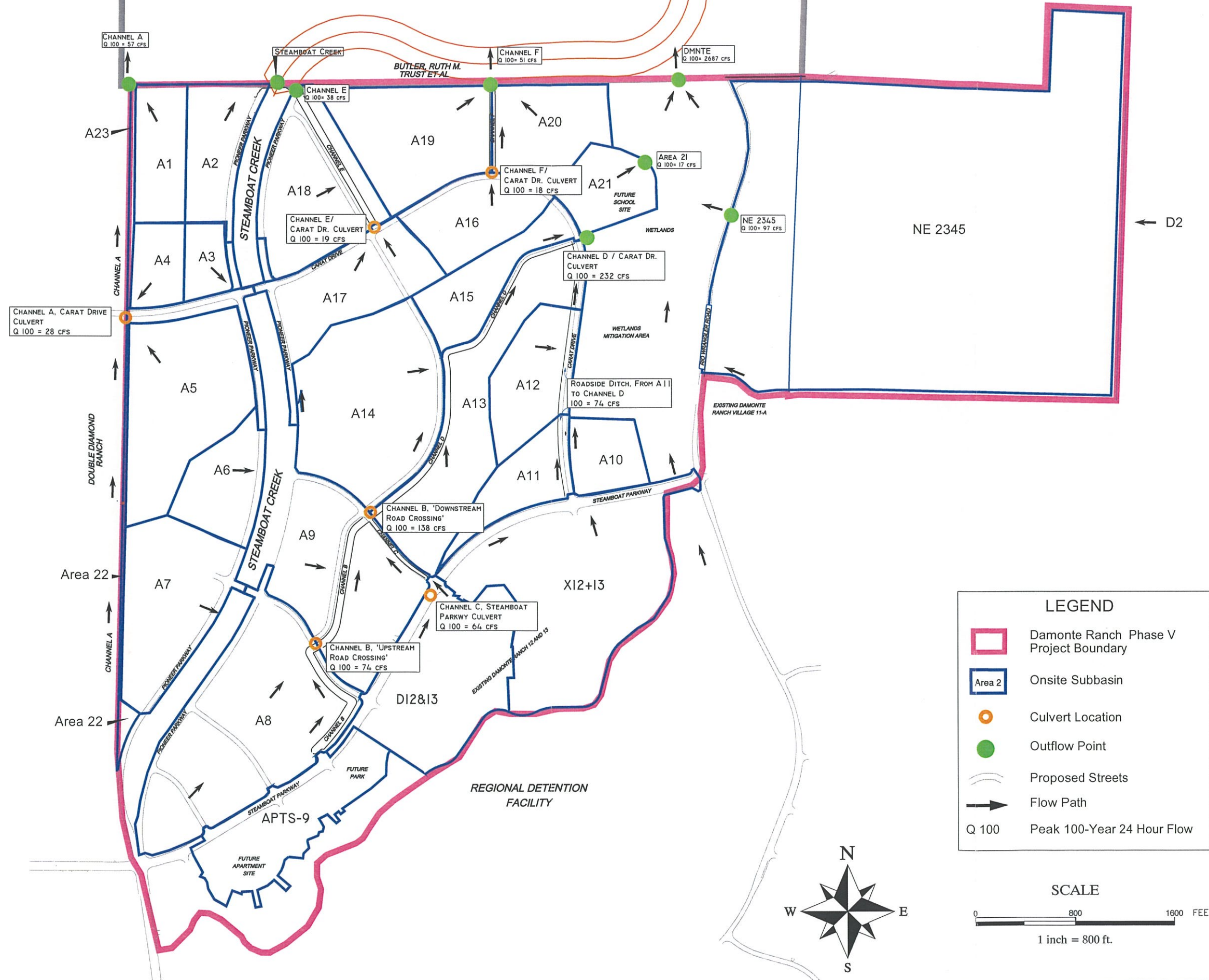
The SCS methodologies were originally used to develop the on-site parameters used in the HEC-1 hydrologic modeling for the Southeast Truckee Meadows. Due to revisions in the grading plan and lot layouts, the number of watersheds has increased from the original Southeast Truckee Meadows study. The watershed boundaries were also modified in this study to reflect as-built grading. The overall drainage patterns were not significantly altered. Figure 3 shows the existing condition watershed map for the region and Figure 4 shows the revised on-site watersheds used in the new post-development HEC-1 model.

Curve numbers originally developed for this area as a part of the Southeast Truckee Meadows Flood Control Master Plan were modified, as needed, based on development type (see the calculations for original curve numbers in Nimbus Engineers, 2004). On-site basins generally drain to the RSCC and the west side channel. The East-West channel will collect a portion of the flows from the future development on the western side of Steamboat Parkway (BVW-7) and from BV-5, BV-6, BV-7, BV-8, BV-9 and BV-10. Times of concentration were determined to be the minimum (10 minutes) based upon the formulas in the Washoe County, Hydrologic Criteria and Drainage Design Manual (Washoe County, 1996); therefore, calculations are not included. The new curve numbers for Bella Vista Ranch Phase 1 were determined based upon the criteria in Table 702 of the Washoe County, Hydrologic Criteria and Drainage Design Manual (Washoe County, 1996). Developed land-use conditions used to estimate curve numbers were 1/8 and 1/4 acre residential lots, neighborhood areas, and wetlands. The hydrologic parameters used in the revised HEC-1 model are included below in Table 1.

Table 1: On-Site Watershed Parameters

Sub-basin ID	Area (acres)	Area (sq mi)	CN Pre-Development	CN Post-Development
BV 1	19.67	0.031	74	90
BV 2	4.5	0.007	74	83
BV 3	7.88	0.012	74	90
BV 4	7.66	0.012	74	90
BV 5	3.38	0.005	74	83
BV 6	5.44	0.009	74	90
BV 7	10.25	0.016	74	90
BV 8	14.94	0.023	74	83
BV 9	11.36	0.018	74	83
BV 10	9.43	0.015	74	83
BV 11	7.66	0.012	74	84
BV 12	19.68	0.031	74	85
BV 13	3.47	0.005	74	87
BV 14	4.69	0.007	74	84
BV 15	11.3	0.018	74	83
BV 16	3.74	0.006	74	83
BVW 1	14.15	0.0271	74	81
BVW 3	18.6	0.0501	74	79
BVW 5	14.04	0.049	74	90
BVW 6	6.5	0.01	74	83
BVW 7	39.83	0.062	74	83
BVW 8	24.13	0.0431	74	83

BELLA VISTA RANCH



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File Name:	LOMR_Fig-3_DamV-on-site.dwg
Drawn By:	GH
Designed By:	DW

FIGURE 3
 Damonte Ranch V
 Onsite Hydrologic Workmap
 Damonte Ranch Phase V

Sheet 1 of 1
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Double Diamond
Detention Basin

D-5

(1,030 feet from Bella Vista
Property Boundary)

D-5

BVW-1

BVW-3

BV-1

WESTERN CHANNEL

BV-7

BELLA VISTA
PROPERTY

D-5

BUTLER RANCH
PROPERTY

STEAMBOAT CREEK CHANNEL

BV-2

BV-3

BV-4

BV-5

BV-6

EAST-WEST CHANNEL

BVW-7

BV-8

BV-9

BV-10

BV-12

BVW-5

BVW-6

BV-16

BV-15

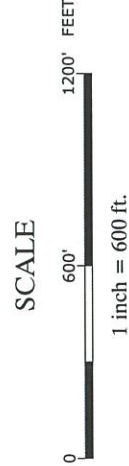
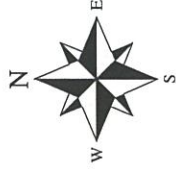
BV-14

BV-13

Storage
Basin #3

Storage Basin #1

DAMONTE RANCH PHASE 5



LEGEND

- Bella Vista Property Boundary
- BV-2 Onsite Watershed
- Storage Basins
- Proposed Lots
- Flow Direction

Sheet 1 of 1

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FIGURE 4 Onsite Hydrologic Workmap Bella Vista Phase-1 LOMR

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Scale: 1" = 600'
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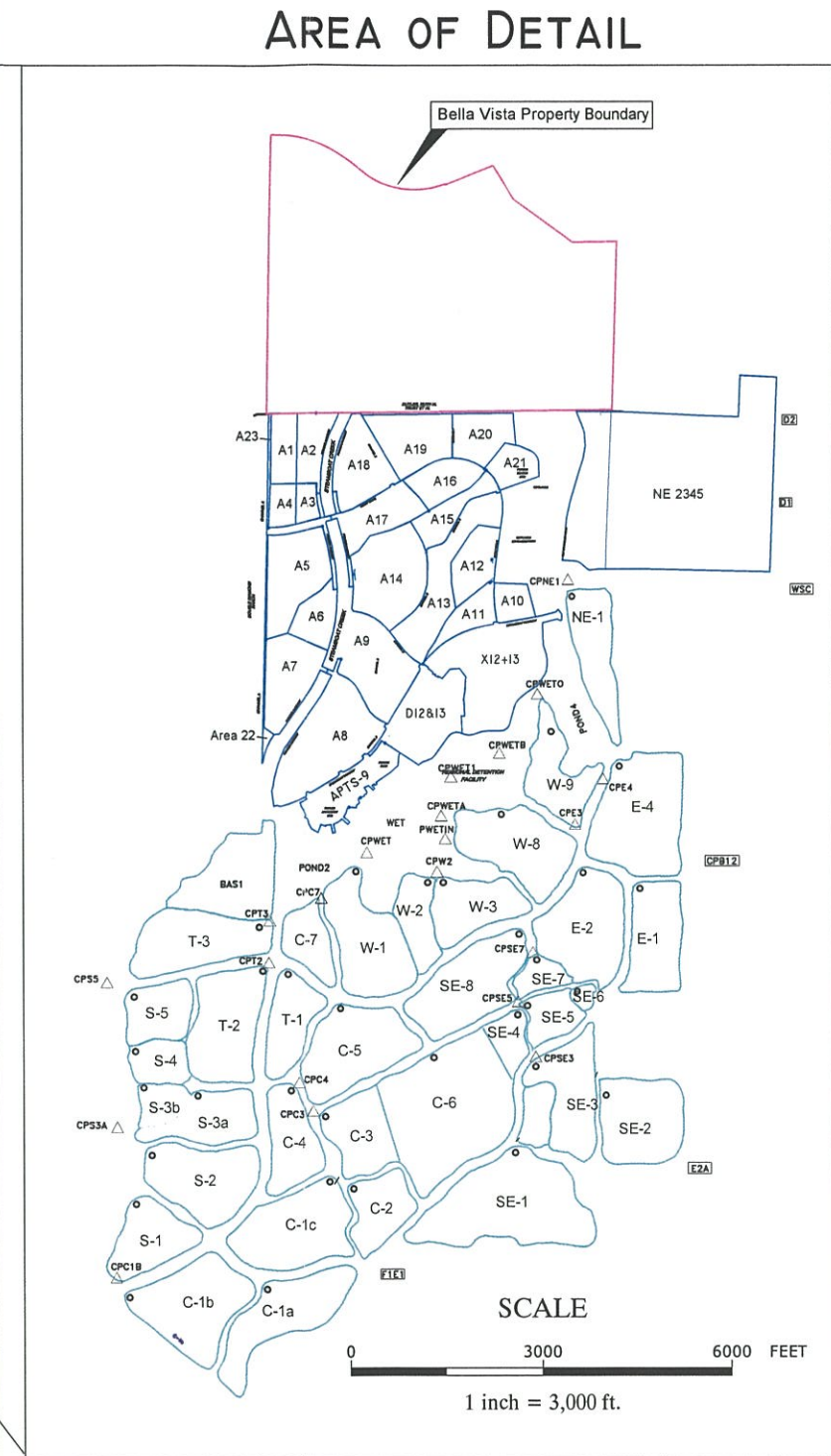
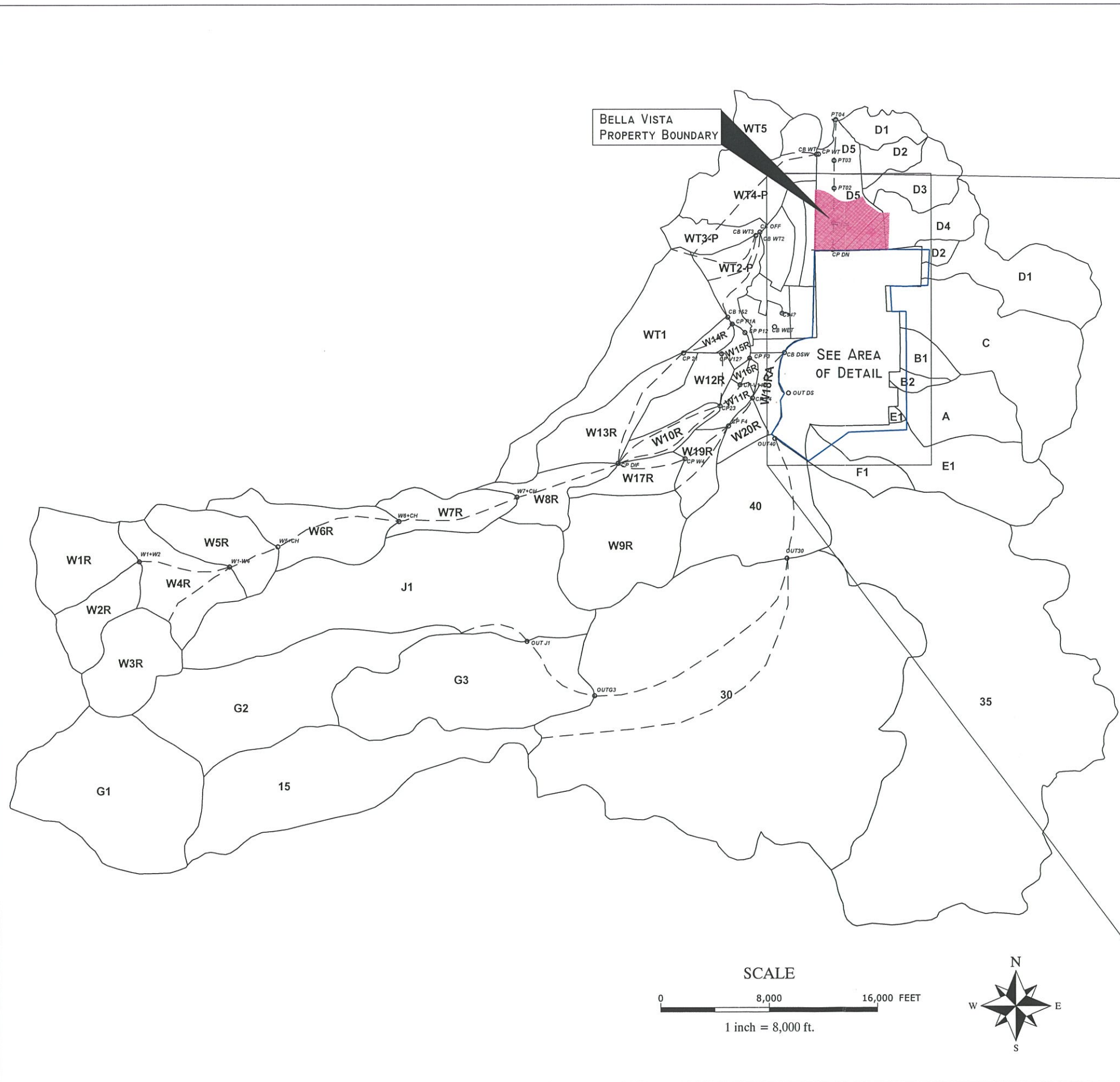
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References:

Scale: 1" = 8000' & 1" = 3000' (inset)	Contour Interval: NA	File: LOMR_Fig-5_Reg-Sheds.dwg
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FIGURE 5
Regional Watershed Map
Bella Vista Phase-1 LOMR
Centex Homes

Nevada
Reno

Sheet 1 of 1	Quad Knopf Job # N0432	January 2008
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3.2 Results

The 100-year, 24-hour peak discharges at key locations/control points are given in Table 2. As previously mentioned the outputs from these models are included in Appendix C, and in electronic format on a CD also located in Appendix C. The peak flows in the Main Steamboat channel are within acceptable limits and in compliance with the Southeast Truckee Meadows Specific Plan (see Section 4.0).

Table 2: 100-year, 24-hour Peak Discharges at Key Locations, Bella Vista Phase 1

Location	Model Node	Flow Rate (cfs)
Main Steamboat Channel, at Damonte Ranch Property Line = Upstream end of Bella Vista Phase 1	STM+E	4193
Main Steamboat Channel, after Channel F	STM+AF	4213
Main Steamboat Channel, after sheet flow from Damonte Wetlands	Stmbv3	6407
Main Steamboat Channel, after onsite sub basin 12	StBV33	6413
Main Steamboat Channel, after Confluence with East-West Channel	STMBV2	6452
Main Steamboat Channel, south of South Meadows Parkway	STM+ 2	6466
StmBV1, Northerly Phase 1 Boundary at Butler Ranch	StmBV1	6477
Western Perimeter Ditch at Outlet to Regional Channel	WSTOUT	117
Channel F	CHNL-F	51
DMNTE, Damonte Wetlands at entrance to Steamboat Realigned Channel	DMNTE	2762

As a check between the existing and proposed models, a comparison of the total flow in the RSCC downstream of Damonte Ranch Phase 5 was conducted. Separate check models, terminating at the northern Damonte Ranch border, were prepared. Drph5_chk drout.dat is the truncated existing condition model. The subbasins contributing to flows in Channel A, also known as the West Boundary Channel, were removed from this model since Channel A does not discharge into the RSCC until downstream from both the Damonte and Bella Vista Ranches. +BV1_chk drout.dat is the truncated proposed condition model. Subbasins for the West Boundary Channel were removed from this model as well. The peak flows from the two truncated models only differ by 2 cfs, 6382 cfs versus 6384 cfs. The flow rate under the natural, pre-development, condition in the Southeast Truckee Meadows is 8525 cfs (FEMA Case No. 01-09-589R; Nimbus Engineers, 2001) and the flow estimated in the approved Damonte/Double Diamond LOMR application (Nimbus Engineers, 2004) is 5972 cfs (6076cfs in the updated HEC-1 model, Appendix C). Hence, the planned development is in compliance with the Master Plan.

4.0 HYDRAULIC ANALYSIS

4.1 Existing Conditions

A series of detention/flow retarding basins were constructed for the Damonte Ranch flood control improvements. These improvements are designed to preserve and/or enhance existing wetlands, and to mitigate the effects of channelization and development on the Damonte Ranch site. The improvements and the resulting change in flow patterns were recognized in a LOMR under FEMA Case No. 05-09-0105P (Nimbus Engineers, 2004). In addition, there is currently a LOMR in review with FEMA for Damonte Ranch Phase V improvements under Case No. 07-09-1677R (Quad Knopf, 2007). The developed condition for the LOMR in review will be considered as the existing condition for this LOMR, as summarized below. The existing FIRM for this area is included as Plate 1.

Just downstream of the point where Branch 3 enters Steamboat Creek, the flow enters a diversion structure that directs approximately 52% of the 100-year peak flood flows (4154 cfs) northward in the Steamboat Creek low-flow channel. The remaining 48%, approximately 3838 cfs, of the flow is diverted eastward through the Regional Detention Basin, Wetlands Detention, and Pond 4, and then northward to the Damonte Ranch property line (Plate 2). Under existing conditions, the flows from both the Steamboat Creek channel and the flood control structures on Damonte Ranch are dispersed into sheet flow before entering the Bella Vista Ranch property line. Table 3 summarizes the HEC-2/HEC-RAS hydraulic models developed for the movement of the channelized flows from both the Steamboat Creek channel and the regional flood control structures to the Bella Vista Ranch (see Nimbus Engineers, 2004). It should be noted that all the elevations in the approved LOMR are referenced to the North American Geodetic Vertical Datum 1929 (NGVD29).

Table 3: Damonte Ranch Flood Control Facilities Models (Nimbus Engineers, 2004)

HEC-2 or HEC-RAS Input File Name	Hydraulic Model Description
30LOMR1.DAT*	Sheet flow across the Bella Vista Ranch
DDVIL30.DAT*	Flow spilling westward out of Steamboat Creek
Wetld.prj	Sheet flow across Wetlands
STEAST.prj	Detention basin flow to Bella Vista Ranch - Channelized flow to sheet flow
WEST.PRJ	Steamboat Creek channel flow to Bella Vista Ranch - Channelized flow to sheet flow

* HEC-2 models, all other are HEC-RAS

The flood control facilities constructed as part of the development of Damonte Ranch V and delineated in the FEMA Case No. 07-09-1677R (Quad Knopf, 2007), currently under review by FEMA, further contain and control flows entering Bella Vista Ranch. The flows enter Bella Vista Ranch from Damonte Ranch at four locations: Steamboat Channel, West Boundary Channel, Channel F, and the Damonte Wetlands. The flows from both the RSCC and the flood control structures on Bella Vista and Damonte Ranches are dispersed into sheet flow before entering the Butler Ranch property north of the Bella Vista Phase I property line.

4.2 Developed Conditions

Hydraulic calculations for the RSCC were performed with HEC-RAS version 3.1.3 using the peak flows generated with the HEC-1, developed condition model described in the Hydrologic Analysis section of this report. The Hydraulic Workmap (see Plate 2) shows the alignment of the RSCC and the location of the HEC-RAS sections along the Channel alignment and wetlands. Standard Table No. 1 and 2 of the HEC-RAS calculations and HEC-RAS cross sections of the channel are contained in Appendix D. The As-Built Drawing for the RSCC in Bella Vista Phase 1 is included as Plate 2.

4.2.1 Completed RSCC: Bella Vista Reach

As-Built RSCC is compatible with the goals of the Steamboat Creek restoration plan and has been developed in consultation with the U.S. Army Corps of Engineers and the wetland scientists for the project. The channel will convey flows from west to east to combine with the flows from the Damonte Wetlands, then turning northward following the historic alignment of Steamboat Creek. Existing slopes and the flowline of the channel are consistent with the proposed construction plans and the CLOMR. The HEC-RAS model for the RSCC in Bella Vista ranch was developed based on the attached as-built hydraulic workmap contours (Plate 2).

The channel between Veterans Parkway and South Meadows Parkway (River Station 84 through River Station 17) is a trapezoidal cross section with a 200-foot bottom and 3:1 side slopes. A meandering low flow channel was constructed throughout this reach. Manning's n-values of 0.035 were assumed for the flat bottom and the sides of the channel and 0.030 for the meandering low flow channel for this reach of creek.

From River Station 18 through River Station 48, the east bank of the RSCC intercepts the existing ground at 3:1 slope. Storage basin No. 3 has been constructed adjacent to the east bank from River Station 48 through River Station 51. From River Station 51 through River Station 54 the east bank intercepts existing ground at a 3:1 slope. Riprap has been placed around the inside and outside of curves to prevent bank erosion, as well as along the south bank of the channel between Storage Basin No. 1 and the beginning of the curve downstream of Basin No. 1. In addition, a riprap pad was placed on the channel bottom along the outside of the curve from station 53+50 to station 61+00. This pad and the riprap sloped and cutoff wall will protect the bank and channel bottom from erosion due to sheet flow spilling over the bank and into the channel from the Damonte Wetlands. Storage basin No. 1 has been constructed adjacent to the south bank from River Station 76 westerly to the culvert under Veterans Parkway, where the bank increases in height to meet culvert wing wall. The proposed development is in fill adjacent to west and north banks, eliminating the need for a levee along these sides. A 12-foot wide combination trail and access road is constructed at the top of the slope adjacent to the channel on the north and west side of the channel, adjacent to the development. The westerly bank increases in height as it approaches Veterans Parkway to meet the culvert wing walls.

Downstream of South Meadows Parkway the flow transitions to sheet flow as it enters the Butler Ranch Property (River Stations 5 through 17). Grading in this reach is within a drainage easement. The bottom of the channel transitions from 200 feet to the existing incised channel. Side slopes intersect the existing ground on both sides of the channel allowing the flow to spill out into the natural floodplain. The divergence angle from channel flow to sheet flow was controlled by the use of non-effective flow areas along the westerly side to provide a theoretical smooth transition in width. A Manning's n-value of 0.030 was used for the first flow channel and a value of 0.035 was used for disturbed areas outside of the

first flow channel. A Manning's value of 0.050 was retained for the undisturbed areas. The 0.050 value was taken from the existing LOMR (HEC-2 model: 30LOMR1.DAT).

The Phase 1 detailed study ends at the downstream side of South Meadows Parkway, the northerly boundary of the Bella Vista Ranch; however, as stated above, grading and construction activities have occurred downstream in a recorded drainage easement on the Butler Ranch property. In order to tie the revised floodplain boundary into the effective base flood boundary at the downstream limit of the study area, a known water surface elevation at HEC-RAS Station 0.225 was used as downstream control for Bella Vista reach (Figure 6). This water surface elevation was obtained from the existing condition hydraulic model (HEC-2 model: 30LOMR1.DAT). Since all elevations in the existing HEC-2 model are referenced to the National Geodetic Vertical Datum of 1929 (NGVD 29), the downstream control elevation for Bella Vista reach was adjusted to North American Vertical Datum of 1988 (NAVD 88) by adding 3.33ft, therefore, the water surface elevation for downstream control is 4428.78 ft (the water surface elevation at HEC-2 Station 0.225 in Appendix D, 4425.45 ft plus 3.33 ft). The water surface elevations computed for the Bella Vista Phase 1 LOMR between Station 0.225 and South Meadows are equal to, or below, the water surface elevations computed in the existing hydraulics model (HEC-2 model: 30LOMR1.DAT); therefore, the new boundary of 100-year flooding within the existing boundary for 100-year flooding (Figure 6). A comparison of the existing water surface elevations and those computed for the Bella Vista Phase 1 LOMR are contained in Table 4 below. A normal depth with a slope of 0.003 was used upstream control of the Bella Vista reach.

From where?

☆

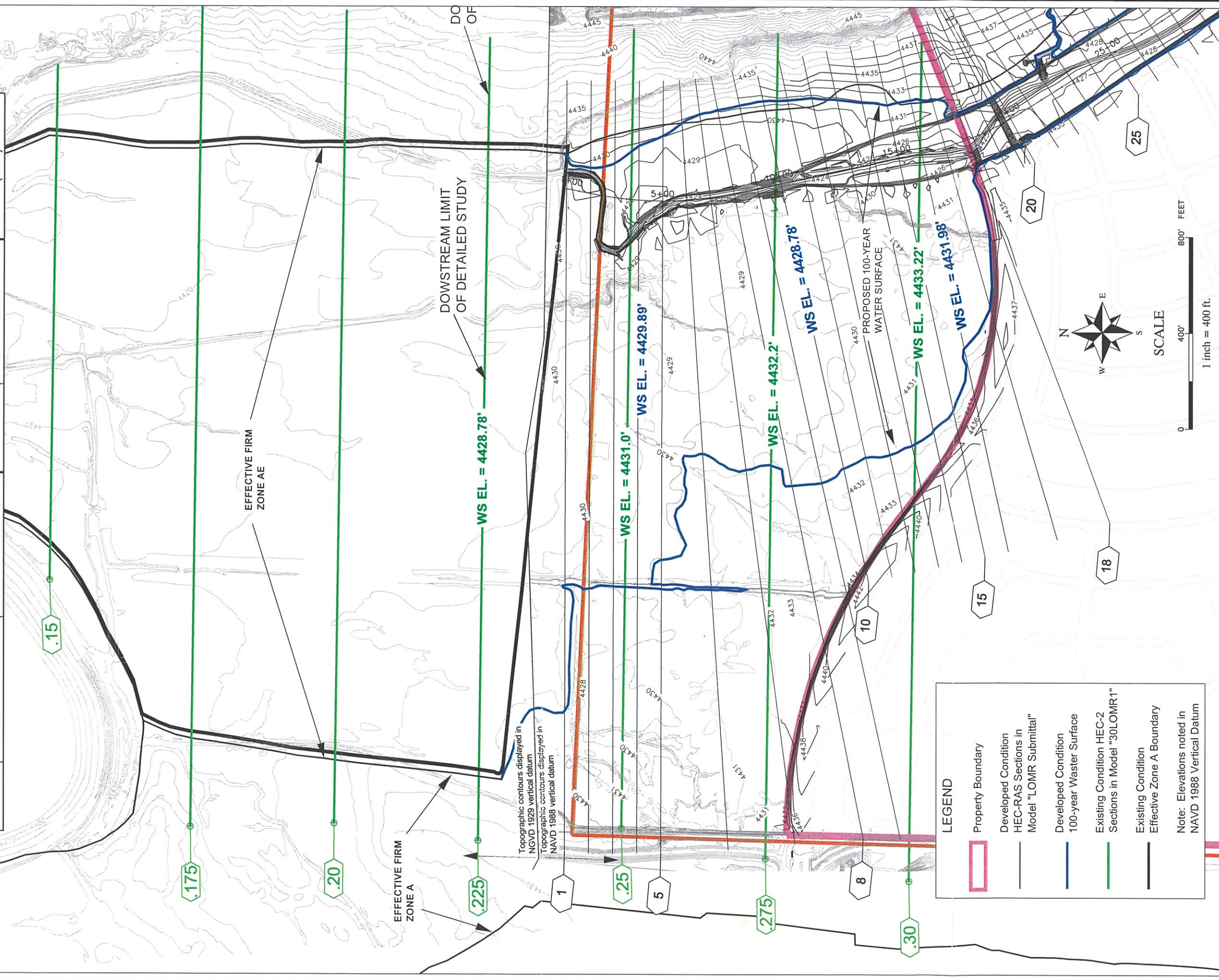
Table 4: Comparison of Proposed Versus Existing Conditions Water Surface Elevations North of Bella Vista Phase 1 Property Boundary

HEC-2 Model: 30LOMR1			HEC-RAS Model: BVPH1		Difference between BVPH1 to 30 LOMR1
HEC-2 Station	Water Surface Elevation (NGVD 29)	Elevation Adjusted to NAVD 88 (+3.33')	HEC-RAS Station	Water Surface Elevation (NAVD 88)	
0.225	4425.45	4428.78	0.225	4428.78	0.00
0.250	4427.67	4431.00	4	4429.89	(1.11)
0.275	4428.87	4432.20	10	4431.42	(0.78)
0.300	4429.89	4433.22	16	4431.98	(1.24)

Flow from the Damonte Wetlands enters the RSCC as sheet flow. Node DMNTE in the proposed HEC-1 model indicates a peak flow of 2762 cfs at the confluence. This flow was used as Profile 1 in the HEC-RAS model for the Damonte Wetlands. (HEC-RAS model Damonte Phase V – Wetlands with a file name of Wetland.prj). The flow from the Damonte Wetlands to the RSCC is 2194 cfs when the RSCC is at its peak. The flow by parts routine in HEC-RAS and the flow of 2194 (Profile 2) were used to calculate the distribution of the wetland flow into the RSCC at Section .20 in the Wetlands model. The calculations are contained in Appendix D, Damonte Wetlands and the results are shown in the Table 5 below and are illustrated in Figure 7.

Comparison of Proposed versus Existing Conditions Water Surface Elevations North of Bella Vista Phase-1 Property Boundary

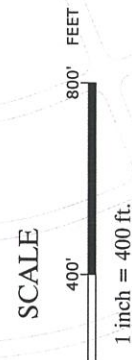
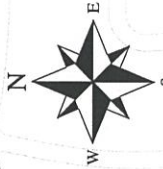
HEC-2 Model: 30LOMR1		HEC-RAS Model: BVPH1		Difference between	
HEC-2 Station	Water Surface Elevation (NGVD 29)	Elevation Adjusted to NAVD 88 (+3.33')	HEC-RAS Station	Water Surface Elevation (NAVD 88)	BVPH1 to 30 LOMR1
0.225	4425.45	4428.78	0.225	4428.78	0.00
0.250	4427.67	4431.00	4	4429.89	(1.11)
0.275	4428.87	4432.20	10	4431.42	(0.78)
0.300	4429.89	4433.22	16	4431.98	(1.24)



LEGEND

- Property Boundary
- Developed Condition HEC-RAS Sections in Model "LOMR Submittal"
- Developed Condition 100-year Waster Surface
- Existing Condition HEC-2 Sections in Model "30LOMR1"
- Existing Condition Effective Zone A Boundary

Note: Elevations noted in NAVD 1988 Vertical Datum



Sheet 1 of 1 Quad Knopf Job: N0432 Date: Jan. 2008	<p style="text-align: center;">FIGURE 6</p> <p style="text-align: center;">Existing Versus Proposed Water Surface Elevations North of Property Boundary</p> <p style="text-align: center;">Bella Vista Phase-1 LOMR</p> <p style="text-align: center;"><small>Centex Homes, Inc. Nevada</small></p>	Revisions: Scale: 1" = 400' CI: 1 foot File Name: LOMR_Fig6&7_Plat2_TWM.dwg Drawn By: GH Designed By: RH
9600 Prototype Ct. Reno, Nevada 89521 TEL: (775) 324-1212 FAX: (775) 324-2311 WEB: www.quadknopf.com		 Quad Knopf N0432

Table 5: Flow from Damonte Wetlands into RSCC

Steamboat Downstream	Flow Added		HEC-RAS FLOW	HEC-1 Node	Steamboat Stationing
5200	18		6408	STMBV3	5200
5300	129		6390		
5400	328		6261		
5500	540		5933		
5600	831		5393		
5700	286		4562		
5800	63		4276		
Total	2164		4213	STM+AF	7000

Culvert

A 10-barrel reinforced concrete box culvert with 12-foot wide barrels was constructed under Veterans Parkway. Eight of the barrels are 6-foot high and the remaining two barrels are 8-foot high to accommodate the low flow channel. The culvert barrels are parallel to the direction of flow and skewed to the roadway alignment. Upstream, the channel bottom transitions from the 150-foot width to the inside wall of the two outside barrels of the culvert. The 1:6 rockery walls intersect the culvert wing walls. Downstream the 200-foot bottom width channel transitions smoothly to the inside wall of the exterior culvert barrels. The 2:1 side riprap slopes parallel the edge of the bottom transition ending at the culvert headwall. A concrete apron is placed upstream and downstream of the culvert. Adjacent to the aprons upstream and downstream the channel is protected by riprap. The low flow channel continues through the riprap, apron, and the two center barrels of the culvert. Downstream of the culvert a riprap apron is serves as an energy dissipater on which a hydraulic jump occurs.

The upstream approach to the culvert is steep enough to cause the super critical flow through the culvert; therefore; the culvert was analyzed as a series of bridge piers. HEC-RAS does not compute super critical flow through culverts with different critical depths in the cells. The culvert does not seal therefore it can be analyzed as a series of bridge piers in lieu using the culvert option in HEC-RAS. The standard HEC-RAS bridge table is contained in Appendix D.

Storage Basins

Two storage basins have been constructed as part of the RSCC improvements (Plate 2 and Figure 4). These were constructed to contain the 20 acre-feet increase in volume of runoff due development, as discussed in the Hydrologic Section and in compliance with the CLOMR (Quad Knopf, 2007). These basins are designed to contain the volume removed from the RSCC near the peak flow for a 100-year design storm. The total capacity of the two basins is 25.71 acre-feet with a net retained volume of 21.82 acre-feet for 72-hours duration from the beginning of a storm event. Further discussion of the storage basin parameters is contained in the section *Storage Basin Outlet Structures*. Calculations for the volumes and the stage discharge curves are included in Appendix B.

Lateral Weirs

The concrete lateral weirs for Storage Basin 1 and Storage Basin 3 are shown on Plate 2. These weirs were designed to pass more than the desired volume to be stored and control the amount stored by placing an overflow spillway on the edge of the basin that will discharge back into the main channel. This eliminates the problem of clipping an exact volume of flow from an earthen channel. Both lateral weirs are constructed of a combination of riprap and concrete.

Varying rates of flow were used for the channel and lateral weir to calculate a rating curve for channel flow versus weir flow. The lateral weir table from HEC-RAS is contained in Appendix B. Using the rating curve and the peak hydrograph, a length of weir and weir elevation was set to pass the approximate volume required from the channel to the basins. Graphs of the computed flow to the basin versus total flow in the RSCC are contained in Appendix B.

Storage Basin Outlet Structures

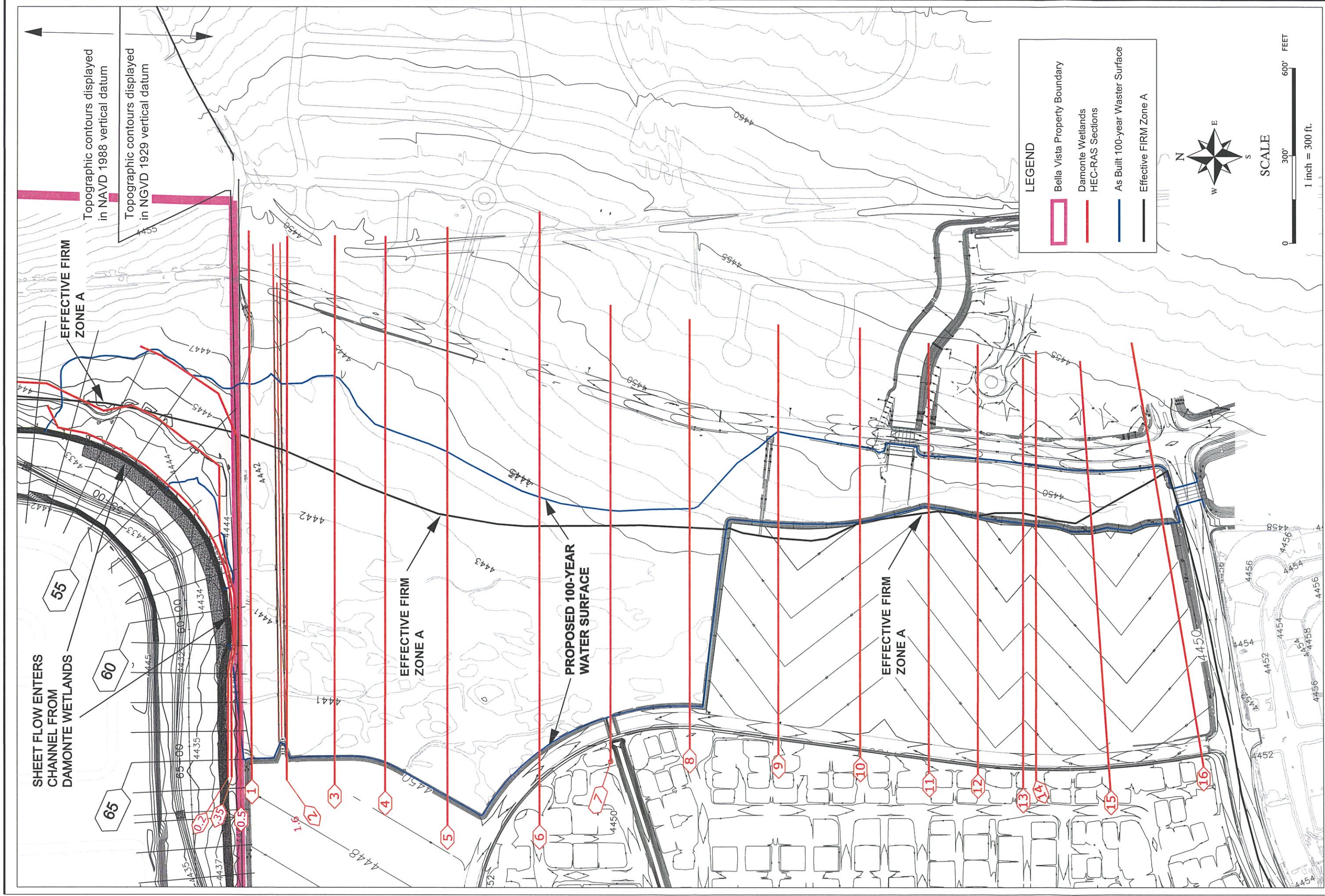
The outlet structures for each storage basin consist of a 12-inch RCP with a "Duck-bill" style flap gate on the downstream end with a 3-inch orifice through a 2-foot concrete plug on the upstream end. The upstream end is enclosed in a 2-foot high vertical slotted 24-inch diameter CMP with a grate on top.

Separate calculations were done for each basin to estimate the volume of flow remaining in the basin after 72 hours. The calculations were done on a time step method utilizing the Steamboat Hydrograph. The calculations were performed using an excel spreadsheet to calculate the amount of flow leaving the basin with a 3-inch orifice as the outlet. The depth of flow in the RSCC will cause the pipe to remain in the outlet control condition during the 72-hour time frame. The depth of flow in the channel during this 72-hour time period was determined by assuming normal depth in the RSCC for the various flows calculation interval. Calculations for the discharge from the outlet structures and the net volume at the 72 hour time period are contained in Appendix B.

4.2.3 Results of Hydraulic Modeling

The annotated FIRM (Plates 3 and 4) illustrates the resulting floodplain areas of the hydraulic analyses. The RSCC will safely contain and convey the 100-year, 24-hour storm flow, and as a result, a large section of the Bella Vista Phase 1 development should be removed from the existing Special Flood Hazard Area (Zone A), as indicated on the annotated FIRM (Plate 3).

The results of the hydraulic analyses also indicate that the 100-year 24-hour storm flow is confined in the RSCC in Bella Vista Ranch Phase 1.



Sheet 1 of 1	Scale: 1" = 300'	Revisions:
Quad Knopf Job: N0432	Cl: 1 foot	
Date: Jan. 2008	File Name: LOMR_Fig6&7_Plat2_TWM.dwg	
1:\0432 as built LOMR BY PH 1\ACAD\LOMR Figs\LOMR_Fig6&7_Plat2_TWM.dwg, Fig-7 Dam wetlands	Drawn By: GH	
	Designed By: RH	

FIGURE 7
Damonte Wetlands
HEC-RAS Cross Sections
Bella Vista Phase-1 LOMR
Centex Homes, Inc. Nevada

9800 Prototype Ct.
Reno, Nevada 89521
TEL: (775) 324-1212
FAX: (775) 324-2311
WEB: www.quadknopf.com
N0432

Quad Knopf

5.0 CONCLUSIONS

The following conclusions are based upon the detailed hydrologic and hydraulic analyses contained in this LOMR request for the Bella Vista Ranch Phase 1:

- 1) Detailed hydrologic and hydraulic analysis of the proposed conditions floodplain within the project study area shows that a large section of the Bella Vista Ranch Phase 1 may be removed from the existing FIRM (Zone A) flood plain.
- 2) The RSCC through the Bella Vista Phase 1 development will safely contain and convey the 100-year, 24-hour storm flow. The revised floodplain is shown in the annotated FIRM (Plates 3 and 4).

6.0 REFERENCES

- Nimbus Engineers, Application for Letter of Map Revision (LOMR): Damonte Ranch / Double Diamond Ranch Regional Flood Control Improvements, September 2004.
- Nimbus Engineers, Application for Conditional Letter of Map Revision (CLOMR): Damonte Ranch / Double Diamond Ranch Regional Flood Control Improvements, March 2001, Addendum September 2001.
- Nimbus Engineers, Application for Letter of Map Revision, Branch 3 of Whites Creek, Hydraulic Analysis of Branch 3, March 2001.
- Quad Knopf, Application for Letter of Map Revision (LOMR) for Damonte Ranch Phase V, City of Reno, Nevada, May 2007, (under review, FEMA Case No. 07-09-1677R).
- Quad Knopf, Application for Conditional Letter of Map Revision (CLOMR) for Damonte Ranch Phase V and Bella Vista Ranch PHASE 1, City of Reno, Nevada, March 2007.
- Quad Knopf, Bella Vista Phase 1 Hydrologic and Hydraulic Report, July 2005.
- Quad Knopf, Flood Control Master Plan Bella Vista Ranch, May 2005.
- Quad Knopf, Southeast Truckee Meadows Flood Control Master Plan Addendum Damonte Ranch Phase V, May 2005.
- U.S. Army Corps of Engineers, Hydrologic Engineering Center, HEC-1: Flood Hydrograph Package, Version 4.1, June 1998.
- U.S. Army Corps of Engineers, Hydrologic Engineering Center, HEC-RAS River Analysis System, Version 3.1.3, May 2005.
- U.S. Department of Agriculture, Soil Conservation Service, Soil Survey of Washoe County, Nevada, South Part, August 1983.
- U.S. Department of the Interior, Geological Survey, 7.5-Minute Series Topographic Map, Verdi Quadrangle, Scale 1:24000, Contour Interval 20 Feet, 1994.
- Washoe County, Hydrologic Criteria and Drainage Design Manual, Final Draft Report, December 2, 1996.

32031C3178E

32031C3178E

32031C3179E

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

WASHOE COUNTY,
NEVADA AND
INCORPORATED AREAS

MAP NUMBER
3203C3179 E

EFFECTIVE DATE:
SEPTEMBER 30, 1994

Panel 3179 of 2399

WASHOE COUNTY, NEVADA
FIRM PANEL 3179 OF 2399

DATE: 09/30/94

SCALE: 1" = 500'

DESIGNED BY: GH

DRAWN BY: RH

CHECKED BY: [Signature]

APPROVED BY: [Signature]

Federal Emergency Management Agency

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

WASHOE COUNTY,
NEVADA AND
INCORPORATED AREAS

MAP NUMBER
3203C3178 E

EFFECTIVE DATE:
SEPTEMBER 30, 1994

Panel 3178 of 2399

WASHOE COUNTY, NEVADA
FIRM PANEL 3178 OF 2399

DATE: 09/30/94

SCALE: 1" = 500'

DESIGNED BY: GH

DRAWN BY: RH

CHECKED BY: [Signature]

APPROVED BY: [Signature]

Federal Emergency Management Agency



LEGEND

- Project Boundary
- Streets and Roads
- Zone A
- Zone AE
- Area Removed From Zone A per Pending LOMR: 7-09-1677P
- Area Added to Zone A per Pending LOMR: 7-09-1677P
- FEMA Panel Number

PLATE 1

Quad Knopf Job #
N0432

January 2008

EXISTING FIRM
PANELS 3178E & 3179E
BELLA VISTA PHASE-1 LOMR

Reno
Washoe County
Nevada

Scale: 1" = 500'

Contour Interval: NA

File: LOMR_FIRM-AllPanels_Ext.dwg

Drawn By: GH

Designed By: RH

Revisions:	Date:	References:
1		
2		
3		
4		
5		
6		

9600 Parklane Ct.
Reno, Nevada 89521
TEL: (775) 324-1212
FAX: (775) 324-2315
WEB: www.quadknopf.com
060082

0 500 1000 FEET

SCALE
1 inch = 500 ft.

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

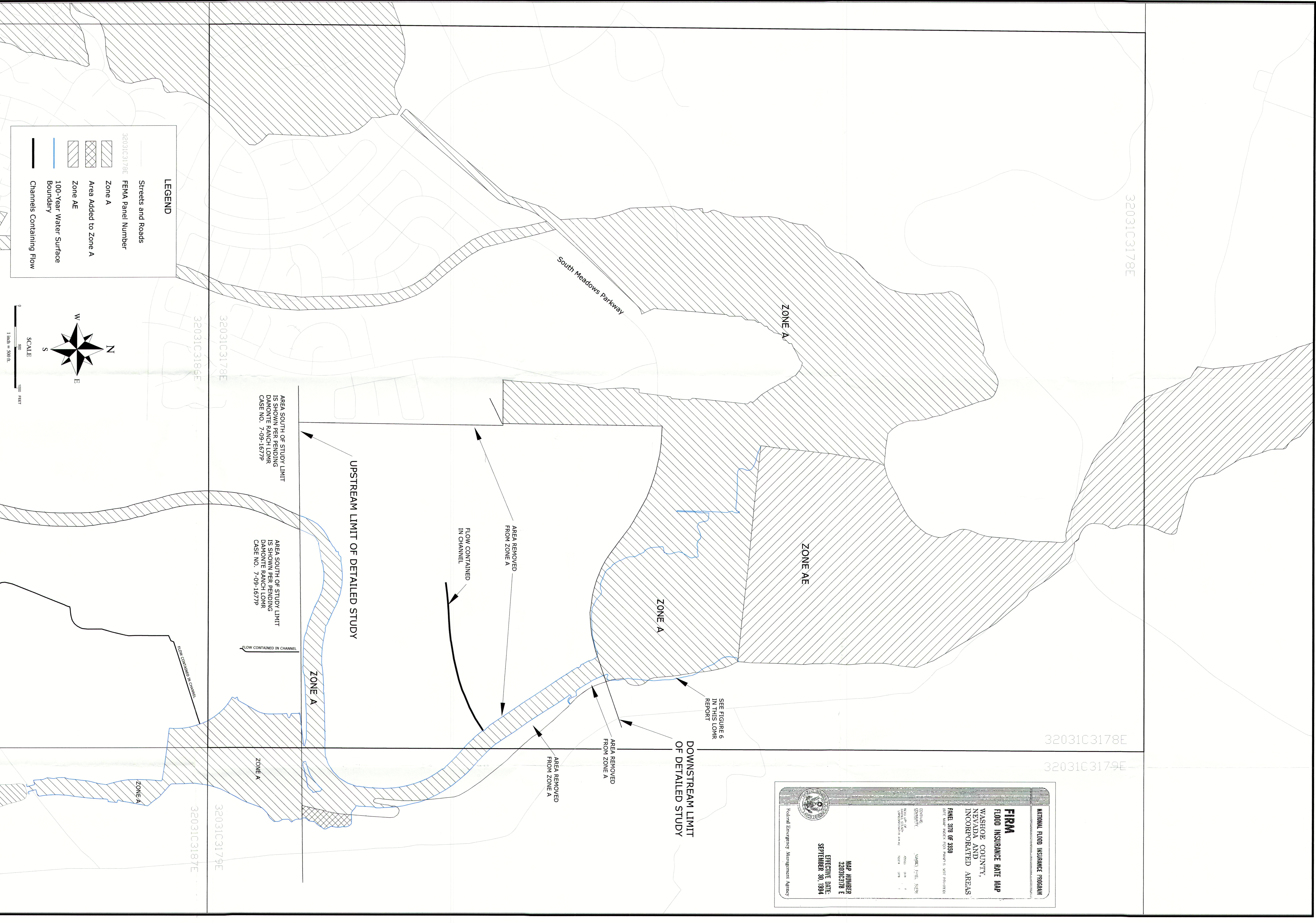
WASHOE COUNTY,
NEVADA AND
INCORPORATED AREAS

PANEL 3178 OF 3390

DATE MAP MADE FOR PANEL'S DATE PRINTED:
SEPTEMBER 30, 1994

MAP NUMBER
3203C3178 E
EFFECTIVE DATE
SEPTEMBER 30, 1994

Federal Emergency Management Agency



LEGEND

Streets and Roads
32031C3178E FEMA Panel Number

Zone A

Area Added to Zone A

Zone AE

100-Year Water Surface Boundary

Channels Containing Flow

Scale: 1" = 500'

Contour Interval: NA

Scale: 1 inch = 500 feet

0 500 1000 FEET

North Arrow

AREA SOUTH OF STUDY LIMIT IS SHOWN PER PENDING DAMONTE RANCHO LOMR CASE NO. 7-09-1677P

AREA SOUTH OF STUDY LIMIT IS SHOWN PER PENDING DAMONTE RANCHO LOMR CASE NO. 7-09-1677P

SEE FIGURE 6 IN THIS LOMR REPORT

PLATE 3

Quad Knopf Job #
N0432

ANNOTATED FIRM
PANEL NO. 32031C 3178E
BELLA VISTA PHASE-1 LOMR

Scale: 1" = 500'

Contour Interval: NA

File: LOMR_Fig2_Plat3_Pan3_Firms.dwg

Drawn By: GH

Designed By: RH

Revisions:

Date: References

Quad Knopf

9600 Protodrive Ct.
Reno, Nevada 89521
TEL: (775) 324-2311
FAX: (775) 324-2311
WEB: www.quadknopf.com

N0432

32031C3179E

32031C3178E 32031C3179E

32031C3179E

32031C3187E

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP
WASHOE COUNTY,
NEVADA AND
INCORPORATED AREAS

PANEL 3178 OF 3180
SEE PANEL 3179 FOR DETAILS NOT PRINTED

COUNTY:
WASHOE COUNTY,
NEVADA

NATIONAL FLOOD INSURANCE PROGRAM
FEDERAL EMERGENCY MANAGEMENT AGENCY

MAP NUMBER
32031C3178 E
EFFECTIVE DATE:
SEPTEMBER 30, 1994

UPSTREAM LIMIT OF DETAILED STUDY

AREA REMOVED FROM ZONE A

AREA ADDED TO ZONE A

AREA REMOVED FROM ZONE A

AREA ADDED TO ZONE A

AREA SOUTH OF STUDY LIMIT IS SHOWN PER PENDING DAKONTE RANCH LOMR CASE NO. 7-09-1677P

SHARPE CREEK CHANNEL FLOWERS DAMONTE WETLANDS

ZONE A

ZONE A

LEGEND

Streets and Roads

FEMA Panel Number

Zone A

Area Added to Zone A

Zone AE

100-Year Water Surface Boundary

Channels Containing Flow

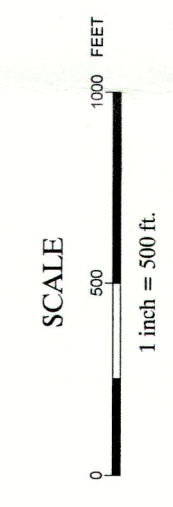
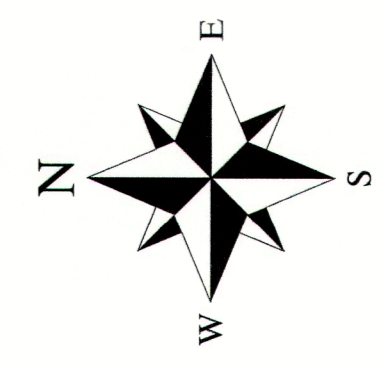


PLATE 4

Quad Knopf Job #
N0432

January 2008

ANNOTATED FIRM

PANEL NO. 32031C 3179E

BELLA VISTA PHASE-1 LOMR

Washoe County

Nevada

Revisions:	Date:	References:
1		
2		
3		
4		
5		
6		

9600 Paradise Ct.
Reno, Nevada 89521
TEL: (775) 334-1212
WEB: www.quadknopf.com

N0432

APPENDIX A

**FEMA FORMS
ANNEXATION MAP
DRAINAGE EASEMENT**

PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this form is estimated to average 1 hour per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless a valid OMB control number appears in the upper right corner of this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, U.S. Department of Homeland Security, Federal Emergency Management Agency, 500 C Street, SW, Washington DC 20472, Paperwork Reduction Project (1660-0016). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. **Please do not send your completed survey to the above address.**

A. REQUESTED RESPONSE FROM DHS-FEMA

This request is for a (check one):

- CLOMR: A letter from DHS-FEMA commenting on whether a proposed project, if built as proposed, would justify a map revision, or proposed hydrology changes (See 44 CFR Ch. 1, Parts 60, 65 & 72).
- LOMR: A letter from DHS-FEMA officially revising the current NFIP map to show the changes to floodplains, regulatory floodway or flood elevations. (See Parts 60 & 65 of the NFIP Regulations.)

B. OVERVIEW

1. The NFIP map panel(s) affected for all impacted communities is (are):

Community No.	Community Name	State	Map No.	Panel No.	Effective Date
Ex: 480301	City of Katy	TX	480301	0005D	02/08/83
480287	Harris County	TX	48201C	0220G	09/28/90
320020	City of Reno, Washoe County	NV	32031C	3178E	09/30/94
320020	Washoe County	NV	32031C	3179E	09/30/94

- 2. Flooding Source: **Steamboat Creek**
- 3. Project Name/Identifier: **Damonte Phase V and Bella Vista Ranch Phase 1**
- 4. FEMA zone designations affected: **A** (choices: A, AH, AO, A1-A30, A99, AE, AR, V, V1-V30, VE, B, C, D, X)
- 5. Basis for Request and Type of Revision:

a. The basis for this revision request is (check all that apply)

- Physical Change
- Improved Methodology/Data
- Regulatory Floodway Revision
- Other (Attach Description)

Note: A photograph and narrative description of the area of concern is not required, but is very helpful during review.

b. The area of revision encompasses the following types of flooding and structures (check all that apply)

- Types of Flooding:
- Riverine
 - Coastal
 - Shallow Flooding (e.g., Zones AO and AH)
 - Alluvial fan
 - Lakes
 - Other (Attach Description)
- Structures:
- Channelization
 - Levee/Floodwall
 - Bridge/Culvert
 - Dam
 - Fill
 - Other, Attach Description

C. REVIEW FEE

Has the review fee for the appropriate request category been included? Yes Fee amount: \$4800
 No, Attach Explanation

Please see the DHS-FEMA Web site at http://www.fema.gov/fhm/frm_fees.shtm for Fee Amounts and Exemptions.

D. SIGNATURE

All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

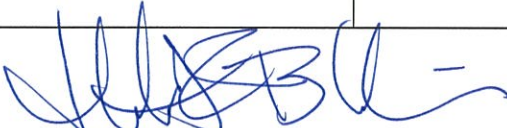
Name: Ralph Hogoboom		Company: Quad Knopf, Inc.	
Mailing Address: 9600 Prototype Court Reno, NV 89521	Daytime Telephone No.:	Fax No.:	
	775-324-1212	775-324-2311	
E-Mail Address: RalphH@quadknopf.com			
Signature of Requester (required): 		Date: 01/10/08	

As the community official responsible for floodplain management, I hereby acknowledge that we have received and reviewed this Letter of Map Revision (LOMR) or conditional LOMR request. Based upon the community's review, we find the completed or proposed project meets or is designed to meet all of the community floodplain management requirements, including the requirement that no fill be placed in the regulatory floodway, and that all necessary Federal, State, and local permits have been, or in the case of a conditional LOMR, will be obtained. In addition, we have determined that the land and any existing or proposed structures to be removed from the SFHA are or will be reasonably safe from flooding as defined in 44CFR 65.2(c), and that we have available upon request by FEMA, all analyses and documentation used to make this determination.

Community Official's Name and Title: Neil Mann, Public Works Director		Telephone No
Community Name: City of Reno	Community Official's Signature (required):	Date:

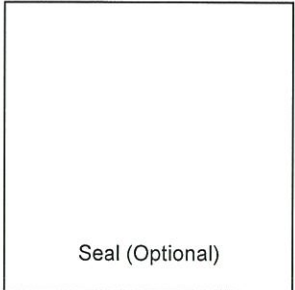
CERTIFICATION BY REGISTERED PROFESSIONAL ENGINEER AND/OR LAND SURVEYOR

This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

Certifier's Name: Jeffrey F. Brooke	License No.: 8658	Expiration Date: 12/31/08
Company Name: PLACES Consulting Services Inc.	Telephone No.: 775-355-7721	Fax No.: 775-355-7795
Signature: 		Date: 01/10/08

Ensure the forms that are appropriate to your revision request are included in your submittal.

<u>Form Name and (Number)</u>	<u>Required if ...</u>
<input checked="" type="checkbox"/> Riverine Hydrology and Hydraulics Form (Form 2)	New or revised discharges or water-surface elevations
<input checked="" type="checkbox"/> Riverine Structures Form (Form 3)	Channel is modified, addition/revision of bridge/culverts, addition/revision of levee/floodwall, addition/revision of dam
<input type="checkbox"/> Coastal Analysis Form (Form 4)	New or revised coastal elevations
<input type="checkbox"/> Coastal Structures Form (Form 5)	Addition/revision of coastal structure
<input type="checkbox"/> Alluvial Fan Flooding Form (Form 6)	Flood control measures on alluvial fans



FEDERAL EMERGENCY MANAGEMENT AGENCY
RIVERINE HYDROLOGY & HYDRAULICS FORM

O.M.B No. 3067-0148
 Expires September 30, 2005

PAPERWORK REDUCTION ACT

Public reporting burden for this form is estimated to average 3 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless a valid OMB control number appears in the upper right corner of this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, SW, Washington DC 20472, Paperwork Reduction Project (3067-0148). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. Please do not send your completed survey to the above address.

Flooding Source: Steamboat Creek
 Note: Fill out one form for each flooding source studied

A. HYDROLOGY

1. Reason for New Hydrologic Analysis (check all that apply)

- Not revised (skip to section 2)
 No existing analysis
 Improved data
 Alternative methodology
 Proposed Conditions (CLOMR)
 Changed physical condition of watershed

2. Comparison of Representative 1%-Annual-Chance Discharges

Location	Drainage Area (Sq. Mi.)	FIS (cfs)	Revised (cfs)
Huffaker Narrows (PTO4)	108.12	7126	7106

3. Methodology for New Hydrologic Analysis (check all that apply)

- Statistical Analysis of Gage Records
 Precipitation/Runoff Model HEC-1 [TR-20, HEC-1, HEC-HMS etc.]
 Regional Regression Equations
 Other (please attach description)

Please enclose all relevant models in digital format, maps, computations (including computation of parameters) and documentation to support the new analysis. The document, "Numerical Models Accepted by FEMA for NFIP Usage" lists the models accepted by FEMA. This document can be found at: http://www.fema.gov/fhm/en_modl.shtml.

4. Review/Approval of Analysis

If your community requires a regional, state, or federal agency to review the hydrologic analysis, please attach evidence of approval/review.

5. Impacts of Sediment Transport on Hydrology

Was sediment transport considered? Yes No If yes, then fill out Section F (Sediment Transport) of Form 3. If No, then attach your explanation for why sediment transport was not considered.

B. HYDRAULICS

1. Reach to be Revised

	Description	Cross Section	Water-Surface Elevations (ft.)	
			Effective	Proposed/Revised
Downstream Limit	Steamboat Channel Bella Vista Phase 1	.225	4428.78	4428.78
Upstream Limit	Steamboat Channel Bella Vista Phase 1	90.9	4451.12	4451.33

2. Hydraulic Method Used

Hydraulic Analysis HEC-RAS [HEC-2 , HEC-RAS, Other (Attach description)]

B. HYDRAULICS (CONTINUED)

3. Pre-Submittal Review of Hydraulic Models

FEMA has developed two review programs, CHECK-2 and CHECK-RAS, to aid in the review of HEC-2 and HEC-RAS hydraulic models, respectively. These review programs verify that the hydraulic estimates and assumptions in the model data are in accordance with NFIP requirements, and that the data are comparable with the assumptions and limitations of HEC-2/HEC-RAS. CHECK-2 and CHECK-RAS identify areas of potential error or concern. These tools do not replace engineering judgment. CHECK-2 and CHECK-RAS can be downloaded from http://www.fema.gov/fhm/frm_soft.shtm. We recommend that you review your HEC-2 and HEC-RAS models with CHECK-2 and CHECK-RAS. If you disagree with a message, please attach an explanation of why the message is not valid in this case. Review of your submittal and resolution of valid modeling discrepancies will result in reduced review time.

HEC-2/HEC-RAS models reviewed with CHECK-2/CHECK-RAS? Yes No

4. Models Submitted

Duplicate Effective Model*	Natural File Name:	Floodway File Name:
Corrected Effective Model*	Natural File Name:	Floodway File Name:
Existing or Pre-Project Conditions Model	Natural File Name:	Floodway File Name:
Revised or Post-Project Conditions Model	Natural File Name:	Floodway File Name:
Other - (attach description)	Natural File Name:	Floodway File Name:

*Not required for revisions to approximate 1%-annual-chance floodplains (Zone A) – for details, refer to the corresponding section of the instructions.

The document "Numerical Models Accepted by FEMA for NFIP Usage" lists the models accepted by FEMA. This document can be found at: http://www.fema.gov/fhm/en_modl.shtm.

C. MAPPING REQUIREMENTS

A certified topographic map must be submitted showing the following information (where applicable): the boundaries of the effective, existing, and proposed conditions 1%-annual-chance floodplain (for approximate Zone A revisions) or the boundaries of the 1%- and 0.2%-annual-chance floodplains and regulatory floodway (for detailed Zone AE, AO, and AH revisions); location and alignment of all cross sections with stationing control indicated; stream, road, and other alignments (e.g., dams, levees, etc.); current community easements and boundaries; boundaries of the requester's property; certification of a registered professional engineer registered in the subject State; location and description of reference marks; and the referenced vertical datum (NGVD, NAVD, etc.).

Note that the boundaries of the existing or proposed conditions floodplains and regulatory floodway to be shown on the revised FIRM and/or FBFM must tie-in with the effective floodplain and regulatory floodway boundaries. Please attach a copy of the effective FIRM and/or FBFM, annotated to show the boundaries of the revised 1%- and 0.2%-annual-chance floodplains and regulatory floodway that tie-in with the boundaries of the effective 1%- and 0.2%-annual-chance floodplain and regulatory floodway at the upstream and downstream limits of the area of revision.

D. COMMON REGULATORY REQUIREMENTS

1. For CLOMR requests, do Base Flood Elevations (BFEs) increase? Yes No

For CLOMR requests, if either of the following is true, please submit evidence of compliance with Section 65.12 of the NFIP regulations:

- The proposed project encroaches upon a regulatory floodway and would result in increases above 0.00 foot.
- The proposed project encroaches upon a SFHA with BFEs established and would result in increases above 1.00 foot.

2. Does the request involve the placement or proposed placement of fill? Yes No

If Yes, the community must be able to certify that the area to be removed from the special flood hazard area, to include any structures or proposed structures, meets all of the standards of the local floodplain ordinances, and is reasonably safe from flooding in accordance with the NFIP regulations set forth at 44 CFR 60.3(a)(3), 65.5(a)(4), and 65.6(a)(14). Please see the MT-2 Instructions for more information.

3. For LOMR requests, is the regulatory floodway being revised? Yes No

If Yes, attach evidence of regulatory floodway revision notification. As per Paragraph 65.7(b)(1) of the NFIP Regulations, notification is required for requests involving revisions to the regulatory floodway. (Not required for revisions to approximate 1%-annual-chance floodplains [studied Zone A designation] unless a regulatory floodway is being added. Elements and examples of regulatory floodway revision notification can be found in the MT-2 Form 2 Instructions.)

4. For LOMR requests, does this request require property owner notification and acceptance of BFE increases? Yes No

If Yes, please attach proof of property owner notification and acceptance (if available). Elements of and examples of property owner notification can be found in the MT-2 Form 2 Instructions.

PAPERWORK REDUCTION ACT

Public reporting burden for this form is estimated to average 7 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless a valid OMB control number appears in the upper right corner of this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, U.S. Department of Homeland Security, Federal Emergency Management Agency, 500 C Street, SW, Washington DC 20472, Paperwork Reduction Project (1660-0016). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. Please do not send your completed survey to the above address.

Flooding Source: Steamboat Creek
Note: Fill out one form for each flooding source studied

A. GENERAL

Complete the appropriate section(s) for each Structure listed below:

- Channelization.....complete Section B
- Bridge/Culvertcomplete Section C
- Damcomplete Section D
- Levee/Floodwallcomplete Section E
- Sediment Transport.....complete Section F (if required)

Description Of Structure

1. Name of Structure

Type (check one): Channelization Bridge/Culvert Levee/Floodwall Dam

Location of Structure: At Veterans Parkway - Bella Vista Phase 1

Downstream Limit/Cross Section: 85.94

Upstream Limit/Cross Section: 86.73

2. Name of Structure:

Type (check one): Channelization Bridge/Culvert Levee/Floodwall Dam

Location of Structure:

Downstream Limit/Cross Section:

Upstream Limit/Cross Section:

3. Name of Structure:

Type (check one) Channelization Bridge/Culvert Levee/Floodwall Dam

Location of Structure: :

Downstream Limit/Cross Section:

Upstream Limit/Cross Section:

NOTE: For more structures, attach additional pages as needed.

B. CHANNELIZATION

Flooding Source: **Steamboat Creek**

Name of Structure: **Steamboat Channel**

1. Accessory Structures

The channelization includes (check one):

- | | |
|--|--|
| <input type="checkbox"/> Levees [Attach Section E (Levee/Floodwall)] | <input checked="" type="checkbox"/> Drop structures |
| <input type="checkbox"/> Superelevated sections | <input type="checkbox"/> Transitions in cross sectional geometry |
| <input type="checkbox"/> Debris basin/detention basin | <input type="checkbox"/> Energy dissipator |
| <input type="checkbox"/> Other (Describe): | |

2. Drawing Checklist

Attach the plans of the channelization certified by a registered professional engineer, as described in the instructions.

3. Hydraulic Considerations

The channel was designed to carry **4193-6477cfs (the 100-year flood)**.

The design elevation in the channel is based on (check one):

- Subcritical flow Critical flow Supercritical flow Energy grade line

If there is the potential for a hydraulic jump at the following locations, check all that apply and attach an explanation of how the hydraulic jump is controlled without affecting the stability of the channel.

- Inlet to channel Outlet of channel At Drop Structures At Transitions
 Other locations (specify): **Below or in Culvert**

4. Sediment Transport Considerations

Was sediment transport considered? Yes No If Yes, then fill out Section F (Sediment Transport).
If No, then attach your explanation for why sediment transport was not considered.

C. BRIDGE/CULVERT

Flooding Source: **Steamboat Creek**

Name of Structure: **Culvert in Steamboat Creek at Veterans Parkway**

1. This revision reflects (check one):

- New bridge/culvert not modeled in the FIS
 Modified bridge/culvert previously modeled in the FIS
 New analysis of bridge/culvert previously modeled in the FIS

2. Hydraulic model used to analyze the structure (e.g., HEC-2 with special bridge routine, WSPRO, HY8): **HEC-RAS**

If different than hydraulic analysis for the flooding source, justify why the hydraulic analysis used for the flooding source could not analyze the structures. Attach justification.

3. Attach plans of the structures certified by a registered professional engineer. The plan detail and information should include the following (check the information that has been provided):

- | | |
|--|---|
| <input checked="" type="checkbox"/> Dimensions (height, width, span, radius, length) | <input checked="" type="checkbox"/> Erosion Protection |
| <input checked="" type="checkbox"/> Shape (culverts only) | <input checked="" type="checkbox"/> Low Chord Elevations – Upstream and Downstream |
| <input checked="" type="checkbox"/> Material | <input checked="" type="checkbox"/> Top of Road Elevations – Upstream and Downstream |
| <input type="checkbox"/> Beveling or Rounding | <input checked="" type="checkbox"/> Structure Invert Elevations – Upstream and Downstream |
| <input checked="" type="checkbox"/> Wing Wall Angle | <input checked="" type="checkbox"/> Stream Invert Elevations – Upstream and Downstream |
| <input checked="" type="checkbox"/> Skew Angle | <input checked="" type="checkbox"/> Cross-Section Locations |
| <input checked="" type="checkbox"/> Distances Between Cross Sections | |

4. Sediment Transport Considerations

Was sediment transport considered? Yes No If yes, then fill out Section F (Sediment Transport).
If No, then attach your explanation for why sediment transport was not considered.

OWNER'S CERTIFICATE
 I, the undersigned, being the owner of the land shown on this map, hereby certify that the information furnished herein is true and correct, and that I have no other interest in the land shown on this map, and that I have no other interest in the land shown on this map, and that I have no other interest in the land shown on this map.

RUTH H. BUTLER TRUST
 PAULETTE BUTLER, TRUSTEE
 8-14-02
 DATE

COUNCIL APPROVAL
 I, EDWARD A. FULLER, A PROFESSIONAL LAND SURVEYOR LICENSED IN THE STATE OF NEVADA, HAVE JUST MADE THIS MAP AND THIS CERTIFICATE IN ACCORDANCE WITH THE PROVISIONS OF NRS 202.010 AND 202.015.



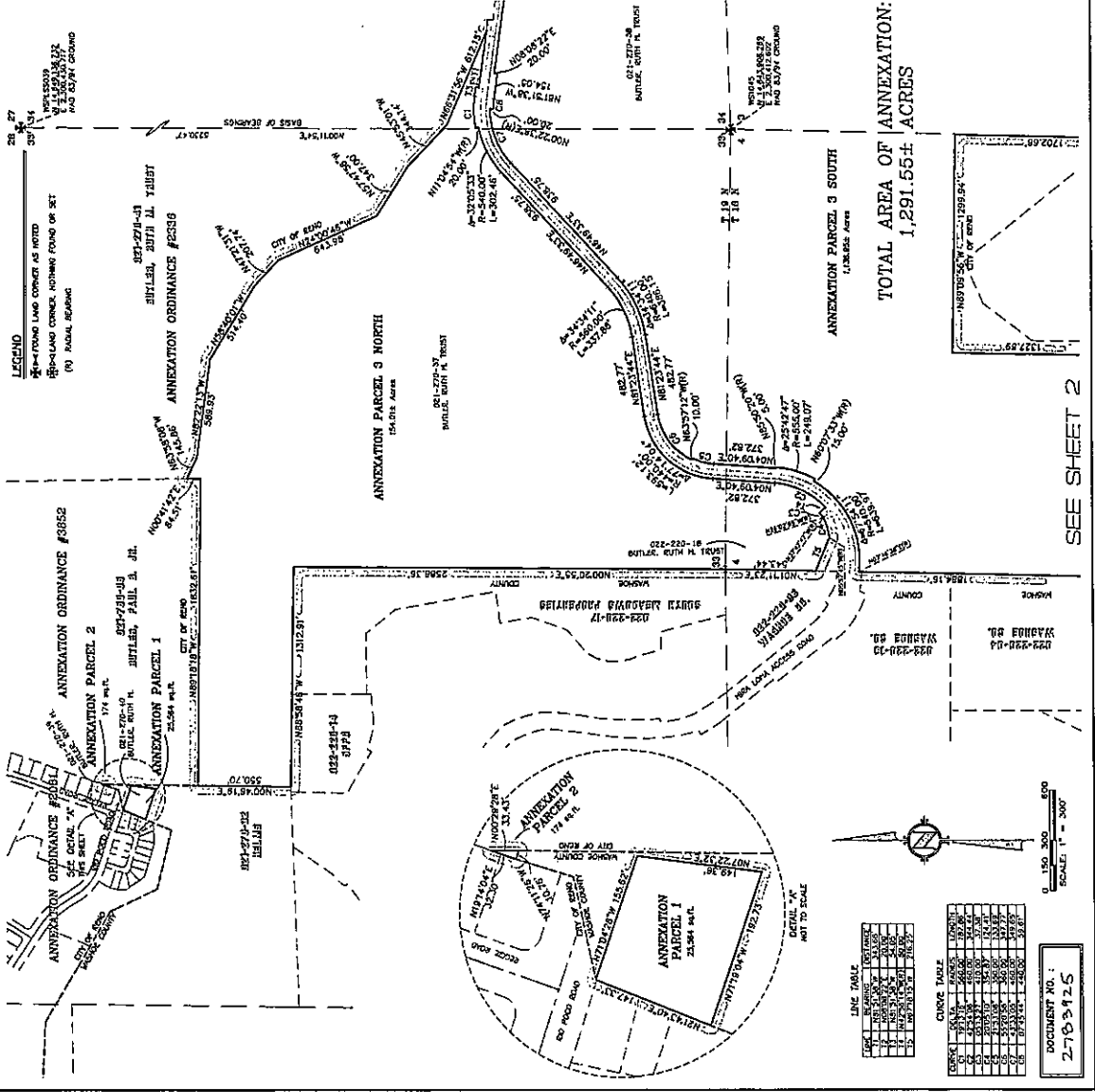
SURVEYOR'S CERTIFICATE
 I, EDWARD A. FULLER, A PROFESSIONAL LAND SURVEYOR LICENSED IN THE STATE OF NEVADA, HAVE JUST MADE THIS MAP AND THIS CERTIFICATE IN ACCORDANCE WITH THE PROVISIONS OF NRS 202.010 AND 202.015.



NOTES
 1. THIS MAP DOES NOT REPRESENT A FIELD SURVEY. DATA SHOWN WAS COMPILED FROM RECORDS AND FIELD NOTES.
 2. REFERENCE IS MADE TO THE RUTH H. BUTLER TRUST.

RECORDER'S STATEMENT
 FILE NO. 2-10-3425
 FEE \$100.00
 PAID FOR RECORD AT THE OFFICE OF THE COUNTY CLERK OF WASHINGTON COUNTY, NEVADA, ON THIS 14th DAY OF DECEMBER, 2002, AT 11:00 AM. BY: [Signature] COUNTY RECORDER

MAP TO SUPPORT ANNEXATION OF CERTAIN LANDS TO THE CITY OF RENO
 WASHINGTON COUNTY RECORDERS OFFICE
 RENO, NEVADA
 AUGUST 2002
 SHEET 1 OF 3
 21135-00



CUMULATIVE INDEXES SHOULD BE EXAMINED FOR ANY SUBSEQUENT CHANGES TO THIS MAP

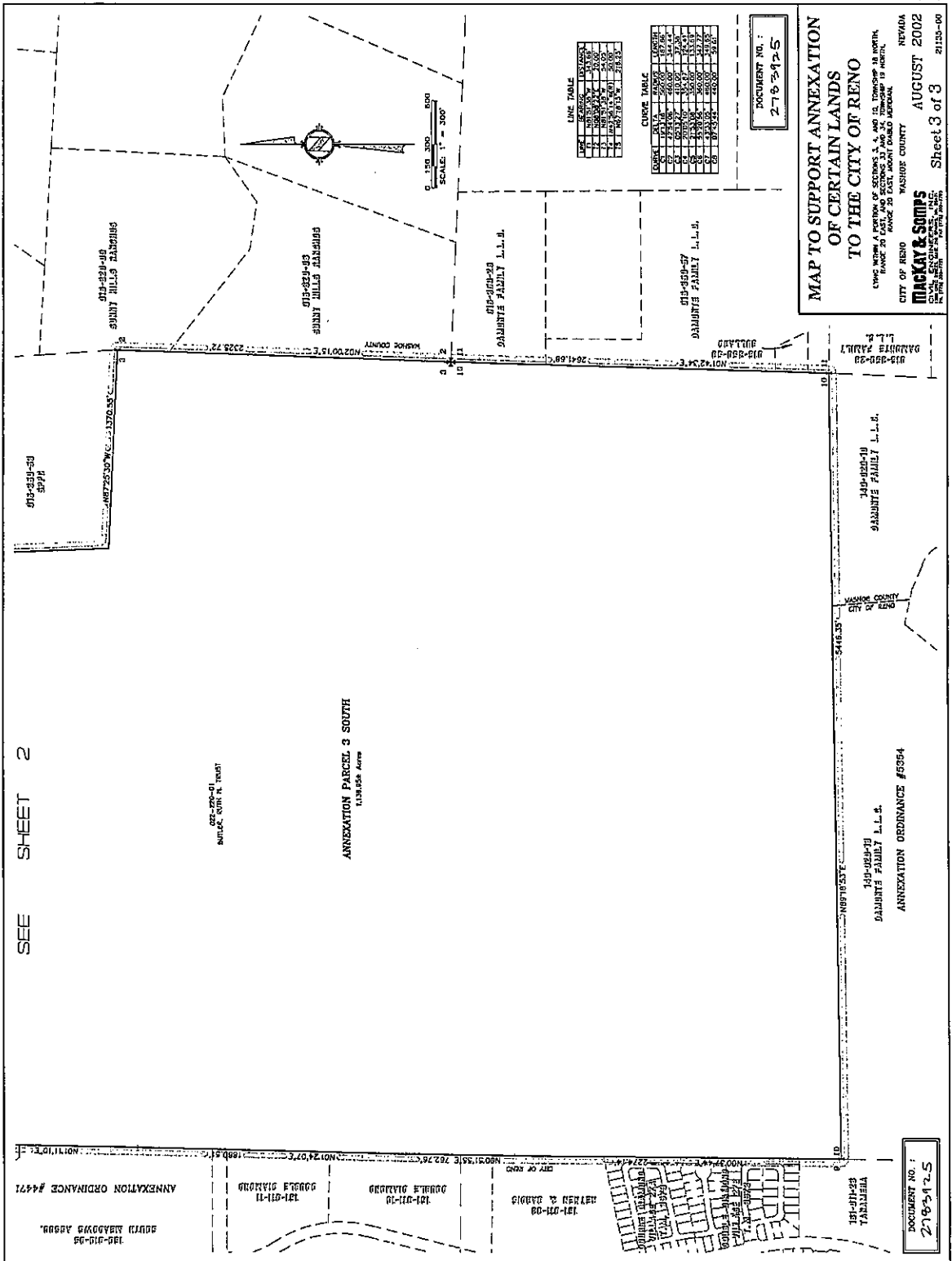
SEE SHEET 2

LS14

ANNEXATION TRACT MAP 4157

4157B

SEE SHEET 2



CUMULATIVE INDEXES SHOULD BE EXAMINED FOR ANY SUBSEQUENT CHANGES TO THIS MAP

4157B

MAP TO SUPPORT ANNEXATION OF CERTAIN LANDS TO THE CITY OF RENO

LVMS MAPS, A PORTION OF SECTION 3, T. 16 N., R. 12 E., TOWNSHIP 16 NORTH, RANGE 12 EAST, MOUNT ROSS AREA, WASHINGTON COUNTY, NEVADA

CITY OF RENO, WASHINGTON COUNTY, NEVADA

AUGUST 2002

Sheet 3 of 3 21133-00

MICKAY & SOMPS

REGISTERED PROFESSIONAL LAND SURVEYORS

1000 S. WASHINGTON AVENUE, SUITE 100, RENO, NEVADA 89502

PHONE: (775) 784-1111 FAX: (775) 784-1112

DOCUMENT NO.: 2783425

LINE TABLE

LINE NO.	START POINT	END POINT	LENGTH	BEARING
1	11	12	222.72	S 89° 00' 00" W
2	12	13	222.72	S 89° 00' 00" W
3	13	14	222.72	S 89° 00' 00" W
4	14	15	222.72	S 89° 00' 00" W
5	15	16	222.72	S 89° 00' 00" W
6	16	17	222.72	S 89° 00' 00" W
7	17	18	222.72	S 89° 00' 00" W
8	18	19	222.72	S 89° 00' 00" W
9	19	20	222.72	S 89° 00' 00" W
10	20	21	222.72	S 89° 00' 00" W

CURVE TABLE

POINT	CHORD	ARC	ANGLE
1	222.72	222.72	90.00
2	222.72	222.72	90.00
3	222.72	222.72	90.00
4	222.72	222.72	90.00
5	222.72	222.72	90.00
6	222.72	222.72	90.00
7	222.72	222.72	90.00
8	222.72	222.72	90.00
9	222.72	222.72	90.00
10	222.72	222.72	90.00

DOCUMENT NO.: 2783425

ANNEXATION TRACT MAP 4157B

RECORDING REQUESTED BY:

First Centennial Title Company of Nevada
1450 Ridgeview Drive, Suite 100
Reno, NV 89509-6335
13/304 NT



AND WHEN RECORDED MAIL TO:

Centex Homes
Attn: Forward Planning
10509 Professional Circle, Suite 200
Reno, NV 89521
300658.8

DRAINAGE EASEMENT AGREEMENT

THIS DRAINAGE EASEMENT AGREEMENT ("Agreement") is made and entered into this June 2, 2006, by and between Paul B. Butler, Jr. and/or Bank of America, N.A., as Co-Trustees or Trustee, as the case may be, of (a) The Ruth M. Butler Trust created under Declaration of Trust dated September 15, 1972, (b) The Allison Sowles Butler Trust dated October 1, 1973, (c) The Daryl Ellen Butler Trust dated October 1, 1973, (d) The Paul Brett Butler, III Trust dated October 1, 1973, (e) The Shelley Bryant Butler Trust dated October 1, 1973, and (f) The Paul B. Butler Trust dated August 10, 1971 (collectively, "Grantor"). and Centex Homes, a Nevada general partnership ("Grantee").

Recitals

A. On the date hereof, Grantee has acquired from Grantor that certain real property located in the City of Reno (the "City"), County of Washoe (the "County"), State of Nevada, more particularly described on Exhibit A attached hereto (the "Grantee Property").

B. In connection with Grantee's acquisition of the Grantee Property, Grantor desires to grant to Grantee certain easement rights over other real property owned by Grantor.

NOW, THEREFORE, for good and valuable consideration, receipt of which is hereby acknowledged, Grantor and Grantee hereby agree as follows:

1. Grant of Easement. Grantor hereby grants to Grantee, for the benefit of the Grantee Property, the following:

(a) a permanent easement for construction and maintenance of a water channel and water dispersion facilities (the "Channel Easement") upon that certain real property owned by Grantor, more particularly described on Exhibit B-1 and depicted on Exhibit B-2 attached hereto (the "Channel Easement Area"), together with the right to enter upon such real



property at all reasonable times to remove any bushes, undergrowth and other obstructions interfering with the such facilities.

(b) an easement for surface drainage of water from the Channel Easement Area (the "Surface Drainage Easement") upon, over, across and through that certain real property owned by Grantor, more particularly described on Exhibit C-1 and depicted on Exhibit C-2 attached hereto (the "Surface Drainage Easement Area"). The Surface Drainage Easement shall automatically terminate as to all or any portion thereof on the date that the City, the County, and/or any other applicable governmental authorities cease to require the Surface Drainage Easement as a condition to the improvement of the Grantee Property as a residential development.

(c) a temporary easement for construction and maintenance of a siltation basin facility (the "Basin Easement") upon that certain real property owned by Grantor, more particularly described on Exhibit D-1 and depicted on Exhibit D-2 attached hereto (the "Basin Easement Area"), together with the right to enter upon such real property at all reasonable times to remove any bushes, undergrowth and other obstructions interfering with the such facility. The Basin Easement shall automatically terminate on the date that is six (6) months after the date hereof with respect to the Basin Easement Area, whereupon Grantee, at its sole expense, shall immediately remove all improvements within the Basin Easement Area and restore the Basin Easement Area to the same condition as existed prior to the date hereof.

The Channel Easement, the Surface Drainage Easement, and the Basin Easement are collectively referred to herein as the "Easements"; and the Channel Easement Area, the Drainage Easement Area, and the Basin Easement Area are collectively referred to herein as the "Easement Areas."

2. Non-Exclusive Easements. The Easements granted herein are non-exclusive and, accordingly, to the extent that other uses do not interfere with the use of the Easements by Grantee as permitted herein, any Grantor Parties (as hereinafter defined) shall be permitted to use the Easement Areas for any purpose they may desire including, without limitation, development of all or any portion of the Easement Areas for any purposes permitted by applicable law.

3. Repair and Maintenance. Grantee shall be solely responsible for maintaining the Easement Areas and the facilities located therein in good condition and repair, including replacement as necessary, except to the extent such maintenance is required as a result of the gross negligence or willful acts of Grantor Parties. As part of Grantee's maintenance responsibilities, Grantee shall restore the Easement Areas to the same condition as existed prior to such maintenance and/or replacement work.

4. Covenants of Grantee; Indemnity. Grantee covenants that it shall at all times comply with applicable laws, rules, regulations, ordinances and rulings (including, but not limited to, laws relating to the environment, natural resources or health and human safety), and Grantee shall indemnify and hold harmless Grantor, its officers, directors, trustees, managers, shareholders, employees, grantees, successors and assigns (collectively, "Grantor Parties") from all losses, costs, damages, claims, liabilities or expenses (including reasonably attorneys' fees) directly or indirectly suffered or incurred by or asserted against any Grantor Parties arising out of



or resulting from the use of the Easement or Easement Areas by Grantee, its employees or agents, except to the extent caused by the gross negligence or willful misconduct of Grantor Parties.

5. Default. If either party fails to perform as required hereunder and is given written notice of default, and if the defaulting party fails to correct the default within fifteen (15) days after such notice, or if in the case of a default involving potential danger to personal health or safety the defaulting party fails to correct the default within one (1) day after notice, then the nondefaulting party, at its election and in its sole discretion, may cure the default for and on behalf of the nondefaulting party, and any amounts which the non-defaulting party may expend for that purpose or which otherwise may be due by the defaulting party to the nondefaulting party shall be due on demand together with interest thereon at a rate which is the greater of fifteen percent (15%) per annum or the maximum rate permissible by law, from the date of expenditure to the date when full payment is made by the defaulting party.

6. Remedies. In the event of a breach or threatened breach of any term, covenant or condition of this Agreement, the nonbreaching party shall have, in addition to all other legal and equitable remedies available, the right to enforce the provisions hereof by injunctive relief or otherwise, without the necessity of proof of actual damage or inadequacy of any legal remedy. If any legal action or other proceeding is brought to enforce this Agreement, or because of an alleged dispute, breach, or default in connection with any of the provisions of this Agreement, the successful or prevailing party will be entitled to recover reasonable attorneys' fees and other costs incurred in that action or proceeding, in addition to any other relief to which it or they may be entitled.

7. Notices. If any notice required or desired to be given to either party hereunder shall be deemed given: (a) when delivered personally to that party, or (b) one (1) day after deposit with a nationally recognized overnight courier service, or (c) three (3) days after deposit in the United States mail, as certified mail, return receipt requested, postage prepaid. Notices delivered pursuant to subsections (b) or (c) hereof shall be delivered to the following addresses, all of which information shall be deemed current unless notice is given to the other party of a change hereto pursuant to the notice requirements herein:

If to Grantor: c/o BVR Company
655 Montgomery Street, Suite 1740
San Francisco, CA 94111
Attention: Paul B. Butler, Jr.

Copy to: Bank of America, N.A.
555 California Street, Suite 700
San Francisco, CA 94104
Attention: David McCune

If to Grantee: Centex Homes
2527 Camino Ramon, Suite 250
San Ramon, CA 94583

Attention: Holly Traube Cordova, Esq.

Copy to: Centex Homes
10509 Professional Circle Suite 200
Reno, NV 89521
Attention: Division President and Land
Acquisitions Manager

8. Successors and Assigns. The rights and obligations of Grantor and Grantee hereunder will be binding upon and will inure to the benefit of their respective successors and assigns. All provisions in this Agreement, including the benefits and burdens, shall run with the land.

9. Governing Law. This Agreement shall be construed in accordance with the laws of the State of Nevada.

10. Severability. All terms and conditions of this Agreement will be deemed severable. Should any of the terms and conditions hereof be deemed void or unenforceable, then (a) the remaining provisions will have full force and effect, and (b) those provisions deemed void or unenforceable will be interpreted, to the extent possible, so as to render such provisions enforceable and in a way consistent with the original intent of the parties hereto.

11. Counterparts. This Agreement may be executed in two or more counterparts, each of which shall be deemed an original, and all of which together shall constitute one and the same instrument.

[SIGNATURES ON FOLLOWING THREE PAGES]

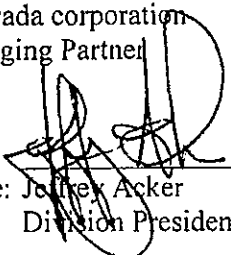


IN WITNESS WHEREOF, Grantor and Grantee have executed this Agreement on the date first above written.

GRANTEE:

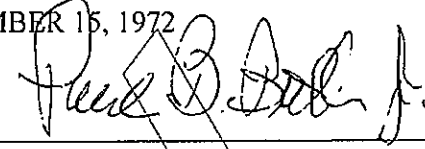
CENTEX HOMES,
a Nevada general partnership

By: Centex Real Estate Corporation,
a Nevada corporation
Title: Managing Partner

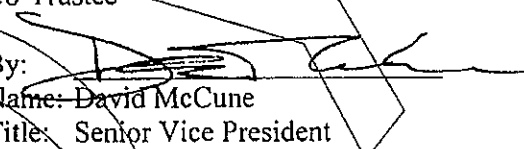
By: 
Name: Jeffrey Acker
Title: Division President

GRANTOR:

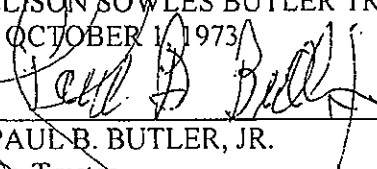
THE RUTH M. BUTLER TRUST DATED
SEPTEMBER 15, 1972

By: 
Name: PAUL B. BUTLER, JR.
Title: Co-Trustee

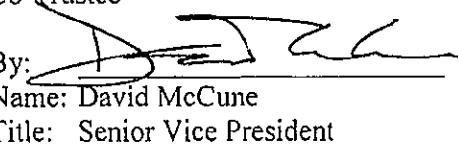
By: BANK OF AMERICA, N.A.
Title: Co-Trustee

By: 
Name: David McCune
Title: Senior Vice President

THE ALLISON SOWLES BUTLER TRUST
DATED OCTOBER 1, 1973

By: 
Name: PAUL B. BUTLER, JR.
Title: Co-Trustee

By: BANK OF AMERICA, N.A.
Title: Co-Trustee

By: 
Name: David McCune
Title: Senior Vice President

[GRANTOR SIGNATURES CONTINUED ON FOLLOWING TWO PAGES]



THE DARYL ELLEN BUTLER TRUST DATED
OCTOBER 1, 1973

By: *Paul B. Butler, Jr.*
Name: PAUL B. BUTLER, JR.
Title: Co-Trustee

By: BANK OF AMERICA, N.A.
Title: Co-Trustee

By: *[Signature]*
Name: David McCune
Title: Senior Vice President

THE PAUL BRETT BUTLER, III TRUST DATED
OCTOBER 1, 1973

By: *Paul B. Butler, Jr.*
Name: PAUL B. BUTLER, JR.
Title: Co-Trustee


By: BANK OF AMERICA, N.A.
Title: Co-Trustee

By: *[Signature]*
Name: David McCune
Title: Senior Vice President

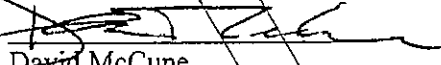
[GRANTOR SIGNATURES CONTINUED ON FOLLOWING PAGE]



THE SHELLEY BRYANT BUTLER TRUST DATED
OCTOBER 1, 1973

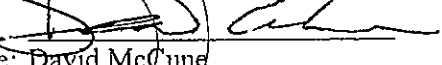
By: 
Name: PAUL B. BUTLER, JR.
Title: Co-Trustee

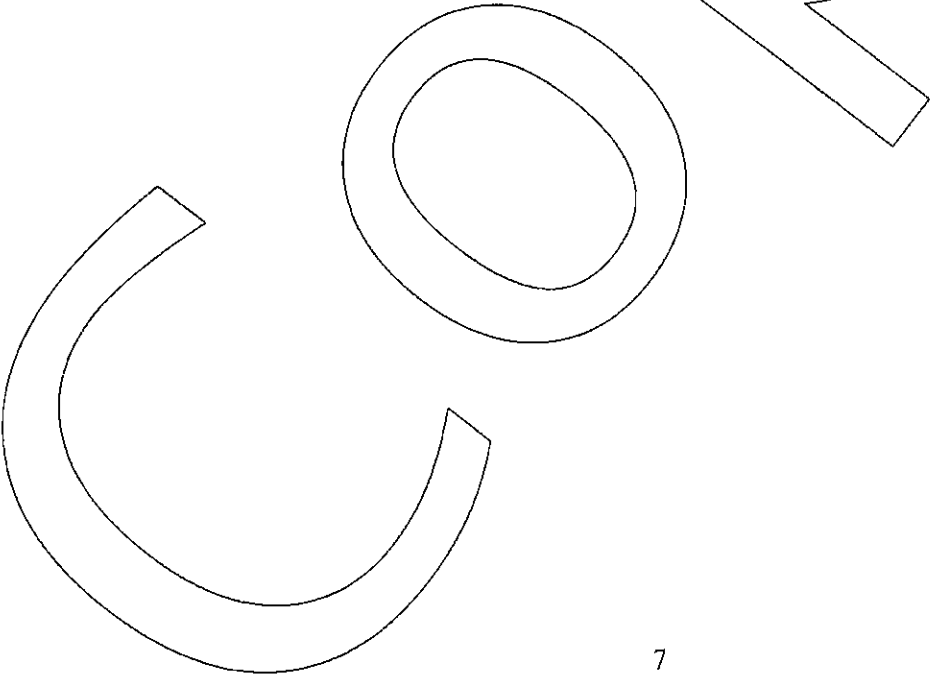
By: BANK OF AMERICA, N.A.
Title: Co-Trustee

By: 
Name: David McCune
Title: Senior Vice President

THE PAUL B. BUTLER TRUST DATED AUGUST
10, 1971

By: BANK OF AMERICA, N.A.
Title: Trustee

By: 
Name: David McCune
Title: Senior Vice President





STATE OF CALIFORNIA

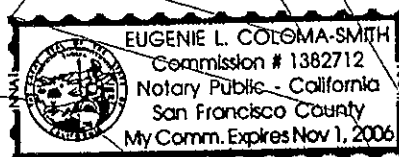
COUNTY OF SAN FRANCISCO

On June 8, 2006 before me, Eugenie Coloma-Smith, a notary public for the State of California, personally appeared Paul B. Butler, Jr., personally known to me (or proved to me on the basis of satisfactory evidence) to be the person(s) whose name(s) ~~is~~ are subscribed to the within instrument, and acknowledged to me that ~~he~~ she/they executed the same in ~~his~~ her/their authorized capacity(ies) and that by ~~his~~ her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

WITNESS my hand and official seal

(SEAL)

Eugenie Coloma-Smith
(Signature)



STATE OF CALIFORNIA

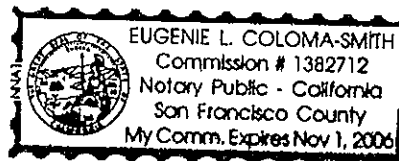
COUNTY OF SAN FRANCISCO

On June 8, 2006 before me, Eugenie Coloma-Smith, a notary public for the State of California, personally appeared David McCune, personally known to me (or proved to me on the basis of satisfactory evidence) to be the person(s) whose name(s) ~~is~~ are subscribed to the within instrument, and acknowledged to me that ~~he~~ she/they executed the same in ~~his~~ her/their authorized capacity(ies) and that by ~~his~~ her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

WITNESS my hand and official seal

(SEAL)

Eugenie Coloma-Smith
(Signature)





STATE OF CALIFORNIA

COUNTY OF SAN FRANCISCO

On June 8, 2006 before me, Eugenie Coloma Smith, a notary public for the State of California, personally appeared Jeffrey Acker, personally known to me (or proved to me on the basis of satisfactory evidence) to be the person(s) whose name(s) is/are subscribed to the within instrument, and acknowledged to me that he/she/they executed the same in ~~his~~/her/their authorized capacity(ies) and that by ~~his~~/her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

WITNESS my hand and official seal

(SEAL)

Eugenie Coloma Smith
(Signature)



COPY



LEGAL DESCRIPTION OF GRANTEE PROPERTY

All that certain real property situate in the City of Reno, County of Washoe, State of Nevada, being Parcels B and C, as depicted on that certain Parcel Map filed for record with the Washoe County Recorder on the 10th day of March, 2006, assigned official number 3359967.

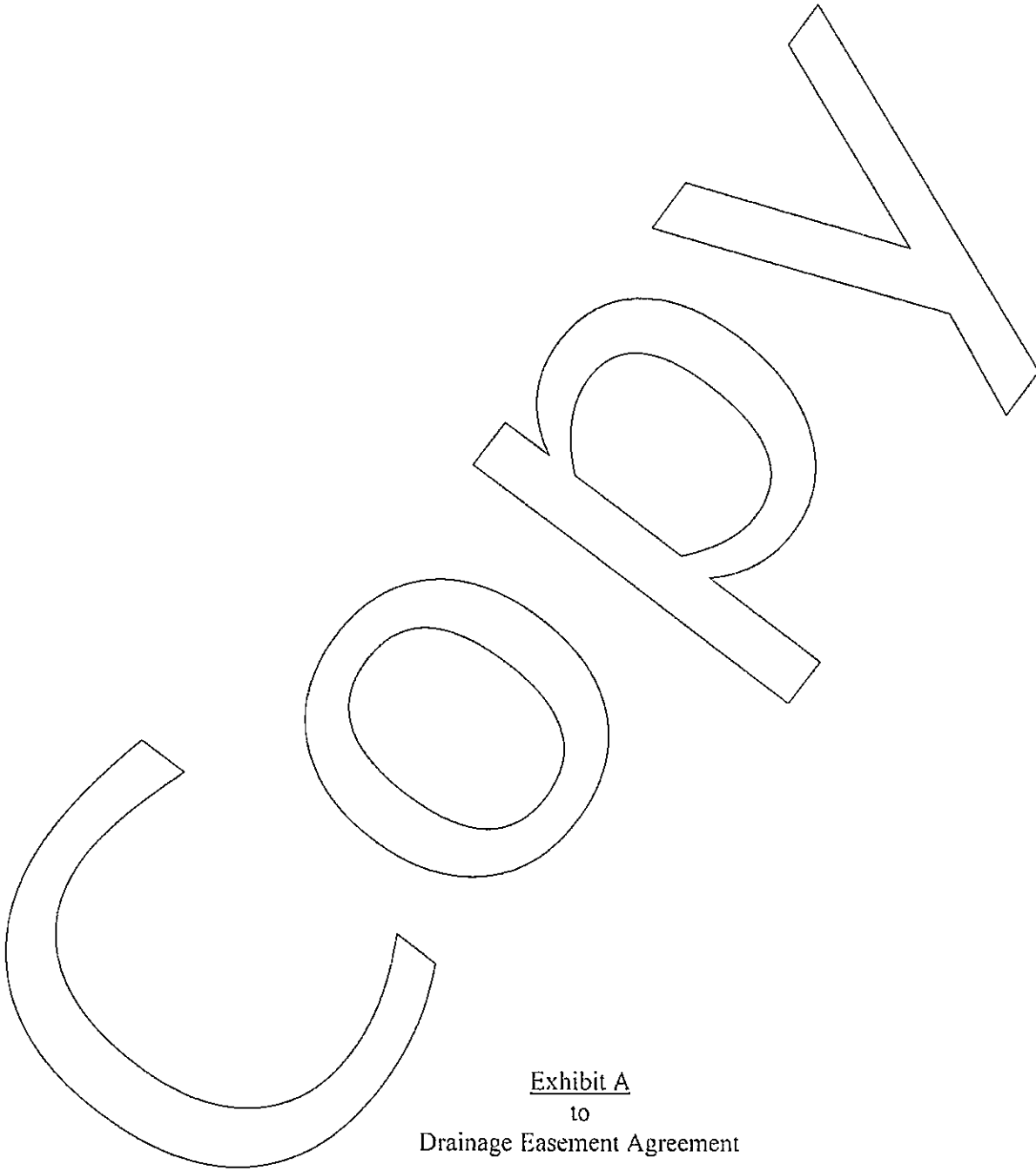


Exhibit A

10

Drainage Easement Agreement



LEGAL DESCRIPTION OF CHANNEL EASEMENT AREA

All that certain real property situate within the southeast one-quarter (1/4) Section 3, T 18 N, R 20 E, MDM, City of Reno, County of Washoe, State of Nevada, lying within Parcel A of "Parcel Map Of Bella Vista Ranch" filed in the office of the Washoe County Recorder March 10, 2006, as Parcel Map 4526, File No. 3359967, Official Records of Washoe County, Nevada, more particularly described as follows:

BEGINNING at a point on said easement, from which point the Northwest corner of said Section Three (3), also known as Washoe County GPS point "WS1045", bears N 39°07'44" W, 3998.08 feet;

Thence, N 87°36'52" E, 61.00 feet;

Thence, along the arc of a non-tangent curve to the left from a tangent which bears S 02°25'27" E, having a radius of 1475.00 feet, a central angle of 10°01'30" and an arc length of 258.08 feet;

Thence, S 12°26'58" E, 183.60 feet;

Thence, S 23°14'10" E, 483.56 feet;

Thence, S 12°26'58" E, 131.75 feet;

Thence, along the arc of a tangent curve to the left, having a radius of 1184.50 feet, a central angle of 07°27'36", and an arc length of 154.23 feet, to the south line of said Parcel A;

Thence, along said south line, S 67°19'56" W, 213.31 feet;

Thence, continuing along said south line, along the arc of a tangent curve to the right, having a radius of 1343.00 feet, a central angle of 01°14'01", and an arc length of 28.91 feet;

Thence, leaving said south line, along the arc of a non-tangent curve to the right, from a tangent which bears N 20°21'55" W, having a radius of 1426.50 feet, a central angle of 07°54'57" and an arc length of 197.08 feet;

Thence, N 12°26'58" W, 113.67 feet;

Thence, N 01°57'36" W, 497.11 feet;

Thence, N 12°26'58" W, 187.90 feet;

Thence, along the arc of a tangent curve to the right, having a radius of 1536.00 feet, a central angle of 10°01'36", and an arc length of 268.80 feet, to the Point of Beginning.

CONTAINING: 3.96 acres of land, more or less.

BASIS OF BEARINGS: Nevada State Plane coordinated system, West Zone (NAD 83/94)..

Exhibit B-1

to

Drainage Easement Agreement



3399487
 96/12/2086
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DEPICTION OF CHANNEL EASEMENT AREA

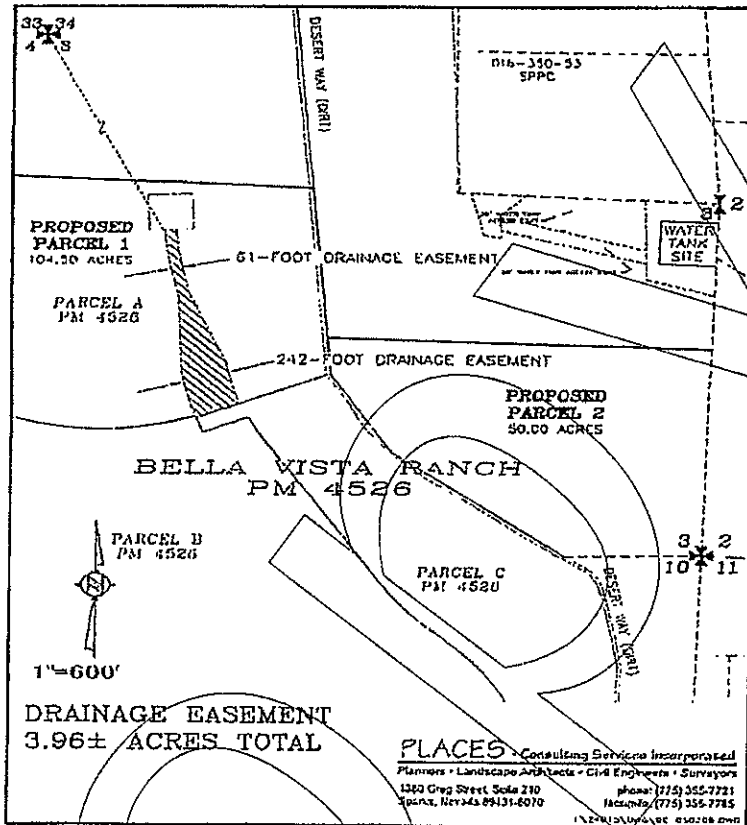


Exhibit B-2

to

Drainage Easement Agreement



3399487
06/12/2006
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LEGAL DESCRIPTION OF SURFACE DRAINAGE EASEMENT AREA

All that certain real property situate in a portion of Section 3, Township 18 North, Range 20 East, Mount Diablo Meridian, City of Reno, County of Washoe, State of Nevada, and being described as a portion of Parcel A of Parcel Map 4526 as recorded in Washoe County Official Records on March 10, 2006 under filing No. 3359967, more particularly described as follows:

COMMENCING at the Northwest corner of said Section Three (3), also known as Washoe County GPS point "WS1045", thence along the north line of said Section 3, N 88°07'21" E, 1147.20 feet, to the POINT OF BEGINNING:

Thence, continuing along the North line of said Section 3, N 88°07'21" E, 1441.44 feet;

Thence, leaving the said North line, along the West line of Lease Area #2 as shown on Record of Survey 4092 as recorded in Washoe County Official Records on June 10, 2002, under filing No. 2697841, the following six (6) courses;

- 1) S 52°06'39" E, 206.31 feet;
- 2) S 26°48'35" E, 219.31 feet;
- 3) S 46°40'54" E, 348.36 feet;
- 4) S 07°04'19" E, 720.02 feet;
- 5) S 00°29'07" E, 245.20 feet;
- 6) S 04°45'31" E, 2622.13 feet, to a point on the South line of said Parcel A;

Thence, leaving said West line, along said South line, the following seven (7) arcs, courses and distances;

- 1) S 67°19'56" W, 746.07 feet,
- 2) Along the arc of a tangent curve to the right, having a radius of 1343.00 feet, a central angle of 01°18'16", and an arc length of 30.58 feet,
- 3) N 21°21'48" W, 14.50 feet,
- 4) Along the arc of a non-tangent curve to the right, from a tangent which bears S 68°38'12" E, having a radius of 1328.50 feet, a central angle of 63°46'28" and an arc length of 1478.72 feet,

Exhibit C-1

to

Drainage Easement Agreement



- 5) Along the arc of a reverse curve to the left, having a radius of 1000.00 feet, a central angle of $09^{\circ}37'33''$, and an arc length of 168.00 feet,
- 6) N $57^{\circ}12'52''$ W, 170.11 feet,
- 7) Along the arc of a tangent curve to the left, having a radius of 2059.00 feet, a central angle of $32^{\circ}45'08''$, and an arc length of 1176.99 feet, to a point on the West line of said Parcel A;

Thence, along the West line of said Parcel, N $01^{\circ}23'46''$ E, 504.29 feet,

Thence, continuing along said West line, N $01^{\circ}10'39''$ E, 1702.75 feet;

Thence, leaving said West line, N $01^{\circ}10'39''$ E, 611.17 feet, to the south line of Lease Area #1 as shown on said Record of Survey 4092;

Thence, along said South line of Lease Area #1, the following four (4) arcs, courses and distances;

- 1) Along the arc of a non-tangent curve to the left, from a tangent which bears S $47^{\circ}39'15''$ E, having a radius of 450.00 feet, a central angle of $74^{\circ}39'25''$ and an arc length of 586.35 feet,
- 2) N $57^{\circ}41'20''$ E, 658.22 feet,
- 3) Along the arc of a tangent curve to the left, having a radius of 300.00 feet, a central angle of $83^{\circ}11'08''$, and an arc length of 435.56 feet,
- 4) N $25^{\circ}29'48''$ W, 98.94 feet, to the Point of Beginning.

CONTAINING: 288.15 acres of land, more or less.

BASIS OF BEARINGS: Nevada State Plane coordinate system, West Zone Modified (NAD 83/94).

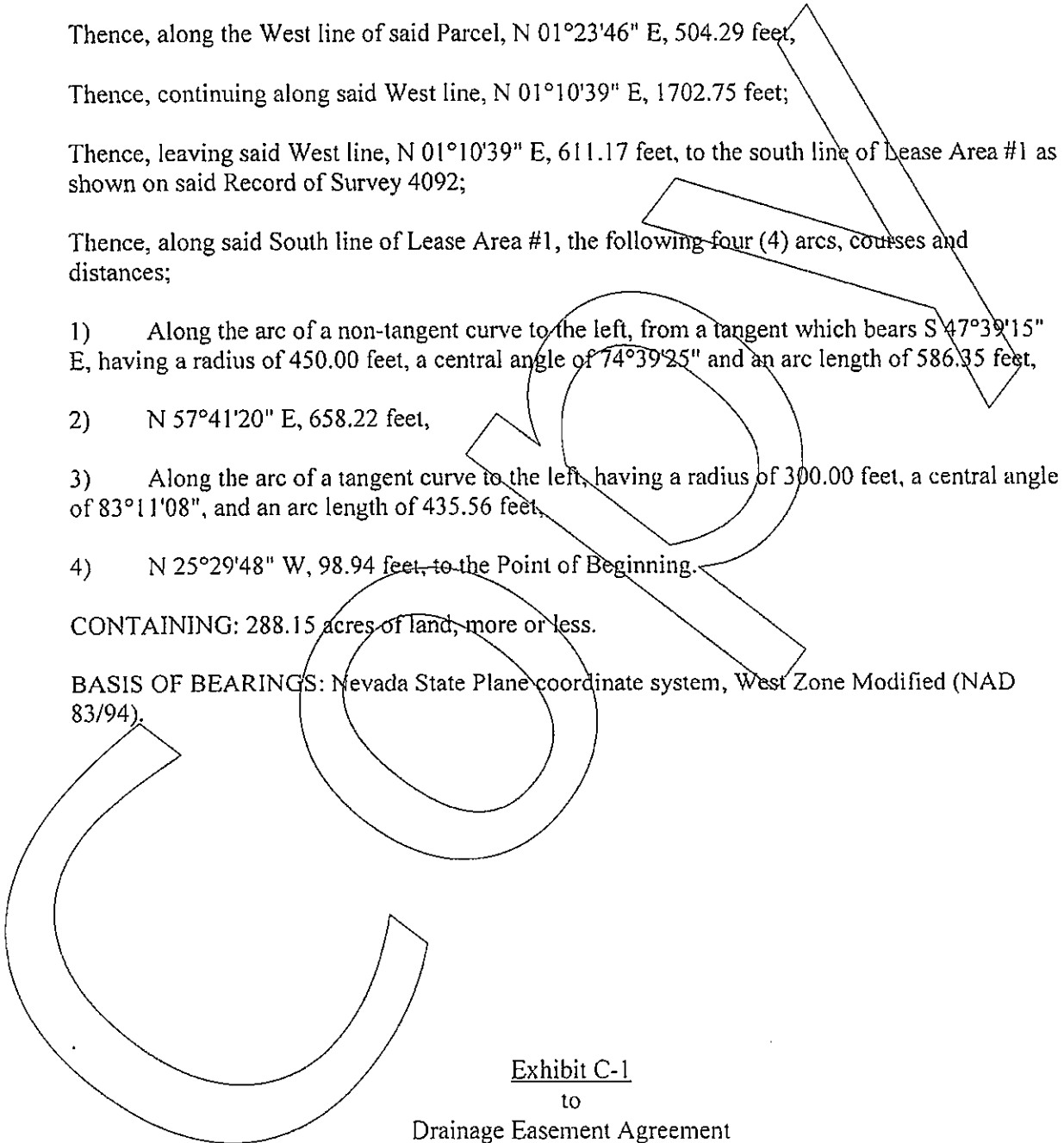


Exhibit C-1
to
Drainage Easement Agreement



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06/12/2006
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DEPICTION OF SURFACE DRAINAGE EASEMENT AREA

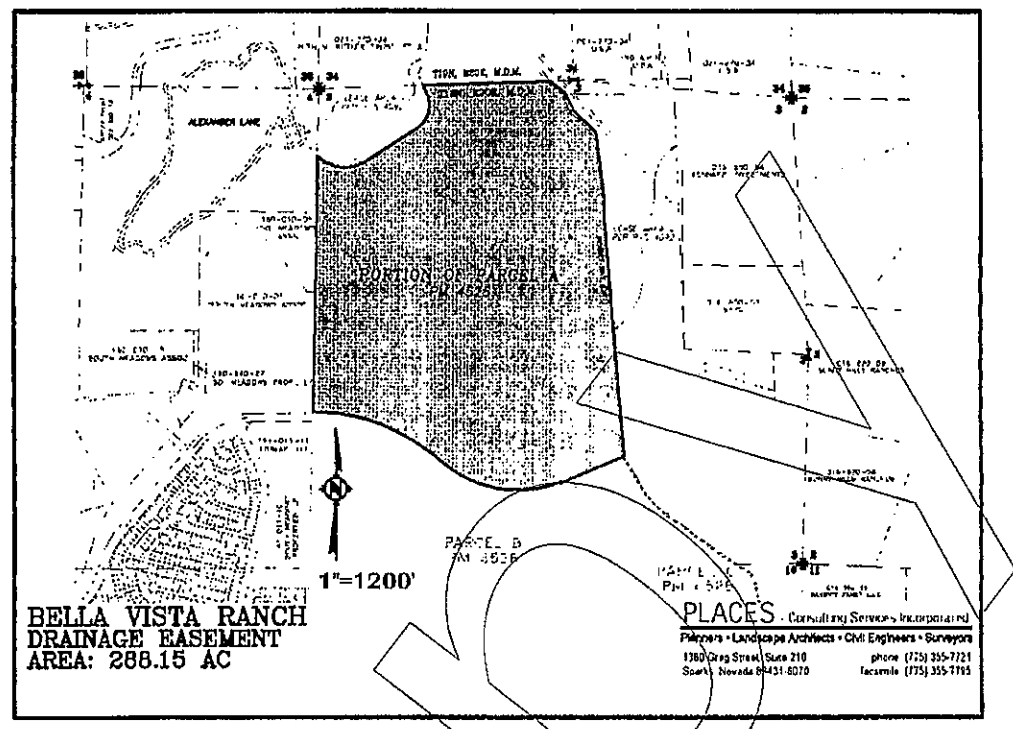


Exhibit C-2
to
Drainage Easement Agreement



LEGAL DESCRIPTION OF BASIN EASEMENT AREA

All that certain real property situate within the southeast one-quarter (1/4) Section 3, T 18 N, R 20 E, MDM, City of Reno, County of Washoe, State of Nevada, lying within Parcel A of "Parcel Map Of Bella Vista Ranch" filed in the office of the Washoe County Recorder March 10, 2006, as Parcel Map 4526, File No. 3359967, Official Records of Washoe County, Nevada, more particularly described as follows:

BEGINNING at a point on said easement, from which point the Northwest corner of said Section Three (3), also known as Washoe County GPS point "WS1045", bears N 40°18'42" W, 3766.55 feet;

Thence, N 88°12'25" E, 230.00 feet;

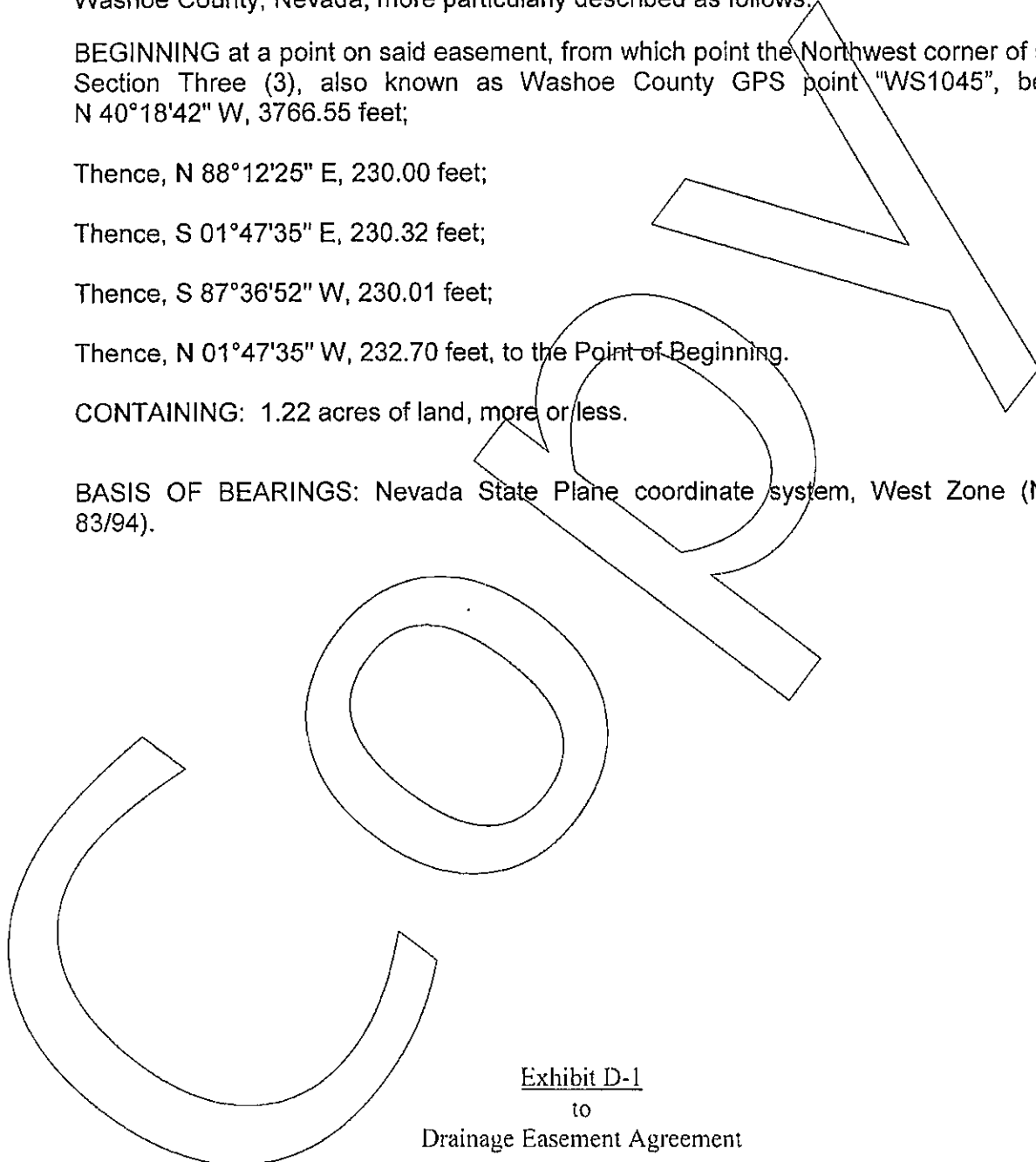
Thence, S 01°47'35" E, 230.32 feet;

Thence, S 87°36'52" W, 230.01 feet;

Thence, N 01°47'35" W, 232.70 feet, to the Point of Beginning.

CONTAINING: 1.22 acres of land, more or less.

BASIS OF BEARINGS: Nevada State Plane coordinate system, West Zone (NAD 83/94).





DEPICTION OF SILTATION BASIN EASEMENT AREA

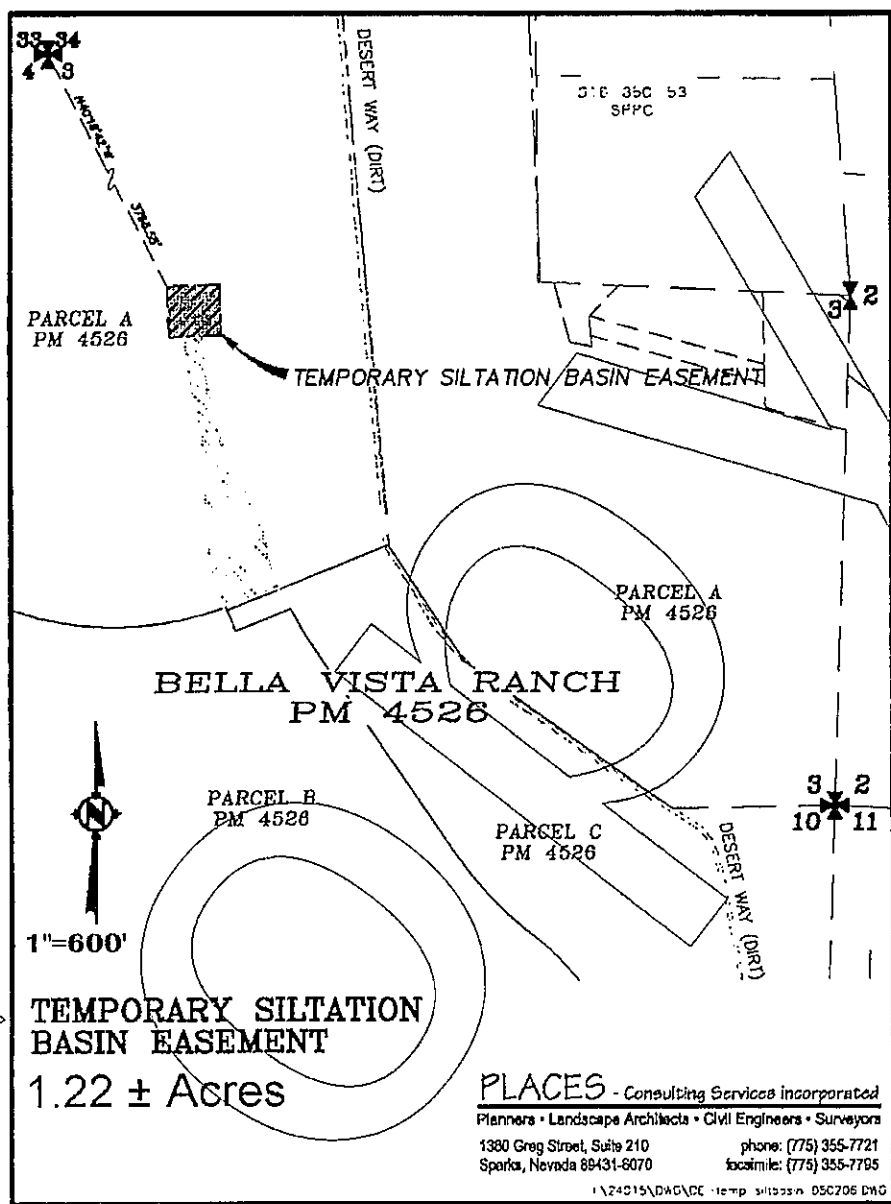


Exhibit D-2
to
Drainage Easement Agreement



3399487
66/12/2886
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WASHOE COUNTY RECORDER

OFFICE OF THE RECORDER
KATHRYN L. BURKE, RECORDER

1001 E. NINTH STREET
POST OFFICE BOX 11130
RENO, NEVADA 89520-0027
PHONE (775) 328-3661
FAX (775) 325-8010

LEGIBILITY NOTICE

The Washoe County Recorder's Office has determined that the attached document may not be suitable for recording by the method used by the Recorder to preserve the Recorder's records. The customer was advised that copies reproduced from the recorded document would not be legible. However, the customer demanded that the document be recorded without delay as the parties rights may be adversely affected because of a delay in recording. Therefore, pursuant to NRS 247.120 (3), the County Recorder accepted the document conditionally, based on the undersigned's representation (1) that a suitable copy will be submitted at a later date (2) it is impossible or impracticable to submit a more suitable copy.

By my signing below, I acknowledge that I have been advised that once the document has been microfilmed it may not reproduce a legible copy.

Lisa Quilici

Signature

6/12/06

Date

Lisa Quilici

Printed Name



APPENDIX B

SUPPORTING CALCULATIONS

**Basins 1 and 3
As-Built UPDATE**

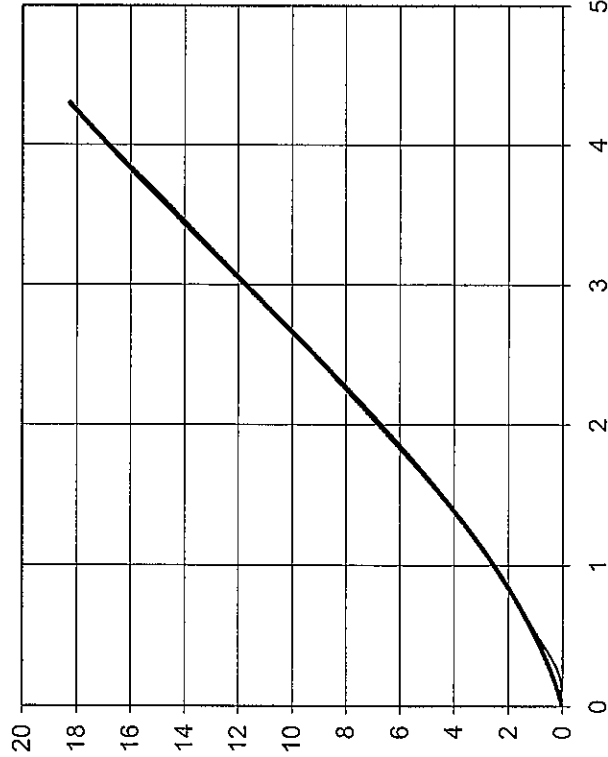


Feet	Feet Elevation	cy Volume	cf Volume	af Volume	Calc Vol	Volume Curve Fit			
Depth						C3	C2	C1	C0
0	4437.7	0.000	0	0.000	0	-0.1299	1.2055	1.4644	0
0.3	4438	470	12690	0.291	0.544				
1.3	4439	5984	161568	3.709	3.656				4437.70
2.3	4440	13346	360342	8.272	8.165				4442.14
3.3	4441	21250	573750	13.171	13.292				18.897
4.3	4442	29517	796959	18.296	18.259				
4.44					18.897				

Volume vs Depth

$$y = -0.1299x^3 + 1.2055x^2 + 1.4644x$$

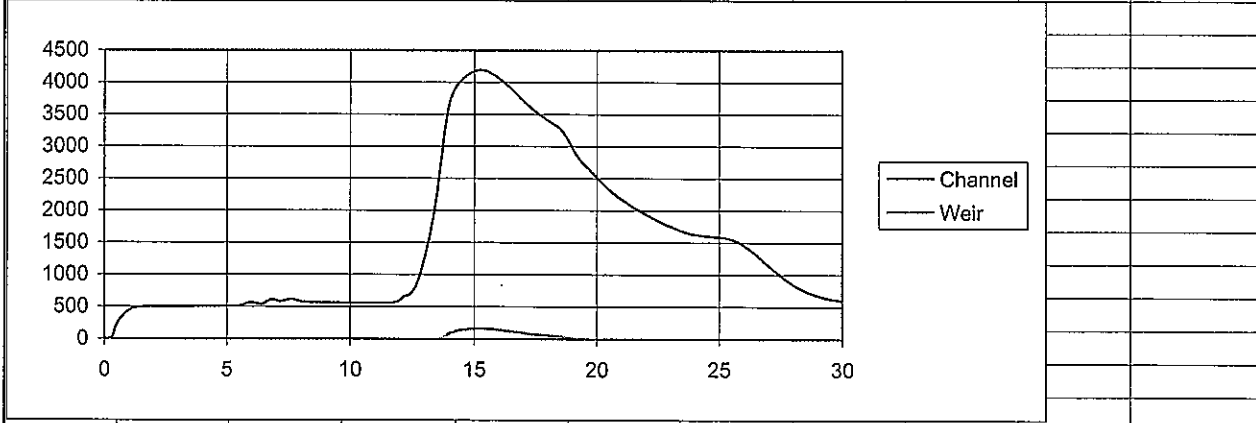
$R^2 = 0.9997$



Current stratum: Basin 1 Site	Elevation	
Current stratum: Basin 1 Site	4438	Cut = 16351 Fill = 470
Site name = Basin 1 Site	4739	Cut = 11467 Fill = 5984
Low Point in Basin is 4437.7	4440	Cut = 8648 Fill = 13346
From Surface Calculations	4441	Cut = 6371 Fill = 21250
	4442	Cut = 4458 Fill = 29517

Hydrograph at Lateral Weir

5	Node Name			STM+E	0					
STM+E	50005	27-Jul	0	0	1	1	360	71.415		
0	0.474	6.993	41.047	124.436	220.874	276.886	318.086	353.606	387.734	
417.612	441.629	459.646	472.588	481.628	487.842	492.07	494.932	496.863	498.164	
499.039	499.628	500.025	500.291	500.47	500.591	500.674	500.733	500.782	500.829	
500.882	500.946	501.02	501.104	501.196	501.295	501.4	501.509	501.623	501.742	
501.874	502.034	502.241	502.505	502.824	503.179	503.549	503.919	504.282	504.637	
504.987	505.339	505.697	506.069	506.459	506.865	507.278	507.683	508.042	508.296	
508.422	508.452	508.437	508.482	509.054	511.457	517.439	527.44	539.63	550.996	
558.824	561.571	559.174	552.852	544.75	537.967	536.636	544.592	562.164	584.154	
602.299	610.414	607.435	597.32	586.769	581.288	582.596	589.346	598.968	608.455	
614.701	615.489	610.581	601.743	591.822	583.347	577.265	573.093	570.076	567.817	
566.16	564.949	564.02	563.249	562.565	561.93	561.326	560.746	560.194	559.675	
559.184	558.698	558.186	557.631	557.059	556.54	556.115	555.763	555.447	555.144	
554.844	554.553	554.284	554.031	553.799	553.601	553.417	553.255	553.155	553.095	
553.085	553.171	553.339	553.604	554.022	554.574	555.293	556.265	557.442	559.989	
565.465	572.977	584.843	605.68	633.605	657.873	671.297	681.511	702.635	739.169	
790.219	856.654	939.329	1040.45	1157.94	1285.02	1419.67	1565.91	1725.44	1900.3	
2094.82	2313.98	2559.9	2827.74	3098.2	3340.22	3534.72	3680.47	3787.55	3866.66	
3925.94	3972.32	4010.73	4044.07	4073.81	4100.5	4124.21	4144.78	4161.95	4175.46	
4185.15	4190.91	4192.76	4190.78	4185.05	4175.74	4163.04	4147.25	4128.74	4107.91	
4085.17	4060.91	4035.51	4009.3	3982.58	3955.54	3928.15	3899.81	3869.65	3837.47	
3804.18	3770.85	3738.16	3706.53	3676.13	3647.05	3619.28	3592.77	3567.5	3543.36	
3519.83	3496.28	3472.75	3449.65	3427.3	3405.88	3385.46	3366	3347.3	3328.31	
3306.2	3277.28	3239.79	3194.84	3144.79	3091.1	3033.78	2973.81	2915.26	2861.89	
2815.12	2774.9	2740.02	2708.43	2678.08	2647.61	2616.37	2583.99	2550.16	2515.43	
2481.28	2448.44	2416.94	2386.65	2357.44	2329.26	2302.06	2275.76	2250.33	2225.69	
2201.79	2178.59	2156.07	2134.22	2113.03	2092.48	2072.53	2053.13	2034.21	2015.67	
1997.42	1979.4	1961.54	1943.82	1926.26	1908.89	1891.75	1874.89	1858.35	1842.16	
1826.35	1810.92	1795.87	1781.22	1766.96	1753.09	1739.61	1726.52	1713.85	1701.62	
1689.9	1678.78	1668.38	1658.81	1650.13	1642.39	1635.57	1629.57	1624.22	1619.35	
1614.81	1610.51	1606.45	1602.67	1599.22	1596.14	1593.44	1591.03	1588.72	1586.24	
1583.27	1579.48	1574.58	1568.34	1560.61	1551.25	1540.19	1527.38	1512.8	1496.45	
1478.37	1458.64	1437.38	1414.74	1390.92	1366.12	1340.33	1313.19	1284.4	1254.91	
1226.12	1197.93	1170.1	1142.51	1115.15	1088.1	1061.43	1035.23	1009.58	984.491	
959.845	935.55	911.985	889.638	868.385	848.146	828.864	810.518	793.095	776.583	
760.963	746.217	732.321	719.253	706.981	695.477	684.707	674.636	665.224	656.431	
648.218	640.545	633.377	626.678	620.416	614.56	609.081	603.955	599.155	594.66	

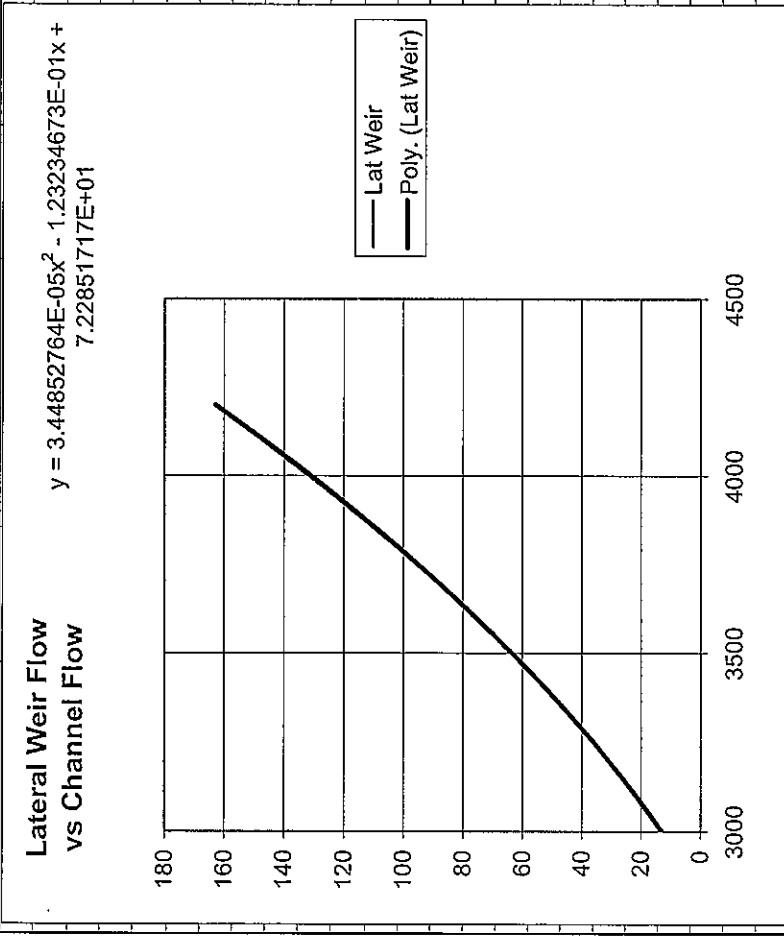


Lateral Weir Calculations

HEC-RAS Plan: latweir		River: Steamboat		Reach: Bella Vista		
Reach	River Sta	Profile	Q US (cfs)	Q Leaving (cfs)	Q DS (cfs)	Q Weir (cfs)
Bella Vista	84.5	PF 1	4200	162.77	4038.02	162.77
Bella Vista	84.5	PF 2	3780	99.95	3680.65	99.95
Bella Vista	84.5	PF 3	3360	46.78	3313.66	46.78
Bella Vista	84.5	PF 4	2950	9.11	2941.02	9.11

Flowline of Weir = 4441.8
Length of Bottom = 50 ft
Wings = 25 ft
Coeff = 3.0

Lateral Weir Discharge vs Channel Flow			
C3	C2	C1	C0
0	3.44852764E-05	-1.23234673E-01	7.22851717E+01

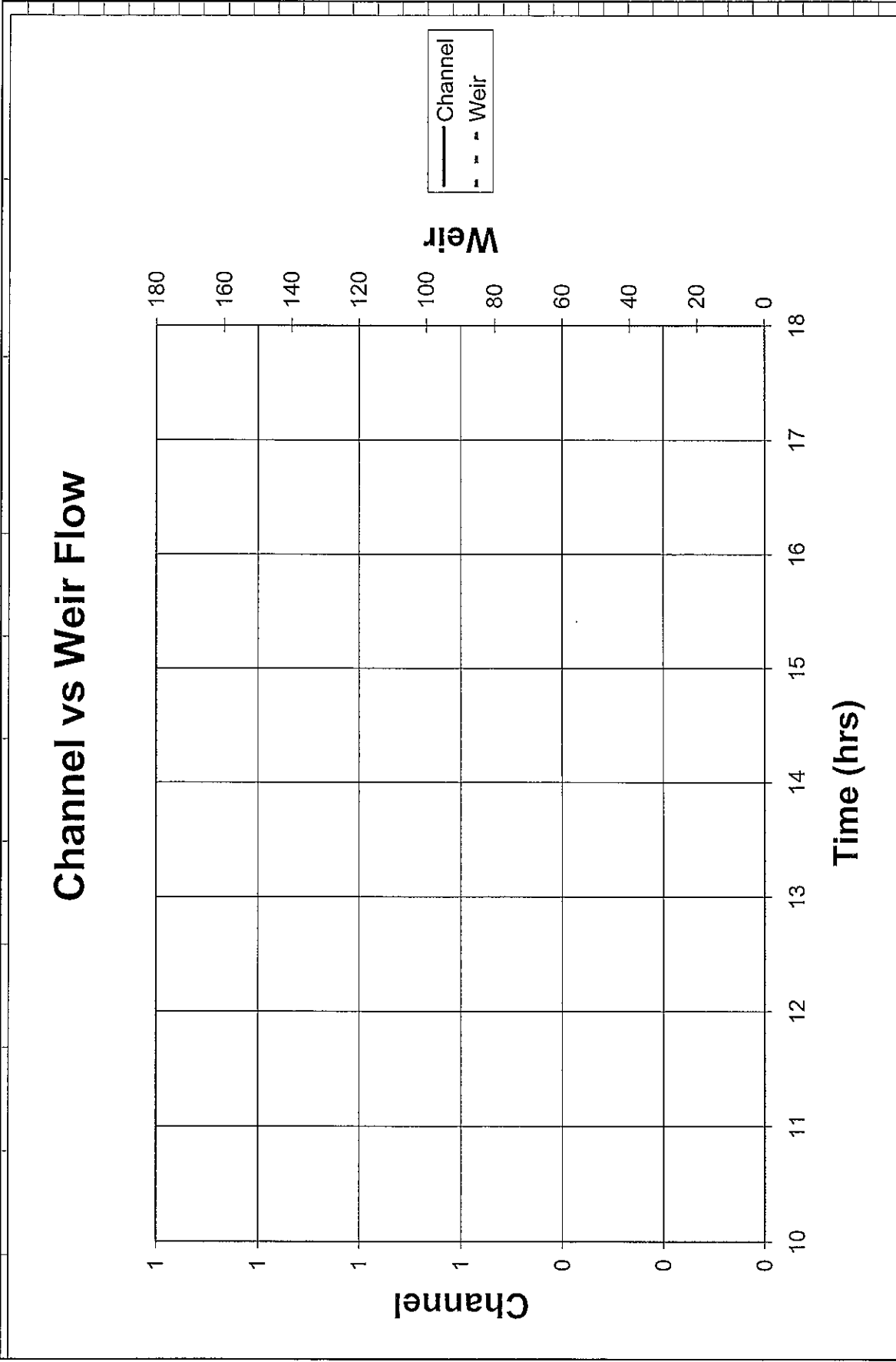


Volume To Basin	
Volume Removed	43.46

Storage Basin 1

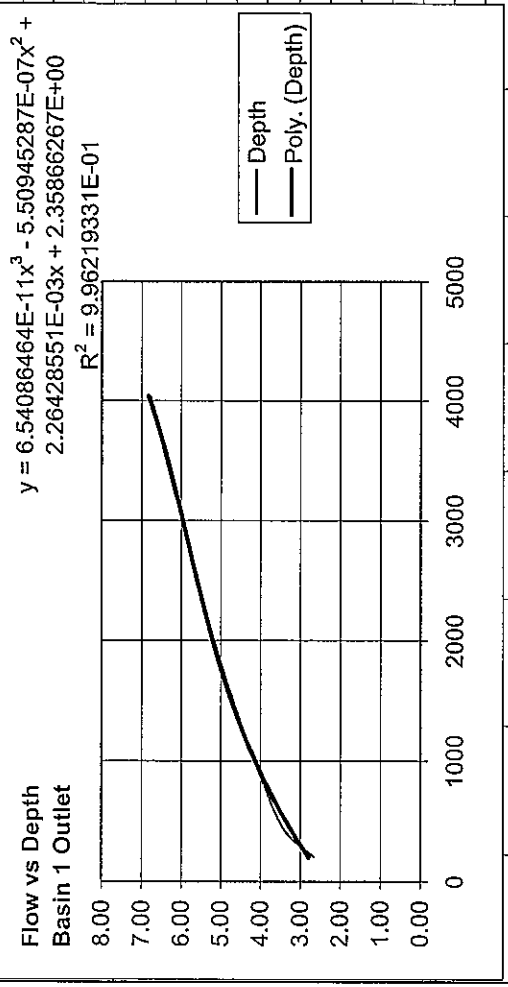
Lateral Weir Calculations

Hours Time	Flow		Vol Basin	Flow		Hours Time	Flow	
	Channel	Weir		Channel	Weir			
11.00	0.00	0.00	0.00	0.00	0.00	13.83	0.00	0.00
11.08	0.00	0.00	0.00	0.00	0.00	13.92	0.00	0.00
11.17	0.00	0.00	0.00	0.00	0.00	14.00	0.00	0.00
11.25	0.00	0.00	0.00	0.00	0.00	14.08	0.00	0.00
11.33	0.00	0.00	0.00	0.00	0.00	14.17	0.00	0.00
11.42	0.00	0.00	0.00	0.00	0.00	14.25	0.00	0.00
11.50	0.00	0.00	0.00	0.00	0.00	14.33	0.00	0.00
11.58	0.00	0.00	0.00	0.00	0.00	14.42	0.00	0.00
11.67	0.00	0.00	0.00	0.00	0.00	14.50	0.00	0.00
11.75	0.00	0.00	0.00	0.00	0.00	14.58	0.00	0.00
11.83	0.00	0.00	0.00	0.00	0.00	14.67	0.00	0.00
11.92	0.00	0.00	0.00	0.00	0.00	14.75	0.00	0.00
12.00	0.00	0.00	0.00	0.00	0.00	14.83	0.00	0.00
12.08	0.00	0.00	0.00	0.00	0.00	14.92	0.00	0.00
12.17	0.00	0.00	0.00	0.00	0.00	15.00	0.00	0.00
12.25	0.00	0.00	0.00	0.00	0.00	15.08	0.00	0.00
12.33	0.00	0.00	0.00	0.00	0.00	15.17	0.00	0.00
12.42	0.00	0.00	0.00	0.00	0.00	15.25	0.00	0.00
12.50	0.00	0.00	0.00	0.00	0.00	15.33	0.00	0.00
12.58	0.00	0.00	0.00	0.00	0.00	15.42	0.00	0.00
12.67	0.00	0.00	0.00	0.00	0.00	15.50	0.00	0.00
12.75	0.00	0.00	0.00	0.00	0.00	15.58	0.00	0.00
12.83	0.00	0.00	0.00	0.00	0.00	15.67	0.00	0.00
12.92	0.00	0.00	0.00	0.00	0.00	15.75	0.00	0.00
13.00	0.00	0.00	0.00	0.00	0.00	15.83	0.00	0.00
13.08	0.00	0.00	0.00	0.00	0.00	15.92	0.00	0.00
13.17	0.00	0.00	0.00	0.00	0.00	16.00	0.00	0.00
13.25	0.00	0.00	0.00	0.00	0.00	16.08	0.00	0.00
13.33	0.00	0.00	0.00	0.00	0.00	16.17	0.00	0.00
13.42	0.00	0.00	0.00	0.00	0.00	16.25	0.00	0.00
13.50	0.00	0.00	0.00	0.00	0.00	16.33	0.00	0.00
13.58	0.00	0.00	0.00	0.00	0.00	16.42	0.00	0.00
13.67	0.00	0.00	0.00	0.00	0.00	16.50	0.00	0.00
13.75	0.00	0.00	0.00	0.00	0.00	16.58	0.00	0.00



Depth vs Channel Flow

HEC-RAS Plan: Depth River: Steamboat Reach: Bella Vista		Reach: Bella Vista				
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Depth (ft)
Bella Vista	74.75	PF 1	4038.02	4434.09	4440.87	6.78
Bella Vista	74.75	PF 2	3680.65	4434.09	4440.61	6.52
Bella Vista	74.75	PF 3	3313.66	4434.09	4440.33	6.24
Bella Vista	74.75	PF 4	2941.02	4434.09	4440.03	5.94
Bella Vista	74.75	PF 5	2520	4434.09	4439.69	5.60
Bella Vista	74.75	PF 6	2100	4434.09	4439.34	5.25
Bella Vista	74.75	PF 7	1680	4434.09	4438.95	4.86
Bella Vista	74.75	PF 8	1260	4434.09	4438.53	4.44
Bella Vista	74.75	PF 9	840	4434.09	4438.06	3.97
Bella Vista	74.75	PF 10	420	4434.09	4437.48	3.39
Bella Vista	74.75	PF 11	200	4434.09	4436.73	2.64
Channel Flow vs Channel Depth of Flow						
			C3	C2	C1	C0
			6.5408665E-11	-5.509453E-07	2.264286E-03	2.3586663E+00
			Channel Flow	HEC-RAS	Curve	
			4038.02	6.78	6.83	
			3680.65	6.52	6.49	
			3313.66	6.24	6.19	
			2941.02	5.94	5.92	
			2520	5.60	5.61	
			2100	5.25	5.29	
			1680	4.86	4.92	
			1260	4.44	4.47	
			840	3.97	3.91	
			420	3.39	3.22	
			200	2.64	2.79	
			4111	0.00	6.90	

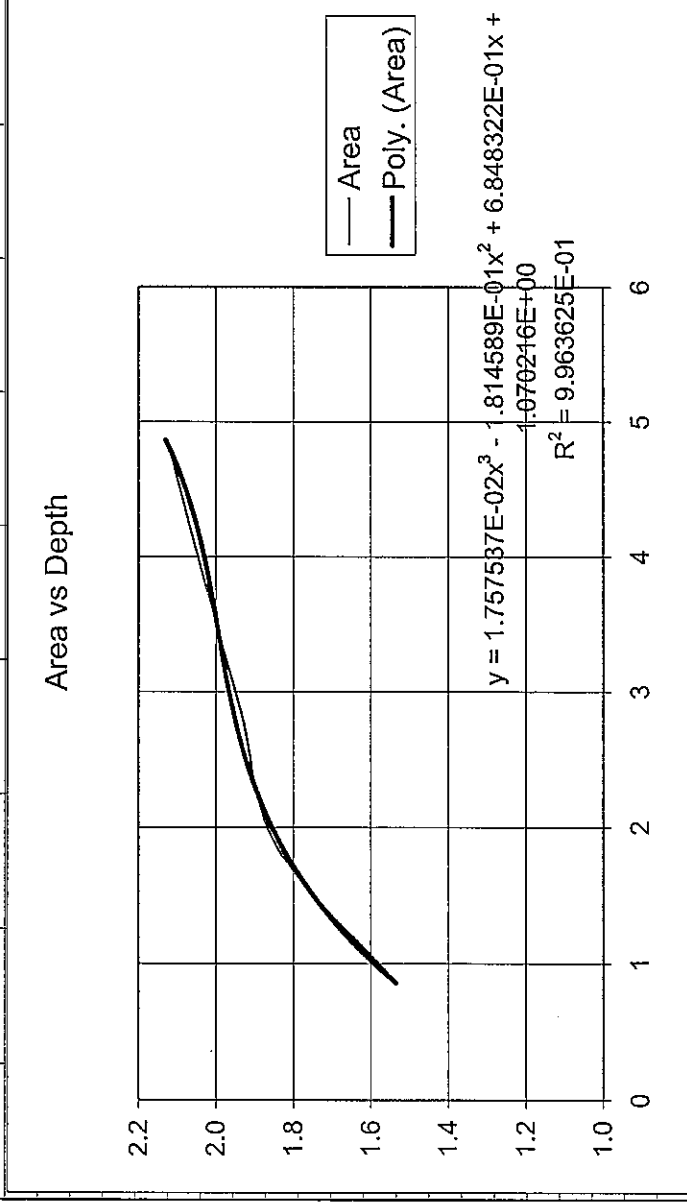


Per	Time		Chn. Flow cfs	Weir Out cfs	Weir AF AF
	Hrs				
198	16.50		3899.81	116.16	0.80
199	16.58		3869.65	111.80	0.77
200	16.67		3837.47	107.21	0.74
201	16.75		3804.18	102.54	0.71
202	16.83		3770.85	97.94	0.67
203	16.92		3738.16	93.51	0.64
204	17.00		3706.53	89.28	0.61
205	17.08		3676.13	85.29	0.59
206	17.17		3647.05	81.53	0.56
207	17.25		3619.28	77.99	0.54
208	17.33		3592.77	74.67	0.51
209	17.42		3567.50	71.54	0.49
210	17.50		3543.36	68.60	0.47
211	17.58		3519.83	65.76	0.45
212	17.67		3496.28	62.97	0.43
213	17.75		3472.75	60.21	0.41
214	17.83		3449.65	57.55	0.40
215	17.92		3427.30	55.00	0.38
216	18.00		3405.88	52.59	0.36
217	18.08		3385.46	50.33	0.35
218	18.17		3366.00	48.19	0.33
219	18.25		3347.30	46.17	0.32
220	18.33		3328.31	44.14	0.30
221	18.42		3306.20	41.80	0.29
222	18.50		3277.28	38.80	0.27
223	18.58		3239.79	35.00	0.24
224	18.67		3194.84	30.56	0.21
225	18.75		3144.79	25.79	0.18
226	18.83		3091.10	20.86	0.14
227	18.92		3033.78	15.81	0.11
228	19.00		2973.81	10.78	0.07
229	19.08		2915.26	6.11	0.04
230	19.17		2861.89	2.05	0.01
231	19.25		2815.12	0.00	0.00

Channel Flow	Channel W.S.	Time Hours	Channel Depth	Storage Bas Vol by depth	Basin W.S.	Basin Depth	Average Delta WS	Outflow 3	Outflow Volume	Storage Volume by outflow
4061	4440.94	16.00	6.85	18.90	4442.14	4.44				18.90
3406	4440.35	18.00	6.26	18.85	4442.13	4.43	1.489	0.288	0.048	18.85
2515	4439.70	20.00	5.61	18.79	4442.12	4.42	2.097	0.342	0.057	18.79
1944	4439.25	22.00	5.16	18.73	4442.10	4.40	2.636	0.383	0.063	18.73
1630	4438.96	24.00	4.87	18.66	4442.09	4.39	2.992	0.409	0.068	18.66
1459	4438.78	26.00	4.69	18.59	4442.07	4.37	3.210	0.423	0.070	18.59
848	4438.01	28.00	3.92	18.52	4442.06	4.36	3.667	0.452	0.075	18.52
595	4437.61	30.00	3.52	18.44	4442.04	4.34	4.234	0.486	0.080	18.44
	4437.59	33.00	3.50	18.31	4442.01	4.31	4.423	0.497	0.123	18.31
	4437.59	36.00	3.50	18.19	4441.99	4.29	4.409	0.496	0.123	18.19
	4437.59	40.00	3.50	18.03	4441.95	4.25	4.378	0.494	0.163	18.03
	4437.59	48.00	3.50	17.70	4441.88	4.18	4.326	0.491	0.325	17.70
	4437.59	60.00	3.50	17.22	4441.78	4.08	4.241	0.486	0.482	17.22
	4437.59	72.00	3.50	16.74	4441.68	3.98	4.141	0.481	0.477	16.74
After depth in channel decreases to 3.5 feet the water surface will be below the 3 inch on face in the basin										
									2.154	

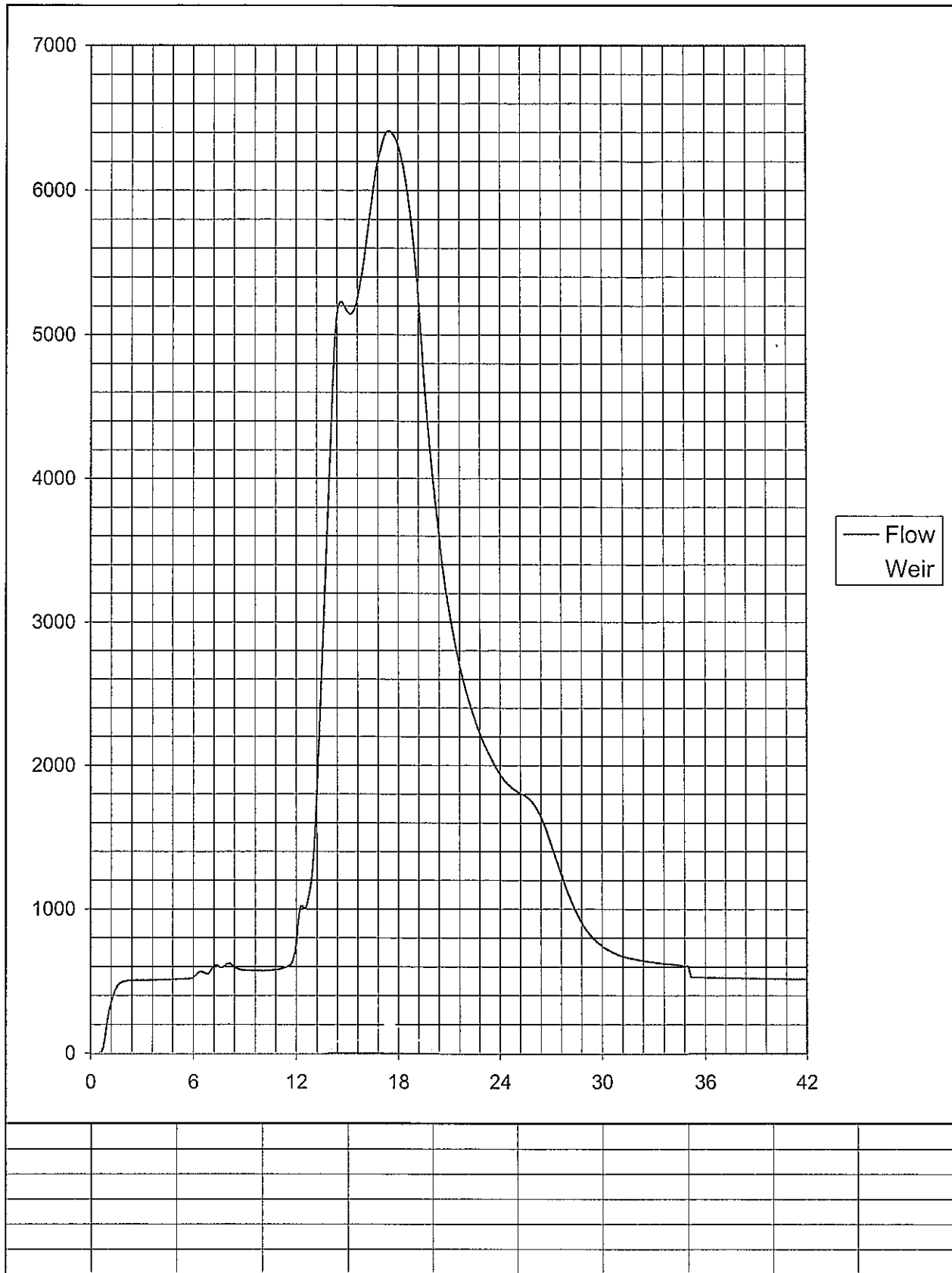
Volume Calculations

		Basin 3 Area and Volume Curves					
		C4	C3	C2	C1	C0	
Depth	Area	Elevation	Area* Calculated	Volume Calculated	Volume	Area	
0	1.0702	4432.14	1.070	0.000	0	0	
0.86	1.5329	4433.00	1.536	1.138	1.302	1.070216	
1.86	1.8425	4434.00	1.829	2.839	2.989	6.85E-01	
2.86	1.9360	4435.00	1.956	4.741	4.878	1.070216	
3.86	2.0340	4436.00	2.021	6.730	6.863	0	
4.86	2.1267	4437.00	2.130	8.797	8.944	0	
		Volume Curve is integrated from Area Curve					
		Flowline of Weir is 4436					6.730 AF
		Flowline of Basin is 4432.14					0 AF
		Net Volume					6.730 AF



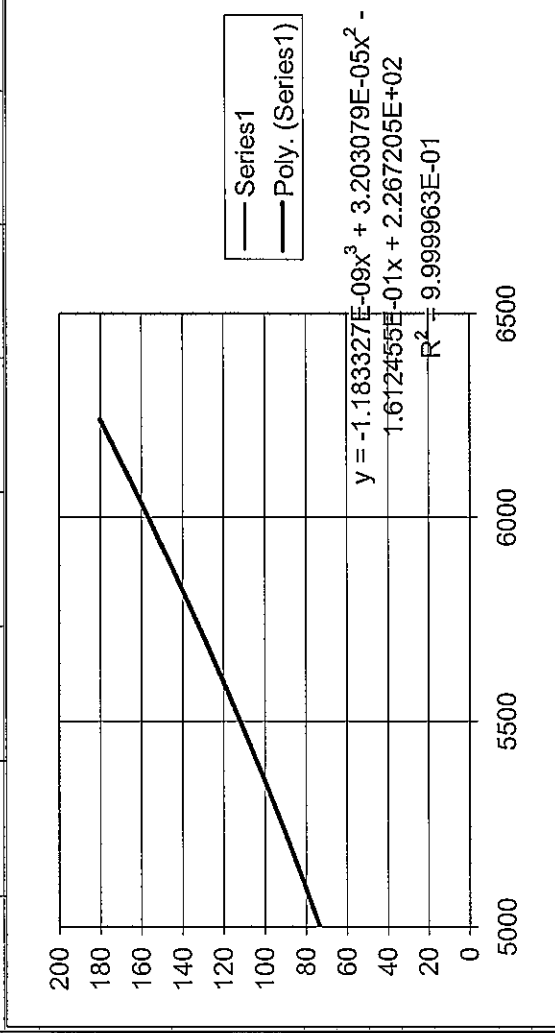
* Areas are calculated from the contour lines on the as-built study map.

5	Node Name			STMBV3	43					
StmBV3	50005	27-Jul	0	0	1	1	420	85.274		
0	0.009	0.047	0.125	0.273	0.93	4.297	17.103	50.39	109.427	
182.209	247.733	298.168	339.409	375.317	406.565	432.524	452.882	468.086	479.041	
486.731	492.103	495.856	498.487	500.34	501.661	502.623	503.338	503.882	504.306	
504.648	504.933	505.18	505.404	505.617	505.803	505.947	506.071	506.196	506.328	
506.465	506.607	506.754	506.906	507.066	507.239	507.443	507.699	508.021	508.393	
508.794	509.206	509.618	510.024	510.423	510.818	511.213	511.617	512.036	512.474	
512.932	513.403	513.868	514.296	514.651	514.91	515.087	515.256	515.629	516.73	
519.488	524.966	533.473	543.914	554.19	562.052	565.816	565.122	560.834	554.81	
549.765	549.101	555.412	568.909	586.428	602.364	611.544	612.335	606.811	599.305	
594.256	594.07	598.647	606.246	614.338	620.168	621.853	618.926	612.391	604.184	
596.316	589.96	585.303	581.992	579.626	577.924	576.698	575.798	575.109	574.561	
574.127	573.782	573.495	573.245	573.03	572.868	572.771	572.721	572.675	572.621	
572.584	572.613	572.745	572.971	573.281	573.706	574.511	575.805	577.408	579.222	
581.186	583.327	585.648	588.122	590.804	593.714	596.9	600.551	604.735	612.331	
628.232	654.124	695.034	762.362	861.012	959.044	1016.7	1022.43	1008.7	1000.87	
1017.19	1057.04	1105.14	1158.74	1242.65	1358.96	1511.44	1698.68	1917.51	2160.65	
2418.34	2672.64	2930.63	3188.19	3443.13	3697.53	3954.57	4213.73	4469.11	4706.7	
4905.08	5052.76	5150.14	5205.09	5227.98	5228.27	5216.2	5198.33	5179.28	5162.22	
5149.47	5143.18	5144.91	5155.41	5174.8	5203.27	5240.69	5287.14	5343.05	5399.95	
5456.75	5521.88	5594.39	5672.89	5751.72	5817.53	5887.78	5961.39	6036.4	6110.8	
6166.9	6211.08	6254.37	6294.56	6330.56	6361.7	6387.56	6403.9	6406.77	6406.69	
6403.09	6395.42	6383.34	6366.48	6344.41	6316.89	6283.78	6245.19	6201.47	6153.1	
6100.49	6044.02	5978.09	5900.16	5818.23	5730.69	5635.5	5531.61	5420.05	5302.38	
5168.68	5020.59	4875.78	4736.72	4605.84	4484.21	4371.87	4262.14	4150.87	4047.4	
3949.33	3855.27	3764.66	3677	3592.17	3507.91	3421.23	3341.37	3267.03	3197.27	
3131.46	3069.13	3010.36	2955.03	2902.63	2852.75	2805.1	2758.61	2710.19	2665.63	
2624	2584.67	2547.21	2511.34	2476.83	2443.5	2411.19	2379.81	2349.49	2320.54	
2292.86	2266.2	2240.42	2215.44	2191.24	2167.76	2144.99	2122.9	2101.5	2080.76	
2060.65	2041.17	2022.31	2004.1	1986.77	1970.39	1954.62	1939.62	1922.53	1907.32	
1894.83	1883.77	1873.76	1864.56	1855.97	1847.86	1840.15	1832.82	1825.87	1819.34	
1813.24	1807.56	1802.21	1796.99	1791.66	1785.94	1779.49	1772.03	1763.36	1753.3	
1741.74	1728.5	1713.59	1697	1678.75	1658.86	1637.39	1614.5	1590.32	1564.98	
1538.57	1511.07	1482.37	1452.58	1422.21	1392	1362.23	1332.86	1303.82	1275.08	
1246.68	1218.68	1191.15	1164.14	1137.67	1111.71	1086.28	1061.6	1037.88	1015.25	
993.656	973.042	953.374	934.632	916.832	899.93	883.902	868.726	854.387	840.87	
828.127	816.123	804.825	794.207	784.229	774.843	766.009	757.693	749.871	742.503	
735.553	728.994	722.801	716.956	711.428	706.195	701.239	696.549	692.118	687.941	
684.017	680.346	676.927	673.738	670.755	667.952	665.306	662.802	660.418	658.141	
655.96	653.868	651.857	649.92	648.05	646.244	644.497	642.804	641.163	639.569	
638.019	636.511	635.043	633.612	632.215	630.852	629.52	628.218	626.945	625.699	
624.48	623.287	622.118	620.972	619.849	618.746	617.665	616.602	615.558	614.531	
613.521	612.527	611.549	610.584	609.633	608.696	607.771	606.857	605.956	605.081	



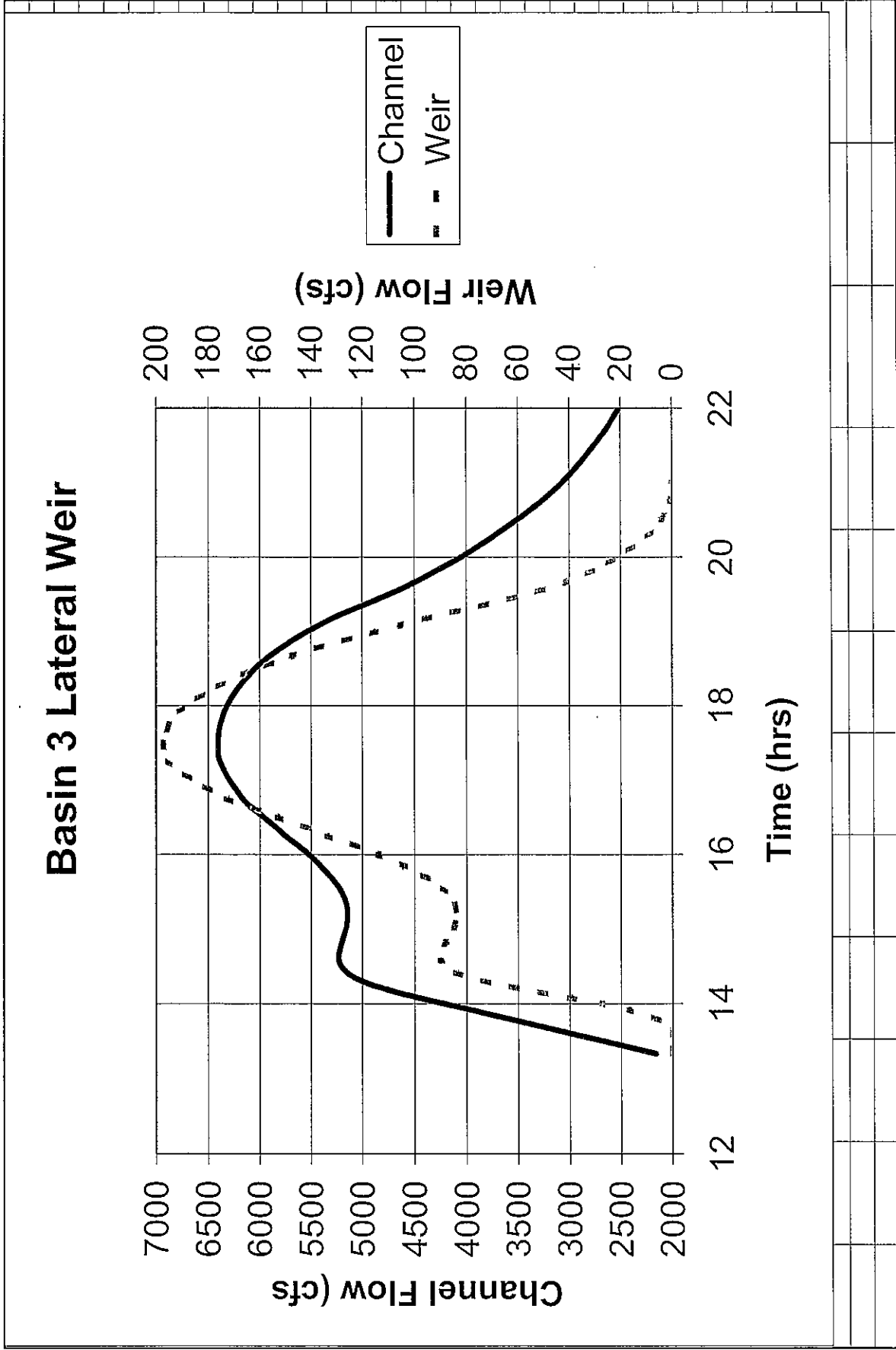
HEC-RAS Plan: LatWeir River: RIVER-1 Reach: Reach-1										
Reach	River Sta	Profile	Q US (cfs)	Q Leaving (cfs)	Q DS (cfs)	Q Weir (cfs)				
Reach-1	49.65	PF 1	6238.02	180.11	6058.47	180.11	Flowline of Weir = 4436.0			
Reach-1	49.65	PF 2	5750.65	133.51	5617.87	133.51	Length of Bottom = 15 ft			
Reach-1	49.65	PF 3	5073.66	78.67	4995.78	78.67	Wing = 25 feet			
Reach-1	49.65	PF 4	4471.02	40.47	4431.2	40.47	Coeff = 3.0			
Reach-1	49.65	PF 5	3840	12.67	3827.44	12.67				
Reach-1	49.65	PF 6	3200	0.01	3200	0.01				

Lateral Weir Flow vs Channel Flow for Basin 3			
C3	C2	C1	C0
-1.18E-09	3.203079E-05	-1.612455E-01	2.267205E+02
Channel	HEC-RAS	Curve	
6238	180.11	180.04	
5751	133.51	133.67	
5074	78.67	78.60	
4471	40.47	40.32	
3840	12.67	12.85	
3200	0.01	-0.05	
3206			



Volume Removed.		
Volume into Basin	61.34	

13.33	2160.65	0.00	16.25	5751.72	133.77	19.17	5302.38	95.88
13.42	2418.34	0.00	16.33	5817.53	139.73	19.25	5168.68	85.61
13.50	2672.64	0.00	16.42	5887.78	146.20	19.33	5020.59	74.80
13.58	2930.63	0.00	16.50	5961.39	153.09	19.42	4875.78	64.84
13.67	3188.19	0.00	16.58	6036.40	160.24	19.50	4736.72	55.85
13.75	3443.13	2.96	16.67	6110.80	167.45	19.58	4605.84	47.92
13.83	3697.53	8.61	16.75	6166.90	172.96	19.67	4484.21	41.04
13.92	3954.57	16.80	16.83	6211.08	177.35	19.75	4371.87	35.11
14.00	4213.73	27.47	16.92	6254.37	181.68	19.83	4262.14	29.72
14.08	4469.11	40.22	17.00	6294.56	185.74	19.92	4150.87	24.66
14.17	4706.70	53.98	17.08	6330.56	189.40	20.00	4047.40	20.35
14.25	4905.08	66.80	17.17	6361.70	192.58	20.08	3949.33	16.61
14.33	5052.76	77.10	17.25	6387.56	195.24	20.17	3855.27	13.35
14.42	5150.14	84.22	17.33	6403.90	196.93	20.25	3764.66	10.51
14.50	5205.09	88.36	17.42	6406.77	197.23	20.33	3677.00	8.06
14.58	5227.98	90.10	17.50	6406.69	197.22	20.42	3592.17	5.96
14.67	5228.27	90.13	17.58	6403.09	196.85	20.50	3507.91	4.16
14.75	5216.20	89.20	17.67	6395.42	196.06	20.58	3421.23	2.59
14.83	5198.33	87.84	17.75	6383.34	194.81	20.67	3341.37	1.41
14.92	5179.28	86.40	17.83	6366.48	193.07	20.75	3267.03	0.54
15.00	5162.22	85.12	17.92	6344.41	190.81	20.83	3197.27	0.00
15.08	5149.47	84.17	18.00	6316.89	188.00	20.92	3131.46	0.00
15.17	5143.18	83.70	18.08	6283.78	184.65	21.00	3069.13	0.00
15.25	5144.91	83.83	18.17	6245.19	180.76	21.08	3010.36	0.00
15.33	5155.41	84.61	18.25	6201.47	176.39	21.17	2955.03	0.00
15.42	5174.80	86.07	18.33	6153.10	171.60	21.25	2902.63	0.00
15.50	5203.27	88.22	18.42	6100.49	166.44	21.33	2852.75	0.00
15.58	5240.69	91.08	18.50	6044.02	160.97	21.42	2805.10	0.00
15.67	5287.14	94.69	18.58	5978.09	154.67	21.50	2758.61	0.00
15.75	5343.05	99.10	18.67	5900.16	147.35	21.58	2710.19	0.00
15.83	5399.95	103.68	18.75	5818.23	139.79	21.67	2665.63	0.00
15.92	5456.75	108.33	18.83	5730.69	131.89	21.75	2624.00	0.00
16.00	5521.88	113.76	18.92	5635.50	123.49	21.83	2584.67	0.00
16.08	5594.39	119.94	19.00	5531.61	114.58	21.92	2547.21	0.00
16.17	5672.89	126.77	19.08	5420.05	105.31	22.00	2511.34	0.00



Depth vs Channel Flow

HEC-RAS Plan: Depth River: Steamboat Reach: Bella Vista										
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	Ch El (ft)	W.S. Elev (ft)	Depth (ft)			
Bella Vista	46	PF 1	6058	4428.65	4428.65	4436.98	8.33			
Bella Vista	46	PF 2	5617.87	4428.65	4428.65	4436.75	8.10			
Bella Vista	46	PF 3	4995.78	4428.65	4428.65	4436.41	7.76			
Bella Vista	46	PF 4	4431.2	4428.65	4428.65	4436.09	7.44			
Bella Vista	46	PF 5	3827.44	4428.65	4428.65	4435.73	7.08			
Bella Vista	46	PF 6	3200	4428.65	4428.65	4435.32	6.67			
Bella Vista	46	PF 7	2560	4428.65	4428.65	4434.88	6.23			
Bella Vista	46	PF 8	1920	4428.65	4428.65	4434.38	5.73			
Bella Vista	46	PF 9	1280	4428.65	4428.65	4433.79	5.14			
Bella Vista	46	PF 10	640	4428.65	4428.65	4433	4.35			
Bella Vista	46	PF 11	405	4428.65	4428.65	4432.55	3.90			

Equation for Depth vs Channel Flow at Basin 3 Outlet					
C3	C2	C1	C0		
0	-7.159131E-08	1.204348E-03	3.582566E+00		
Channel	HEC-RAS	Curve	WS Elev		
6058	8.33	8.25	4436.90		
5618	8.10	8.09	4436.74		
4996	7.76	7.81	4436.46		
4431	7.44	7.51	4436.16		
3827	7.08	7.14	4435.79		
3200	6.67	6.70	4435.35		
2560	6.23	6.20	4434.85		
1920	5.73	5.63	4434.28		
1280	5.14	5.01	4433.66		
640	4.35	4.32	4432.97		
405	3.90	4.06	4432.71		
4154	0.00	7.35	4436.00	FL of Weir	

Depth vs Channel Flow

$y = -7.159131E-08x^2 + 1.20434766E-03x + 3.58256618E+00$

— Depth
- - Poly. (Depth)

Outflow Calculations

Channel W.S.	Time Hours	Channel Depth	Storage Bas Vol by depth	Basin W.S.	Basin Depth	Average Delta WS	Outflow 3	Outflow Volume	Storage Volume by outflow
4434.30	24.00	5.65	6.73	4436.00	3.86				6.73
4434.19	25.00	5.54	6.70	4435.98	3.84	1.750	0.312	0.026	6.70
4433.83	27.00	5.18	6.65	4435.96	3.82	1.964	0.331	0.055	6.65
4433.22	29.00	4.57	6.59	4435.93	3.79	2.417	0.367	0.061	6.59
4432.99	32.00	4.34	6.49	4435.88	3.74	2.801	0.395	0.098	6.49
4432.95	34.00	4.30	6.42	4435.85	3.71	2.898	0.402	0.066	6.42
4432.94	35.00	4.29	6.39	4435.83	3.69	2.899	0.402	0.033	6.39
4432.15	40.00	3.50	6.21	4435.74	3.60	3.245	0.426	0.176	6.21
4432.15	48.00	3.50	5.92	4435.60	3.46	3.521	0.443	0.293	5.92
4432.15	60.00	3.50	5.49	4435.38	3.24	3.340	0.432	0.428	5.49
4432.15	72.00	3.50	5.08	4435.17	3.03	3.128	0.418	0.414	5.08
4432.15	48.00	3.50	5.92	4435.60	3.46	3.235	0.425	-0.843	5.92
4432.15	60.00	3.50	5.49	4435.38	3.24	3.340	0.432	0.428	5.49
4432.15	72.00	3.50	5.08	4435.17	3.03	3.128	0.418	0.414	5.08
								1.650	
After depth in channel decreases to 3.5 feet the water surface will be below the 3-inch orifice in the basin									

As-Built UPDATE for Damonte Ranch/Double Diamond Ranch Regional Flood Control Improvements

1. Rating Table for the Regional Detention Basin (HEC-1 Model Node BAS1)

For the range of flows used in the Regional Detention Basin rating table (HEC-1 model node BAS1), the basin outlet culverts are under outlet control. When a culvert functions under outlet control (also called tailwater control or exit control), the headwater elevation for a given discharge is a function of the downstream condition (the tailwater elevation). For each flow, the headwater elevation is found by computing the losses through the culvert and adding them to the downstream tailwater energy grade elevation (see the E.G. US output in the culver table). These losses are the sum of the entrance loss, the exit loss, and the friction loss through the culvert barrel.

The analysis of culverts was made based on CON/SPAN shape as well as Box shape through out the length. Hydraulic Analysis for the culverts was performed using HEC-RAS version 3.1.3. The culvert data are updated based on document from Odyssey (see the attachment) and field measurements. The upstream and down stream HEC-RAS cross sections were obtained from the as built drawing (see Figure B-1) obtained from Odyssey Engineering. The HEC-RAS output is attached. The result is summarized in Table B-1. It indicates that change in head water (HW) elevation is insignificant of the culvert shape. Therefore, the rating table based on box culvert is used to update HEC-1 model.

Table B-1 Outflow Rating Table for HEC-1 Model Node BAS 1

CON/SPAN HW Elev. (ft)		BOX HW Elev. (ft)	Outflow Discharge (cfs)		
In Original HEC-1 Model	New	New	Culverts	36" Low Flow Pipe	Total
4477.6	4477.64	4477.64	500	15	515
4478.5	4478.54	4478.54	1000	21	1021
4479.3	4479.28	4479.28	1500	27	1527
4480.1	4479.95	4479.95	2000	31	2031
4480.7	4480.59	4480.59	2500	37	2537
4481.3	4481.24	4481.25	3000	59	3059
4481.9	4481.88	4481.87	3500	61	3561
4482.6	4482.44	4482.43	4000	63	4063

2. **Rating Table for Trapezoidal Weir from wetlands to Pond 4
(HEC-1 Model Node RT DT2)**

As-Build Dimensions for Trapezoidal Weir

Crest Elevation: 4454 ft

Crest Length, L= 30 ft and varies with side slopes: 3H:1V

Crest Width, W= 5ft

Weir Head, H=Water Surface Elev. – Crest Elevation

Weir Coefficient: C=2.80

The discharge over the weir is calculated using $Q=CL_{ave}H^{1.5}$, where $L_{ave} = 0.5 * (L_{crest} + L_{surface})$. See the attached sheet for detail calculation. The result is summarized in Table B-2.

Table B-2 Outflow Rating Table for HEC-1 Model Node RT DT2

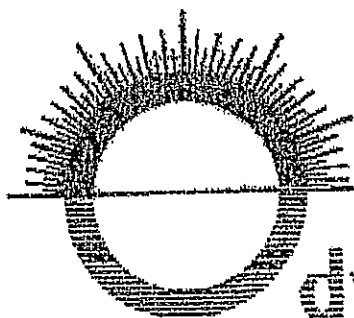
Elevation (ft)	Outflow Discharge (cfs)		
	12" Culvert	Weir	Total
4453	3	0	3
4454	7.5	0	8
4455	17.5	92	110
4456	Negligible	285	285
4457	Negligible	567	567
4458	Negligible	941	941
4459	Negligible	1409	1409
4460	Negligible	1975	1975
4461	Negligible	2645	2645
4462	Negligible	3421	3421

3. **Result update for Post Project modeling**

The HEC-1 rating tables for BAS 1 and RT DT2 were updated using Table B-1 and Table B-2. The new HEC-1 model output (0243AB.out) is attached in Appendix C. A summary of flow rates and other data at key points in the HEC-1 model are shown in Table B-3.

Location	Model Point	Qin, cfs	Qout, cfs	W.S. Elev., ft.	Freeboard, ft.
Diversion Structure	DIVSTR	7992	7992	4488.0	1.0
Steamboat @ North Property Line	OUTDN	n/a	4150	n/a	n/a
Regional Detention Basin	BAS 1	3838	3410 (3238)	4481.68 (4481.51)	4.32 (3.49)
Wetlands Detention	RS DT2	3410 (3276)	2806 (2689)	4461.21 (4461.3)	3.79 (typical) (3.70)
Pond 4	POND4	2812 (2695)	2652 (2579)	4456.36 (4456.20)	1.64 (1.80)
Downstream End of Project	PT04	n/a	6424 (6362)	n/a	n/a

(.) previous results in LOMR (FEMA Case No. 05-09-0105P)



895 Roberta Lane, Suite 104, Sparks, NV 89431
(775) 359-3303 Fax (775) 359-3329

odyssey ENGINEERING
INCORPORATED

FAX TRANSMITTAL

Date: 12/12/06 Destination Fax Number: 775-324-2311

To: David Westhoff

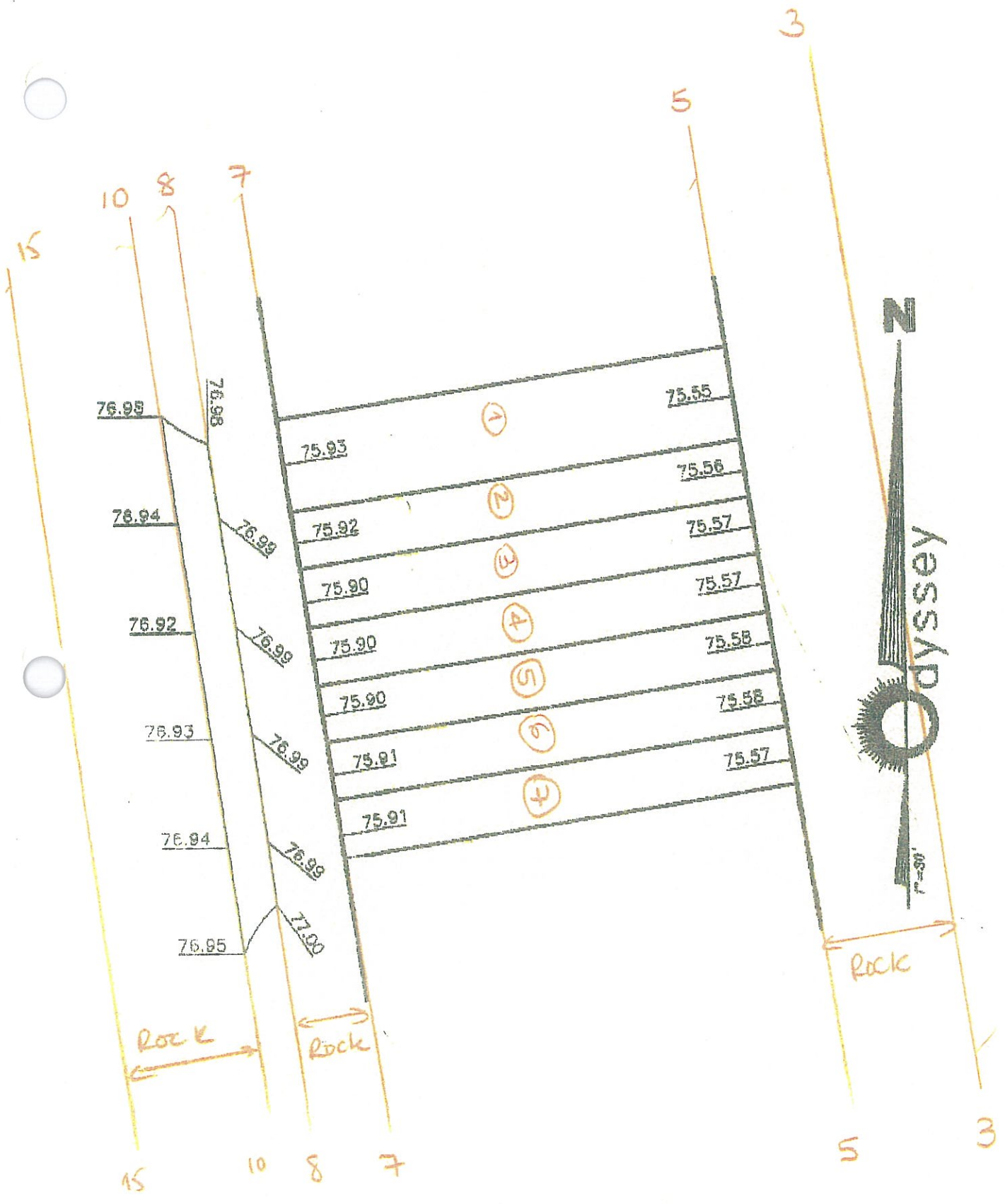
From: Sonny Bradley

Odyssey Job Number: _____

Subject: Damonte ranch as-built elevations

Remarks: _____

Total Number of Pages Including Cover Page: 2



HEC-RAS Version 3.1.3 May 2005
 U.S. Army Corp of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

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X   X XXXXXX XXXX   XXXX   XX   XXXX
X   X X   X   X   X   X X   X   X
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PROJECT DATA
 Project Title: Culvert out of Regional DB
 Project File : RDB.prj
 Run Date and Time: 1/2/2007 2:16:30 PM

Project in English units

PLAN DATA

Plan Title: Box Culvert(detailed data)
 Plan File : j:\0432 Bella Vista -Centex Homes\hd\ras\CLOMR DPH5+BVPH1\Rating Table Update\RDB.p04

Geometry Title: Box Culvert (detailed data)
 Geometry File : j:\0432 Bella Vista -Centex Homes\hd\ras\CLOMR DPH5+BVPH1\Rating Table Update\RDB.g03

Flow Title : Box Culvert(detailed data)
 Flow File : j:\0432 Bella Vista -Centex Homes\hd\ras\CLOMR DPH5+BVPH1\Rating Table Update\RDB.f03

Plan Summary Information:

Number of: Cross Sections = 8 Multiple Openings = 0
 Culverts = 1 Inline Structures = 0
 Bridges = 0 Lateral Structures = 0

Computational Information

Water surface calculation tolerance = 0.01
 Critical depth calculation tolerance = 0.01
 Maximum number of iterations = 20
 Maximum difference tolerance = 0.3
 Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary
 Conveyance Calculation Method: At breaks in n values only
 Friction Slope Method: Average Conveyance
 Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Box Culvert(detailed data)
 Flow File : j:\0432 Bella Vista -Centex Homes\hd\ras\CLOMR DPH5+BVPH1\Rating Table Update\RDB.f03

Flow Data (cfs)

River	Reach	RS	PF 1	PF 2	PF 3	PF 4	PF 5
PF 6	PF 7	PF 8					
Test	Culvert	20	500	1000	1500	2000	2500
3000	3500	4000					
Regional DetentiBasin Outlet		20	500	1000	1500	2000	2500
3000	3500	4000					
Regional DBasin Outlet Culverts		20	500	1000	1500	2000	2500
3000	3500	4000					

River	Reach	RS	PF 9	PF 10
Test	Culvert	20	5000	6000
Regional DetentiBasin Outlet		20	5000	6000
Regional DBasin Outlet Culverts		20	5000	6000

Boundary Conditions

River	Reach	Profile	Upstream	Downstream
Regional DBasin Outlet Culverts		PF 1		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 2		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 3		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 4		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 5		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 6		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 7		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 8		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 9		Normal S = 0.008333
Regional DBasin Outlet Culverts		PF 10		Normal S = 0.008333

SUMMARY OF MANNING'S N VALUES

River: Regional DBasin

Reach	River Sta.	n1	n2	n3

Outlet Culverts	20	.035	.035	.035
Outlet Culverts	15	.045	.045	.045
Outlet Culverts	10	.013	.013	.013
Outlet Culverts	8	.013	.013	.013
Outlet Culverts	7	.013	.013	.013
Outlet Culverts	5.5	Culvert		
Outlet Culverts	5	.045	.045	.045
Outlet Culverts	3	.035	.035	.035
Outlet Culverts	2	.035	.035	.035

SUMMARY OF REACH LENGTHS

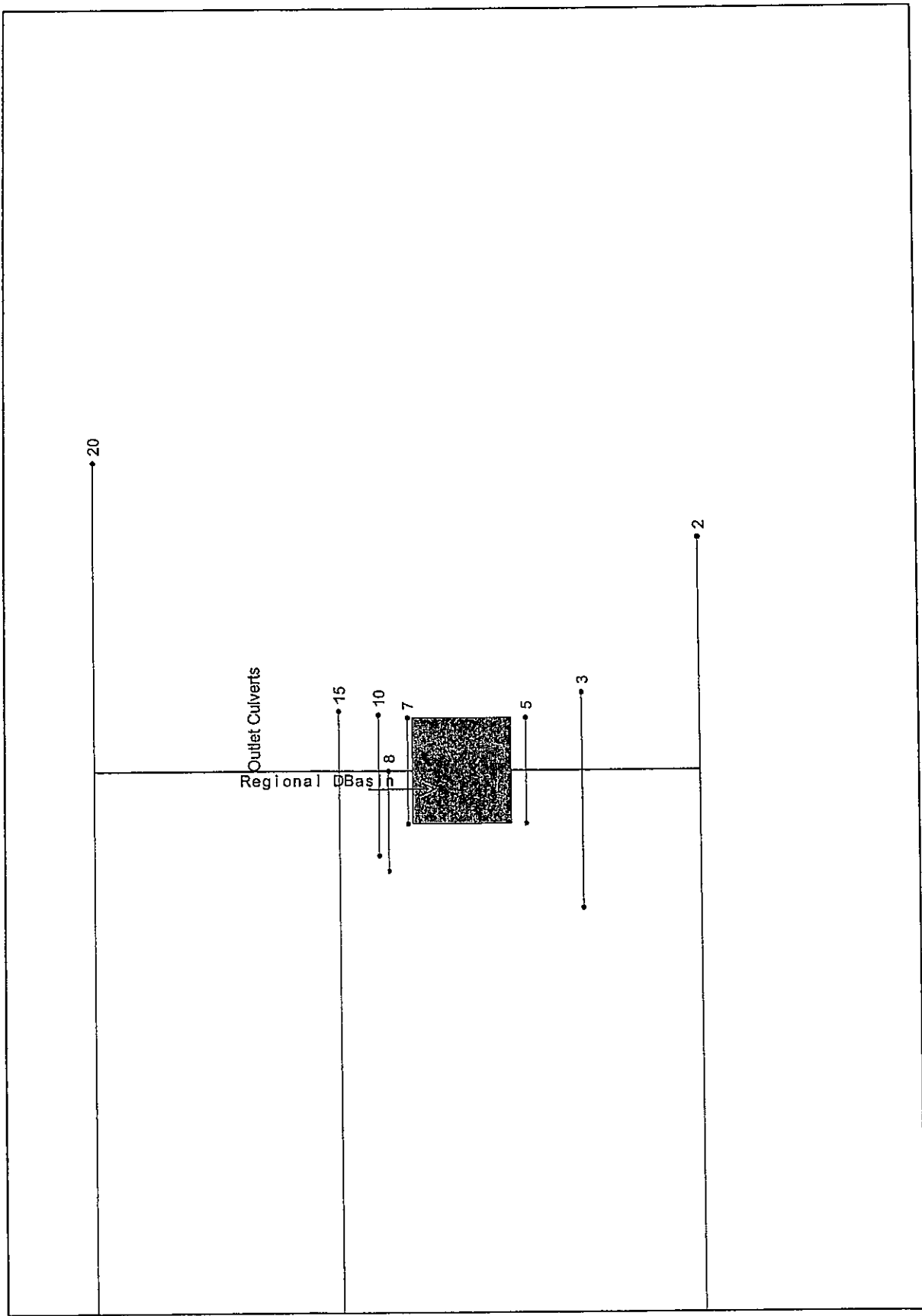
River: Regional DBasin

Reach	River Sta.	Left	Channel	Right
Outlet Culverts	20	248	248	248
Outlet Culverts	15	40	40	40
Outlet Culverts	10	10	10	10
Outlet Culverts	8	20	20	20
Outlet Culverts	7	120	120	120
Outlet Culverts	5.5	Culvert		
Outlet Culverts	5	72	58	42
Outlet Culverts	3	120	120	120
Outlet Culverts	2	0	0	0

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Regional DBasin

Reach	River Sta.	Contr.	Expan.
Outlet Culverts	20	.1	.3
Outlet Culverts	15	.3	.5
Outlet Culverts	10	.1	.3
Outlet Culverts	8	.1	.3
Outlet Culverts	7	.1	.3
Outlet Culverts	5.5	Culvert	
Outlet Culverts	5	.1	.3
Outlet Culverts	3	.3	.5
Outlet Culverts	2	.1	.3



HEC-RAS Plan: Detailed River: Regional DBasin Reach: Outlet Culverts

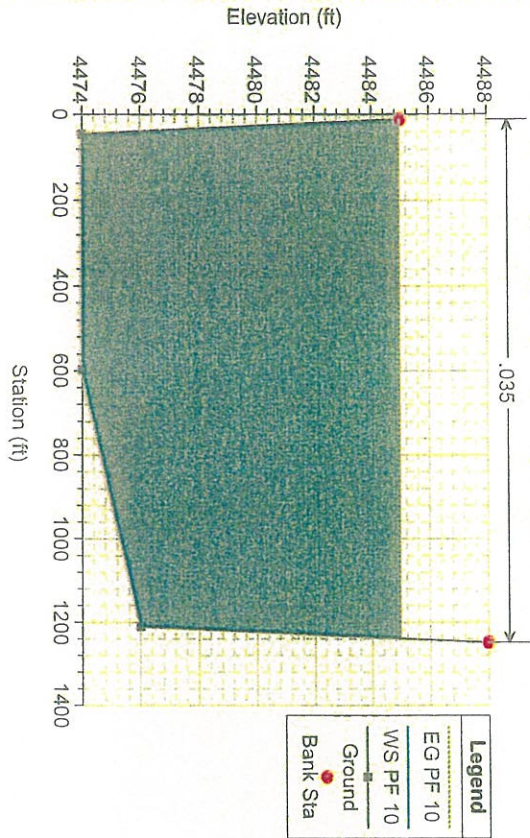
Station	Water Surface Elevation (ft)	Channel Bottom Elevation (ft)	Flow Area (sq ft)	Velocity (ft/s)	Discharge (cfs)	Water Surface Elevation (ft)	Channel Bottom Elevation (ft)	Flow Area (sq ft)	Velocity (ft/s)	Discharge (cfs)	Water Surface Elevation (ft)	Channel Bottom Elevation (ft)	Flow Area (sq ft)	Velocity (ft/s)	Discharge (cfs)	
4477.64	4477.64	4477.50	4477.48	4477.56	4477.66	4477.48	4477.50	4477.56	4477.66	73.01	4485.01	4477.50	4477.48	4477.56	3.70	2.89
4477.64	4477.64	4477.50	4477.46	4477.65	4477.65	4477.46	4477.50	4477.65	4477.65	72.18	4485.01	4477.50	4477.46	4477.65	3.61	2.87
4477.64	4477.64	4477.50	4477.42	4477.64	4477.64	4477.42	4477.50	4477.64	4477.64	71.24	4485.01	4477.50	4477.42	4477.64	3.50	2.85
4477.64	4477.64	4477.50	4477.42	4477.64	4477.64	4477.42	4477.50	4477.64	4477.64	71.24	4485.01	4477.50	4477.42	4477.64	3.50	2.85
4477.64	4477.64	4477.50	4477.41	4477.63	4477.63	4477.41	4477.50	4477.63	4477.63	70.40	4485.01	4477.50	4477.41	4477.63	3.45	2.83
4477.64	4477.64	4477.50	4477.42	4477.64	4477.64	4477.42	4477.50	4477.64	4477.64	70.58	4485.01	4477.50	4477.42	4477.64	3.49	2.84
4477.64	4477.64	4477.50	4477.44	4477.64	4477.64	4477.44	4477.50	4477.64	4477.64	71.36	4485.01	4477.50	4477.44	4477.64	3.54	2.85
4478.54	4478.54	4478.30	4478.37	4478.56	4478.56	4478.37	4478.30	4478.56	4478.56	144.26	4485.01	4478.30	4478.37	4478.56	5.09	4.23
4478.54	4478.54	4478.30	4478.35	4478.55	4478.55	4478.35	4478.30	4478.55	4478.55	143.67	4485.01	4478.30	4478.35	4478.55	5.02	4.23
4478.54	4478.54	4478.30	4478.32	4478.54	4478.54	4478.32	4478.30	4478.54	4478.54	142.74	4485.01	4478.30	4478.32	4478.54	4.91	4.22
4478.54	4478.54	4478.30	4478.32	4478.54	4478.54	4478.32	4478.30	4478.54	4478.54	142.74	4485.01	4478.30	4478.32	4478.54	4.91	4.22
4478.54	4478.54	4478.30	4478.31	4478.53	4478.53	4478.31	4478.30	4478.53	4478.53	141.79	4485.01	4478.30	4478.31	4478.53	4.86	4.21
4478.54	4478.54	4478.30	4478.32	4478.54	4478.54	4478.32	4478.30	4478.54	4478.54	141.96	4485.01	4478.30	4478.32	4478.54	4.90	4.22
4478.54	4478.54	4478.30	4478.33	4478.54	4478.54	4478.33	4478.30	4478.54	4478.54	142.84	4485.01	4478.30	4478.33	4478.54	4.94	4.23
4479.28	4479.28	4478.94	4479.12	4479.30	4479.30	4479.12	4478.94	4479.30	4479.30	215.49	4485.01	4478.94	4479.12	4479.30	6.32	5.38
4479.28	4479.28	4478.94	4479.10	4479.29	4479.29	4479.10	4478.94	4479.29	4479.29	215.05	4485.01	4478.94	4479.10	4479.29	6.24	5.39
4479.28	4479.28	4478.94	4479.08	4479.27	4479.27	4479.08	4478.94	4479.27	4479.27	214.28	4485.01	4478.94	4479.08	4479.27	6.12	5.39
4479.28	4479.28	4478.94	4479.08	4479.27	4479.27	4479.08	4478.94	4479.27	4479.27	214.28	4485.01	4478.94	4479.08	4479.27	6.12	5.39
4479.28	4479.28	4478.94	4479.08	4479.27	4479.27	4479.08	4478.94	4479.27	4479.27	213.24	4485.01	4478.94	4479.08	4479.27	6.07	5.38
4479.28	4479.28	4478.94	4479.09	4479.28	4479.28	4479.09	4478.94	4479.28	4479.28	214.30	4485.01	4478.94	4479.09	4479.28	6.16	5.39
4479.95	4479.95	4479.53	4479.78	4479.96	4479.96	4479.78	4479.53	4479.96	4479.96	285.65	4485.01	4479.53	4479.78	4479.96	7.45	6.41
4479.95	4479.95	4479.53	4479.77	4479.96	4479.96	4479.77	4479.53	4479.96	4479.96	286.14	4485.01	4479.53	4479.77	4479.96	7.37	6.44
4479.95	4479.95	4479.53	4479.75	4479.94	4479.94	4479.75	4479.53	4479.94	4479.94	286.08	4485.01	4479.53	4479.75	4479.94	7.24	6.46
4479.95	4479.95	4479.53	4479.75	4479.94	4479.94	4479.75	4479.53	4479.94	4479.94	286.08	4485.01	4479.53	4479.75	4479.94	7.24	6.46
4479.95	4479.95	4479.53	4479.74	4479.94	4479.94	4479.74	4479.53	4479.94	4479.94	285.19	4485.01	4479.53	4479.74	4479.94	7.19	6.46
4479.95	4479.95	4479.53	4479.76	4479.95	4479.95	4479.76	4479.53	4479.95	4479.95	285.04	4485.01	4479.53	4479.76	4479.95	7.24	6.46
4479.95	4479.95	4479.53	4479.76	4479.95	4479.95	4479.76	4479.53	4479.95	4479.95	285.83	4485.01	4479.53	4479.76	4479.95	7.29	6.45
4480.59	4480.59	4480.10	4480.37	4480.60	4480.60	4480.37	4480.10	4480.60	4480.60	354.61	4485.01	4480.10	4480.37	4480.60	8.57	7.37
4480.59	4480.59	4480.10	4480.38	4480.60	4480.60	4480.38	4480.10	4480.60	4480.60	356.87	4485.01	4480.10	4480.38	4480.60	8.49	7.44
4480.59	4480.59	4480.10	4480.37	4480.59	4480.59	4480.37	4480.10	4480.59	4480.59	356.23	4485.01	4480.10	4480.37	4480.59	8.33	7.49
4480.59	4480.59	4480.10	4480.37	4480.59	4480.59	4480.37	4480.10	4480.59	4480.59	358.23	4485.01	4480.10	4480.37	4480.59	8.33	7.49
4480.59	4480.59	4480.10	4480.37	4480.58	4480.58	4480.37	4480.10	4480.58	4480.58	357.64	4485.01	4480.10	4480.37	4480.58	8.27	7.50
4480.59	4480.59	4480.10	4480.37	4480.59	4480.59	4480.37	4480.10	4480.59	4480.59	356.99	4485.01	4480.10	4480.37	4480.59	8.33	7.48
4481.25	4481.25	4480.71	4480.91	4481.25	4481.25	4480.91	4480.71	4481.25	4481.25	357.43	4485.01	4480.71	4480.91	4481.25	8.38	7.47
4481.25	4481.25	4480.71	4480.93	4481.25	4481.25	4480.93	4480.71	4481.25	4481.25	357.43	4485.01	4480.71	4480.93	4481.25	8.38	7.47
4481.25	4481.25	4480.71	4480.96	4481.25	4481.25	4480.96	4480.71	4481.25	4481.25	424.53	4485.01	4480.71	4480.96	4481.25	9.90	8.30
4481.25	4481.25	4480.71	4480.96	4481.25	4481.25	4480.96	4480.71	4481.25	4481.25	431.46	4485.01	4480.71	4480.96	4481.25	9.76	8.38
4481.25	4481.25	4480.71	4480.96	4481.24	4481.24	4480.96	4480.71	4481.24	4481.24	431.42	4485.01	4480.71	4480.96	4481.24	9.48	8.55
4481.25	4481.25	4480.71	4480.97	4481.24	4481.24	4480.97	4480.71	4481.24	4481.24	432.21	4485.01	4480.71	4480.97	4481.24	9.48	8.55
4481.25	4481.25	4480.71	4480.96	4481.24	4481.24	4480.96	4480.71	4481.24	4481.24	430.08	4485.01	4480.71	4480.96	4481.24	9.41	8.55
4481.25	4481.25	4480.71	4480.96	4481.25	4481.25	4480.96	4480.71	4481.25	4481.25	429.00	4485.01	4480.71	4480.96	4481.25	9.56	8.50

HEC-RAS Plant Detailed River: Regional DBasin Reach: Outlet Culverts (Continued)

Structure ID	Structure Name	Structure Type	Structure Material	Structure Length (ft)	Structure Height (ft)	Structure Width (ft)	Structure Depth (ft)	Structure Slope (ft/ft)	Structure Inlet Elevation (ft)	Structure Outlet Elevation (ft)	Structure Inlet Velocity (ft/s)	Structure Outlet Velocity (ft/s)	Structure Inlet Froude Number	Structure Outlet Froude Number	Structure Inlet Reynolds Number	Structure Outlet Reynolds Number	Structure Inlet Manning's n	Structure Outlet Manning's n	Structure Inlet Headloss (ft)	Structure Outlet Headloss (ft)	Structure Inlet Energy Loss (ft)	Structure Outlet Energy Loss (ft)	Structure Inlet Total Head (ft)	Structure Outlet Total Head (ft)
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.50	4481.87	4481.87	0.00	4481.87	4485.01	497.18	1.95	10.46	9.38										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.50	4481.87	4481.87	0.00	4481.87	4485.01	498.38	1.95	10.47	9.43										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.49	4481.87	4481.87	0.00	4481.87	4485.01	500.90	1.95	10.48	9.50										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.49	4481.87	4481.87	0.00	4481.87	4485.01	500.90	1.95	10.48	9.50										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.51	4481.87	4481.87	0.00	4481.87	4485.01	503.61	1.95	10.37	9.58										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.49	4481.87	4481.87	0.00	4481.87	4485.01	499.61	1.95	10.47	9.50										
4481.87	Outlet Culvert	55	Concrete	4481.29	4481.49	4481.87	4481.87	0.00	4481.87	4485.01	499.41	1.95	10.47	9.47										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.02	4482.43	4482.43	0.00	4482.43	4485.01	569.56	2.30	10.94	10.32										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.02	4482.43	4482.43	0.00	4482.43	4485.01	570.49	2.30	10.95	10.36										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.01	4482.43	4482.43	0.00	4482.43	4485.01	572.23	2.30	10.96	10.42										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.01	4482.43	4482.43	0.00	4482.43	4485.01	572.23	2.30	10.96	10.42										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.02	4482.43	4482.43	0.00	4482.43	4485.01	573.39	2.30	10.90	10.47										
4482.43	Outlet Culvert	55	Concrete	4481.79	4482.01	4482.43	4482.43	0.00	4482.43	4485.01	570.89	2.30	10.95	10.42										
4483.47	Outlet Culvert	55	Concrete	4482.73	4483.00	4483.47	4483.47	0.00	4483.47	4485.01	711.70	3.03	11.79	12.36										
4483.47	Outlet Culvert	55	Concrete	4482.73	4483.00	4483.47	4483.47	0.00	4483.47	4485.01	712.62	3.03	11.79	12.11										
4483.47	Outlet Culvert	55	Concrete	4482.73	4482.99	4483.47	4483.47	0.00	4483.47	4485.01	715.25	3.03	11.76	11.80										
4483.47	Outlet Culvert	55	Concrete	4482.73	4482.99	4483.47	4483.47	0.00	4483.47	4485.01	715.25	3.03	11.76	11.80										
4483.47	Outlet Culvert	55	Concrete	4482.73	4482.99	4483.47	4483.47	0.00	4483.47	4485.01	718.13	3.03	11.65	11.82										
4483.47	Outlet Culvert	55	Concrete	4482.73	4482.99	4483.47	4483.47	0.00	4483.47	4485.01	713.76	3.03	11.75	11.80										
4483.47	Outlet Culvert	55	Concrete	4482.73	4482.99	4483.47	4483.47	0.00	4483.47	4485.01	713.27	3.03	11.79	11.89										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.00	4484.54	4484.54	0.00	4484.54	4485.01	867.84	3.52	12.59	13.05										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.44	4484.44	0.00	4484.44	4485.01	853.92	3.52	12.52	12.77										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.41	4484.41	0.00	4484.41	4485.01	856.09	3.52	12.38	12.53										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.41	4484.41	0.00	4484.41	4485.01	856.09	3.52	12.38	12.53										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.39	4484.39	0.00	4484.39	4485.01	856.09	3.52	12.25	12.53										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.41	4484.41	0.00	4484.41	4485.01	854.98	3.52	12.38	12.53										
4484.54	Outlet Culvert	55	Concrete	4483.72	4484.54	4484.44	4484.44	0.00	4484.44	4485.01	854.98	3.52	12.51	12.53										

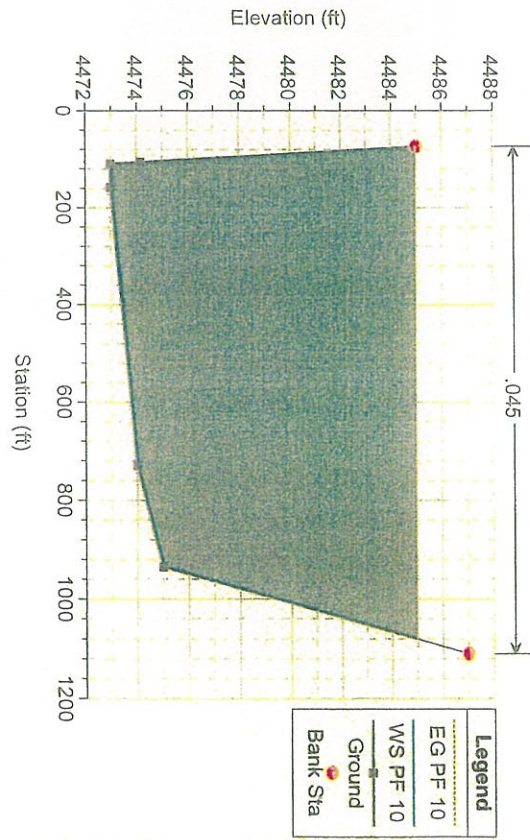
Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

River = Regional DBasin Reach = Outlet Culverts RS = 20



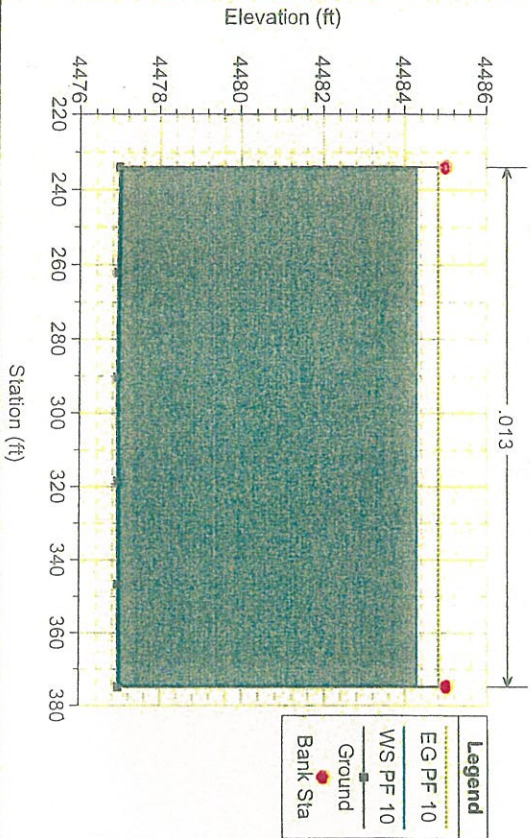
Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

River = Regional DBasin Reach = Outlet Culverts RS = 15



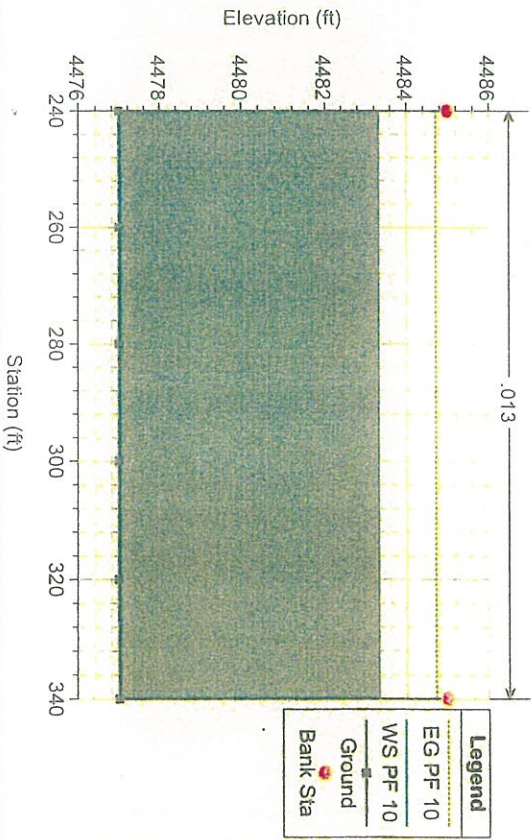
Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

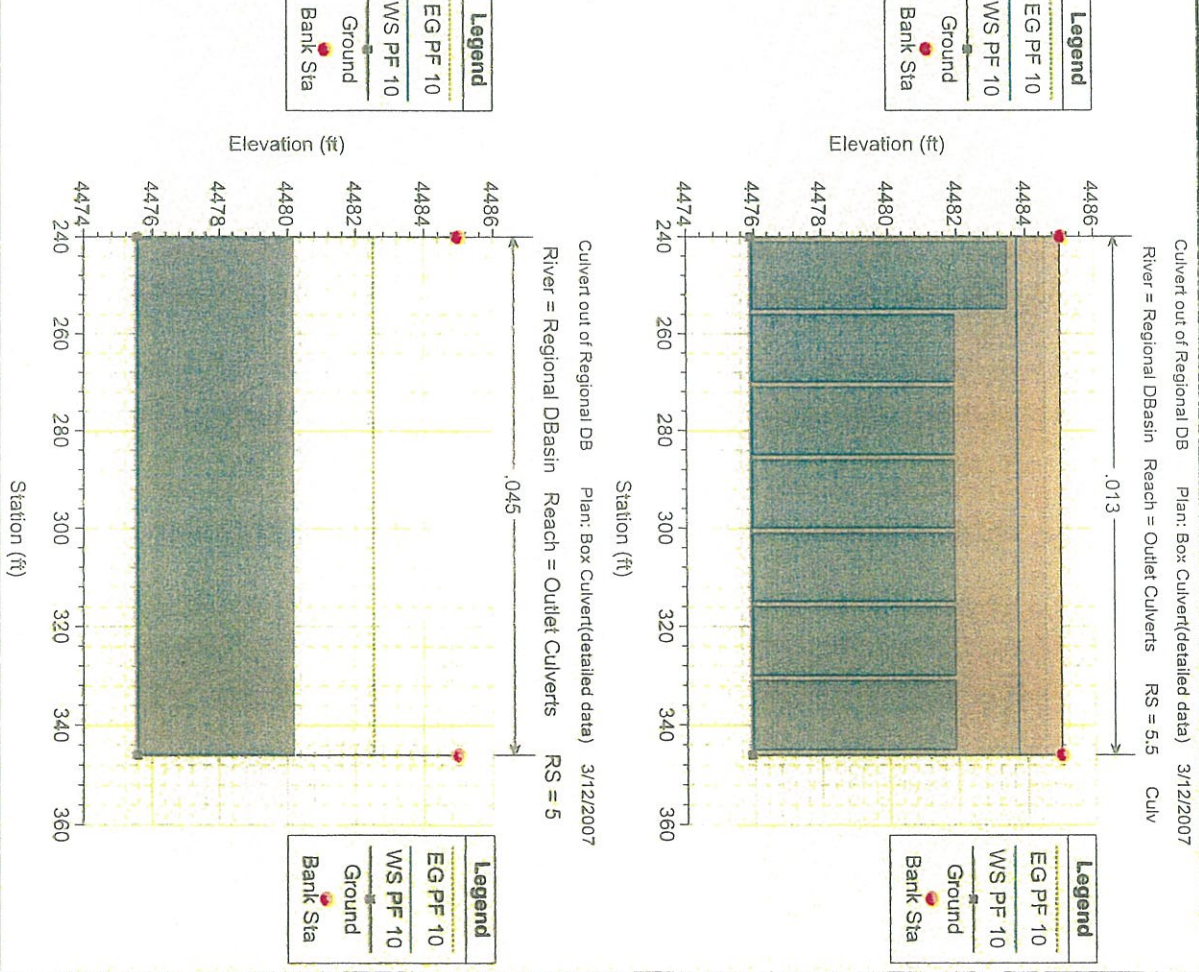
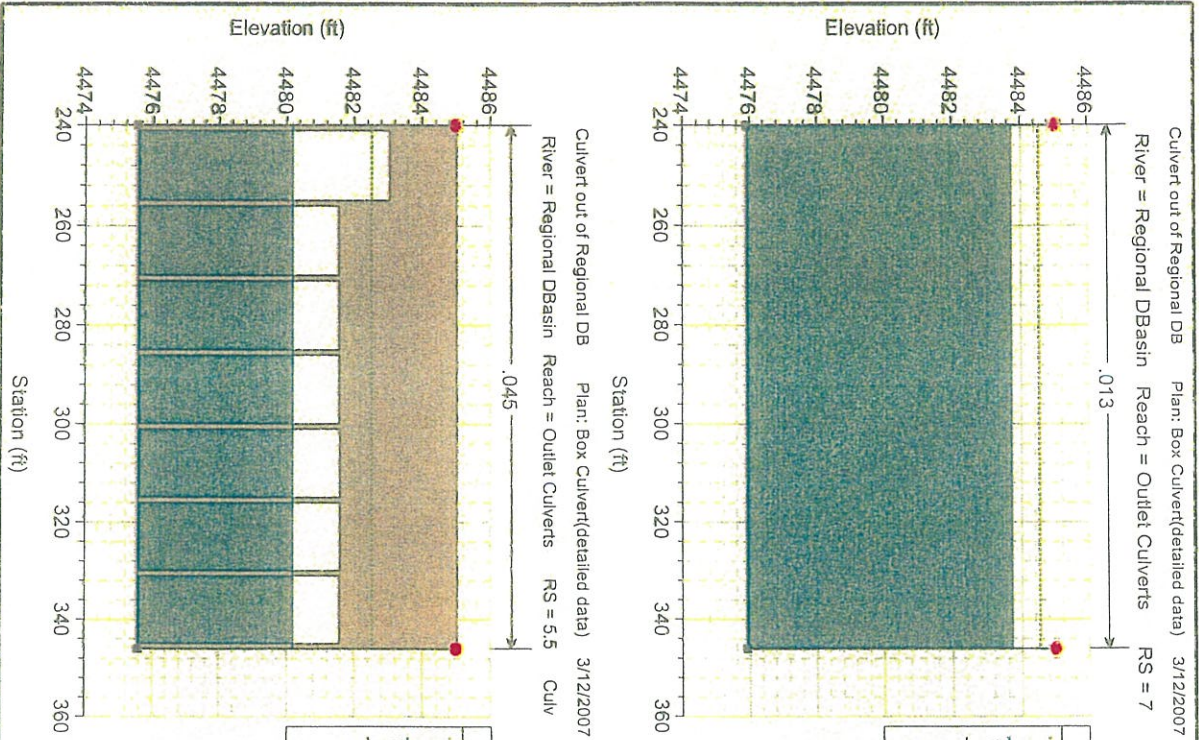
River = Regional DBasin Reach = Outlet Culverts RS = 10



Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

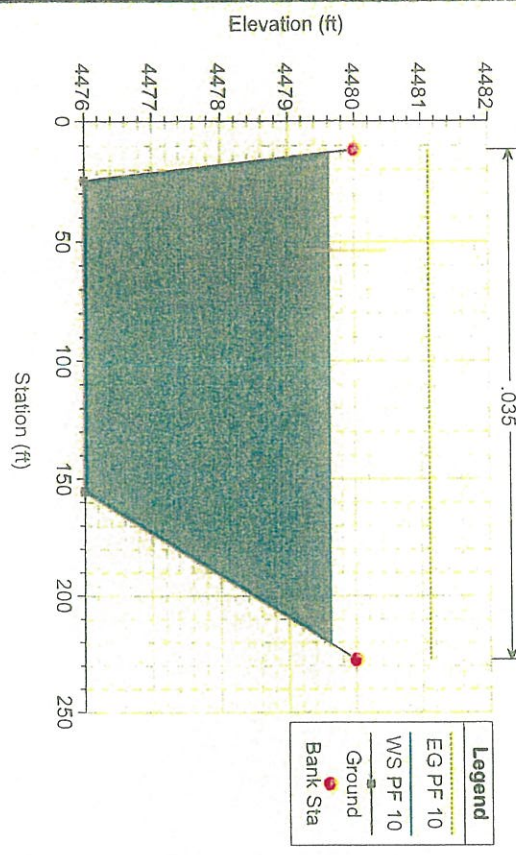
River = Regional DBasin Reach = Outlet Culverts RS = 8





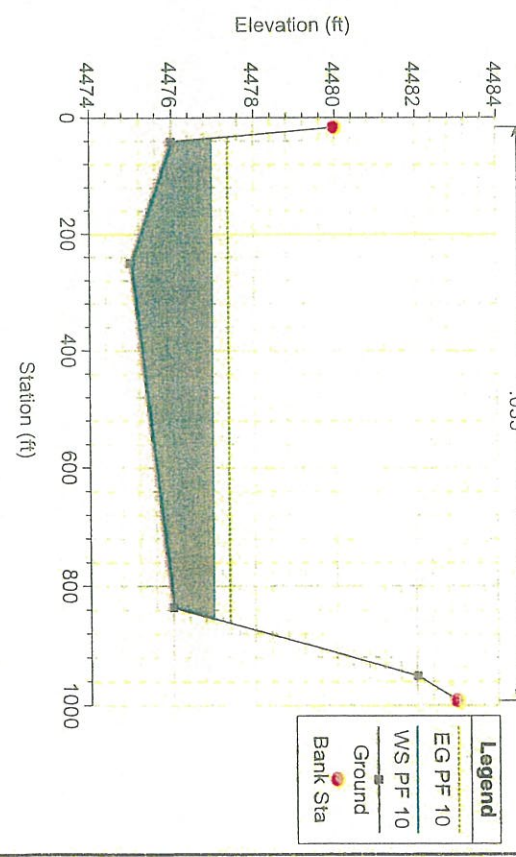
Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

River = Regional DBasin Reach = Outlet Culverts RS = 3



Culvert out of Regional DB Plan: Box Culvert(detailed data) 3/12/2007

River = Regional DBasin Reach = Outlet Culverts RS = 2







Revisions:	Date: References
A	
B	
C	
D	
E	
F	

1" = 200'

PONDUS-ASBUILT.dwg

HYDRAULIC WORKMAP

FIGURE B-1

Quad Knopf Job #	
N0432	
March, 2007	



APPENDIX C



HEC-1 MODELS

DRph5.out

DRph5+BV1.out

Truncated

CD containing electronic version of models listed above



```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
* JUN 1998 *
*
* VERSION 4.1 *
*
* RUN DATE 04JAN08 TIME 13:38:25 *
*
*
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

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X X XXXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID DRph5 THE PROPOSED MODEL FOR DAMONTE PHASE 5 LOMR (CASE No. 07-09-1667P)
2 ID IS ALSO THE EXITING CONDITIONS MODEL FOR THE BELLA VISTA PHASE 1 LOMR.
3 ID IT WAS RE-RUN ON JANUARY 4, 2008. ONLY THE ID INFORMATION WAS UPDATED
4 ID FOR THIS RUN. JANUARY 2008 - Model Run date is 01/04/2008
5 ID *****
6 ID CLOMR MODEL WAS USED WITHOUT CHANGE FOR THE LOMR MODEL FOR DAMONTE RANCH
7 ID PHASE 5 SUBMITTED MAY 5, 2007 AND NOT RERUN. LOMR AS-BUILT PLANS DID NOT
8 ID CHANGE THE HYDRAULIC PARAMETERS USED IN THE CLOMR.
9 ID MARCH 2007 - Model Run date is 3/12/2007
10 ID *****
11 ID UPDATED MODEL FOR DAMONTE RANCH PHASE V and BELLA VESTA PHASE 1 CLOMR
12 ID MARCH 2007 - Model Run date is 3/12/2007
13 ID *****
14 ID DAMONTE RANCH PHASE V - MARCH 2005
15 ID
16 ID * * INCLUDES DEVELOPMENT OF VILLAGE 11-B * *
17 ID
18 ID UPDATED MODEL FROM LOMR SUBMITTAL FILE NAME 0243AB.DAT (Orig. 128CLOMR.DAT)
19 ID TO REFLECT GRADING PLANS AS OF 3/2005
20 ID 100-Year HEC-1 for AS BUILT conditions. Includes Steamboat Creek &
21 ID tributaries (i.e. Galena, Jones, Browns, Bailey, 30, & 40 watersheds);
22 ID Damonte Ranch with refined watersheds, detention structures, & refined
23 ID east range watersheds; Whites Creek watersheds collected by Branch 3 & 4
24 ID with routing onto Damonte; the remainder of the Whites Creek & split flow
25 ID from Thomas Creeks watersheds routed through Double Diamond;
26 ID & Bella Vista Ranch with the remaining east range watersheds.
27 ID
28 ID File Name: DRph5.dat
29 ID Quad Knopf - formerly Nimbus Engineers
30 ID
31 ID
32 ID
33 ID REVISIONS REFLECT PHASE V DEVELOPMENT PER GRADING PLAN DATED 2/2005
34 ID The model also includes the previous changes at the Diversion structure:
35 ID a) box culverts replaced the RCPs; b) an overflow weir was added to control
36 ID a major flood event
37 ID
38 ID
39 ID *****
40 ID
41 ID * * MODIFIED 5-2005 TO REFLECT GRADING PLAN CHANGES AFFECTING EASTERN * *
42 ID * * BASINS NE-2, NE-3, NE-4, & NE-5. THESE HAVE ALL BEEN COMBINED AS * *
43 ID * * THE REMOVAL OF MIRA LOMA RD. MAKES SEPARATION UNECESSARY * *
44 ID
45 ID *****

```

Legend :

```

* W(No.)R = Subbasin
* CP XX = Combine flows at point XX
* RT XX = Route to CP XX
* DV XX = Divert hydrograph XX
* DR XX = Recall hydrograph XX
* XX = Street and Channel #, where applicable
* V = Virginia, Z = Zolezzi, F = 580 (Freeway), W = Wedge
* *****

```

1

HEC-1 INPUT

PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
46 IT 5 27JUL00 0005 288

```

47 IO 5 0
 48 IN 15.0
 * TOTAL WATERSHED AREA = 85 SQ. MI.
 * AREAL REDUCTION = 0.94
 49 JR PREC 0.94

50 KK W1R Whites Creek 1
 51 BA 1.36
 52 PB 5.5
 53 PC 0.0 .002 .005 .008 .011 .014 .017 .020 .023 .026
 54 PC .029 .032 .035 .038 .041 .044 .048 .052 .056 .060
 55 PC .064 .068 .072 .076 .080 .085 .090 .095 .100 .105
 56 PC .110 .115 .120 .126 .133 .140 .147 .155 .163 .172
 57 PC .181 .191 .203 .218 .236 .257 .283 .387 .663 .707
 58 PC .735 .758 .776 .791 .804 .815 .825 .834 .842 .849
 59 PC .856 .863 .869 .875 .881 .887 .893 .898 .903 .908
 60 PC .913 .918 .922 .926 .930 .934 .938 .942 .946 .950
 61 PC .953 .956 .959 .962 .965 .968 .971 .974 .977 .980
 62 PC .983 .986 .992 .995 .998 1.00
 63 LS 63
 64 UD 0.48
 *

65 KK W2R Whites Creek No. 2
 66 BA 0.84
 67 PB 5.4
 68 LS 65
 69 UD 0.52
 *

70 KK W1+W2 Combine W1 and W2
 71 HC 2
 *

72 KK RT-A Route to pt A
 73 RM 1 .1 0.4
 *

74 KK W3R Whites Creek No. 3
 75 BA 1.38
 76 PB 5.25
 77 LS 65
 78 UD 0.54
 *

79 KK RT-A Route to pt A
 80 RM 1 .1 .4
 *

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81 KK W4R Whites Creek No. 4
 82 BA 1.47
 83 PB 5.0
 84 LS 57
 85 UD 0.72
 *

86 KK W1234 Combine W1-W4
 87 HC 3
 *

88 KK RT-B Route to pt B
 89 RM 1 .1 0.4
 *

90 KK W5R Whites Creek No. 5
 91 BA 1.27
 92 PB 4.8
 93 LS 58
 94 UD 0.85
 *

95 KK W5+CH Combine W5 and channel
 96 HC 2
 *

97 KK RT-C Route to pt C
 98 RM 2 0.185 0.4
 *

99 KK W6R Whites Creek No. 6
 100 BA 1.43
 101 PB 4.1
 102 LS 57
 103 UD 1.23
 *

104 KK W6+CH Combine W6 and channel
 105 HC 2
 *

106 KK RT-D Route to pt D
 107 RM 1 0.1 0.4
 *

108 KK W7R Whites Creek No. 7
 109 BA 0.85
 110 PB 3.4
 111 LS 68
 112 UD 0.96
 *

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

113 KK W7+CH Combine W7 and channel
114 HC 2
*

115 KK RT-DIF Route flows to Difffluence
116 RM 1 0.104 0.4
*

117 KK W8R Whites Creek No. 8
118 BA 0.75
119 PB 3.0
120 LS 65
121 UD 1.19
*

122 KK CP DIF Combine flows at Difffluence
123 HC 2
*

124 KK DV 4 Divert flows into channel #4 - south branch
125 KM Hydrograph at this station is flow in channel 4
126 DT CH 123
127 DI 0 2000 3500 5100
128 DQ 0 1700 2700 3750
*

129 KK RT W4 Route flows in channel #4 to Wedge Parkway
130 RM 2 .178 .3
*

131 KK W17R Whites Creek No. 17
132 BA 0.58
133 PB 2.8
134 LS 67
135 UD 0.31
*

136 KK CP W4 Combine flows at Wedge Parkway
137 HC 2
*

138 KK RT F4 Route flows to proposed RCB at 580
139 RM 1 0.111 .3
*

140 KK W19R Whites Creek No. 19
141 BA 0.33
142 PB 2.75
143 LS 60
144 UD 0.22
*

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

145 KK W9R Whites Creek No. 9 (Steamboat Hills Area, above Mt. Rose Hwy)
146 BA 2.39
147 PB 2.8
148 LS 69
149 UD 0.51
*

150 KK RT F4 Route flows to proposed RCB at 580 (Channel 4)
151 RM 2 0.181 0.3
*

152 KK CP F4 Combine flows at proposed I-580 RCB (Channel 4)
153 HC 3
*

154 KK RT V4 Route flows to Virginia Street (Channel 4 near Browns School)
155 RM 1 0.121 .3

156 KK W20R Whites Creek No. 20
157 BA 0.22
158 PB 2.73
159 LS 61
160 UD 0.22
*

161 KK CP V4 Combine flows at Channel #4 and Virginia St. (near Browns School)
162 HC 2
*

163 KK RT STM ROUTE BRACH 4 TO STEAMBOAT CREEK - THRU PROPOSED CHANNEL
164 RK 2250 0.013 .035 TRAP 75 3
*
*
* *****
* STEAMBOAT CREEK MODEL
* *****
*
*
165 KK G1G2 Upper Galena Creek - G1 & G2 COMBINED
166 BA 8.0
167 PB 4.89
168 LS 70
169 UD 1.9
*

170 KK OUTJ1 Route to Confluence with Jones Creek
171 RD 5280 .046 0.07 TRAP 15 0.5
*

1

HEC-1 INPUT

PAGE 6

LINE	ID	1	2	3	4	5	6	7	8	9	10
172	KK	J1 Jones Creek Watershed									
173	BA	6.4									
174	PB	3.51									
175	LS		58								
176	UD	1.3									
	*										
177	KK	OUTJ1 Combine Jones and Galena Creek									
178	HC	2									
	*										
179	KK	OUTG3 Route Galena to Pleasant Valley foothill									
180	RD	7392 0.043 0.07 TRAP 15 1									
	*										
181	KK	G3 Lower Galena Creek									
182	BA	3.9									
183	PB	3.4									
184	LS		62								
185	UD	1.2									
	*										
186	KK	OUTG3 Combine Galena flows at Pleasant Valley foothill									
187	HC	2									
	*										
188	KK	OUT30 Route Galena Creek watershed to Steamboat Gage (use COE routing)									
189	RM	7 0.61 0.2									
	*										
190	KK	15 Browns Creek									
191	BA	4.2									
192	PB	4.10									
193	LS		61								
194	UD	1.7									
	*										
195	KK	OUT30 Route Browns Creek to Steamboat Gage (use COE routing)									
196	RM	16 1.34 0.2									
	*										
197	KK	30 COE Watershed No. 30									
198	BA	16.7									
199	BF	500 0 1									
200	PB	2.8									
201	LS		77								
202	UD	1.8									
	*										

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
203	KK	OUT30 Combine									
204	HC	3									
	*										
205	KK	OUT40 Route flows to HWY 341 (use COE routing)									
206	RM	3 0.23 0.2									
	*										
207	KK	35 Bailey Canyon									
208	BA	15.3									
209	BF	0 10 1.1									
210	PB	2.95									
211	LS		80								
212	UD	2.2									
	*										
213	KK	40 Watershed No.40									
214	BA	2.5									
215	PB	2.77									
216	LS		77								
217	UD	1.1									
	*										
218	KK	OUT40 Combine Steamboat Ck with areas 35 and 40 at HWY 341									
219	HC	3									
	*										
220	KK	OUT341 ROUTE STEAMBOAT THROUGH HWY 341 USING MODIFIED PULS									
221	RS	1 STOR 0									
222	SA	.31 9.48 46.1									
223	SE	4550 4560 4570									
224	SQ	300 2475 58000									
	*										
225	KK	C-1B									
226	BA	0.072									
227	PB	2.5									
228	LS		69 64								
229	UD	0.22									
	*										
230	KK	C-1A									
231	BA	0.062									
232	LS		64								
233	UD	0.20									
	*										
234	KK	RT C1 ROUTING POD C-1A THRU CHANNEL C-1C TO CHANNEL C-1E									
235	RD	1000 0.014 0.030 TRAP 5 3									
	*										

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
236	KK	RT C1	ROUTING	POD C-1A	THRU CHANNEL C-1E	TO CULVERT C-C2C					
237	RD	1800	0.0056	0.030	TRAP	5	3				
	*										
238	KK	CPC1B									
239	HC	2									
	*										
240	KK	CB CUR	Combine flows	just north of SR 341	(Steamboat Ck)						
241	HC	2									
	*										
242	KK	OUTDS	Route Steamboat	to just north of south Damonte	property line						
243	RM	2	0.153	.35							
	*										
244	KK	CB DS	COMBINE STEAMBOAT &	WHITES BRANCH 4 @ DAMONTE	SOUTH BOUNDARY						
245	HC	2									
	*										
246	KK	RT WHT	ROUTE TO SOUTH BOUNDARY	OF WHITE'S CREEK MEADOW	SUBDIVISION						
247	RM	1	0.084	0.2							
	*										
	*										
	*										
248	KK	DR 123	Recall channel 1, 2, and 3	flows							
249	DR	CH 123									
	*										
250	KK	DV 2&3	Divert flows into channels 2	and 3 - two middle branches							
251	KM		Hydrograph at this station	is flow in channels 2 and 3							
252	DT	CH 1									
253	DI	0	1700	2700	3750						
254	DQ	0	350	550	700						
	*										
255	KK	RT 2&3	Route flows to pt where	channels 2 and 3 combine	(2000' u/s Virginia)						
256	RM	3	.245	.3							
257	KK	W10R	Whites Creek No. 10								
258	BA	0.3									
259	PB	2.8									
260	LS		55								
261	UD	.32									
	*										
262	KK	CP 23	Combine local flows	with channels 2 and 3							
263	HC	2									
	*										

1

HEC-1 INPUT

PAGE 9

LINE	ID	1	2	3	4	5	6	7	8	9	10
264	KK	DV 23A	Divert flows at CP 23	(Channels 2 and 3 Diverge)							
265	KM		Hydrograph at this station	is in channel 3 (Channel 2 is diverted)							
266	DT	CH 2									
267	DI	0	2000	3500							
268	DQ	0	1000	1750							
	*										
269	KK	RT V3	Route flow to Virginia St.	(CP V3)							
270	RM	2	0.136	.2							
271	KK	W11R	Whites Creek No. 11								
272	BA	0.32									
273	PB	2.7									
274	LS		75								
275	UD	0.27									
	*										
276	KK	CP V24	Combine Subbasin W11R,	and Channel 3 at Virginia	Street						
277	HC	2									
278	KK	RT F3	Route flow to F3	(Channel 3 at 580)							
279	RM	3	0.234	0.2							
	*										
280	KK	W16R	Whites Creek No. 16								
281	BA	0.11									
282	PB	2.7									
283	LS		81								
284	UD	0.21									
	*										
285	KK	CP F3	Combine flows at proposed	RCB on 580 (Channel 3)							
286	HC	2									
	*										
287	KK	RT DSW	ROUTE THRU DRAINAGE	DITCH TO STEAMBOAT CREEK							
	*										
	*										
288	RD	2700	0.003	0.035	TRAP	50	3				
	*										
289	KK	W18RA									
	*										
	*										
290	BA	0.21									
291	PB	2.7									
292	LS		80								
293	UD	0.33									
	*										
294	KK	CB DSW	COMBINE WHITES CREEK	BRANCHES 3 & W18RA @	STEAMBOAT CREEK						

LINE	ID	1	2	3	4	5	6	7	8	9	10
296	KK	S-1									
297	BA	0.041									
298	PH	1	0.001	0.478	0.869	0.145	1.52	1.58	2.11	2.53	
299	LS		66								
300	UD	0.17									
301	KK	RT S3 ROUTING	POD S-1	THRU STEAMBOAT	TO CPS3A						
302	RM	2	.2	.4							
303	KK	S-2									
304	BA	0.062									
305	LS		62								
306	UD	0.20									
307	KK	RT S3 ROUTING	POD S-2	THRU STEAMBOAT	TO CPS3A						
308	RM	1	.1	.1							
309	KK	S-3A									
310	BA	0.039									
311	LS		63								
312	UD	0.17									
313	KK	RT S3 ROUTING	POD S-3A	THRU CHANNEL	ST-1 TO CPS3A						
314	RD	1000	0.0025	0.030	TRAP	5	3				
315	KK	CPS3A									
316	HC	3									
317	KK	RT S5 ROUTING	CPS3A	THRU STEAMBOAT	TO CPS5						
318	RM	4	0.3311	0.4							
319	KK	S-3B									
320	BA	0.016									
321	LS		63								
322	UD	0.14									
323	KK	RT S5 ROUTING	POD S-3B	THRU STEAMBOAT	TO CPS5						
324	RM	3	0.2837	0.4							
325	KK	S-4									
326	BA	0.021									
327	LS		63								
328	UD	0.16									

LINE	ID	1	2	3	4	5	6	7	8	9	10
329	KK	RT S5 ROUTING	POD S-4	THRU STEAMBOAT	TO CPS5						
330	RM	2	0.1497	0.4							
331	KK	S-5									
332	BA	0.032									
333	LS		76								
334	UD	0.16									
335	KK	RT S5 ROUTING	POD S-5	OVERLAND	TO CPS5						
336	RM	2	0.1230	0.1							
337	KK	CPS5									
338	HC	4									
339	KK	RT WHT ROUTINT	CPS5	TO WHT	THRU STEAMBOAT						
340	RM	2	0.1775	.4							
341	KK	CB WHT	COMBINE STEAMBOAT	CREEK W/ WHITES	CREEK BRANCHES	3&4					
342	HC	3									
343	KK	HD	WATERSHED TO ACCOUNT	FOR COM & IND	AREA IN WHITES	CK MEADOWS					
344	KM		DISCHARGES TO	STEAMBOAT	CREEK						
345	BA	.114									
346	LS		95								
347	UD	.32									
348	KK	CP HD	COMBINE HD WITH	STEAMBOAT	CREEK UPSTREAM	OF DIVERSION	STRUCTURE				
349	HC	2									
	*		DIVERSION FROM	STEAMBOAT	TO EAST						
350	KK	DIVSTR	STAGE, STORAGE,	AND DISCHARGE	FROM DIVERSION	POND					
351	KM		BACKWATER FROM	THE 4 8'X10'	RCBs						
352	KO	3									
353	RS	1	ELEV	4475							
	*		DIVERSION POND	AREAS FOR	ELEVATION	4475 TO 4490;	4 8'x 10'	RCBs, I.E.	4475		
	*		WEIR WIDTH =	240' @	CREST	4485'					

* ADDITIONAL ELEVATIONS ADDED TO RESERVOIR , AREAS IN THESE 2 ARE
 * KEPT CLOSE TO THE AREA AT ELEVATION 4488

354	SA	.07	0.25	0.35	0.72	1.13	2.93	3.23	3.51	3.83	4.11
355	SA	4.34	4.69								
356	SE	4475	4476	4477	4479	4480	4483	4484	4485	4486	4487
357	SE	4488	4489								
358	SQ	0	124	336	920	1272	2512	2976	3272	4222	5914
359	SQ	8003	10364								

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

360 KK STEAM DIVERSION
 * DI=CULVERT+WEIR FLOW, DQ=WEIR FLOW INTO DETENTION BASIN 1
 361 DT BAS 1
 * DI CARDS FOR 5-108" RCP CULVERTS AND WEIR
 362 DI 0 124 336 920 1272 2512 2976 3272 4222 5914
 363 DI 8003 10364
 * DQ CARDS INDICATE FLOW OVER WEIR INTO BASIN 1
 364 DQ 0 0 0 0 0 0 0 0 726 2074
 365 DQ 3847 5980

366 KK OUTDM Route Steamboat to DM (near middle of Damonte property)
 367 RM 2 0.15 0.25

368 KK OUTDN ROUTE STEAMBOAT TO DN -DAMONTE NORTH BOUNDARY
 369 RM 2 0.2 0.25

DAMONTE RANCH PHASE V

* NOTE: Basins denoted "* DR" correspond to Nimbus Model
 443Post.dat (1/2005)

* PHASE V: ON-SITE AREA DRAINING TO STEAMBOAT CREEK

370 KK A7
 * KK DR 2
 371 BA 0.037
 372 PB 2.8
 373 LS 85
 374 UD 0.531

375 KK STM+7
 376 KM COMBINE A7 INTO STEAMBOAT CRK
 377 HC 2

378 KK A6
 * KK DR 8
 379 BA .019
 380 LS 90
 381 UD .289

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

382 KK STM+6
 383 KM COMBINE A6 INTO STEAMBOAT CRK
 384 HC 2

385 KK A3
 386 BA .005
 387 LS 90
 388 UD .167

389 KK STM+3
 390 KM COMBINE A3 INTO STEAMBOAT CRK
 391 HC 2

392 KK A2
 393 BA .020
 394 LS 90
 395 UD .167

396 KK STM+2
 397 KM COMBINE A2 INTO STEAMBOAT CRK
 398 HC 2

399 KK A17
 400 KM CHANNEL E CROSSING AT CARAT DR.
 * KK DR 18
 401 BA 0.029
 * BA 0.031
 402 LS 83

403 UD .235
 *
 *
 404 KK A18
 * KK DR 19
 405 BA 0.036
 * BA 0.021
 406 LS 83
 407 UD .319
 *

1

HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

408 KK CHNL-E
 409 KM CHNL-E CHANNEL E
 410 HC 2
 *
 *

411 KK STM+E
 412 KM COMBINE CHANNEL E WITH STEAMBOAT CRK
 413 KM DOWNSTREAM DAMONTE BNDRY
 414 HC 2
 *
 *

415 KK RT NST ROUTING CPSTM2 TO CPN4STM2
 416 RM 5 0.3916 .4
 *
 *
 *

* * NW-4 IS BEING DEVELOPED UNDER PHASE V
 * *
 * KK NW-4
 * BA 0.129
 * PB 2.5
 * LS 73 68
 * UD 0.33
 *
 *

* * FOLLOWING DAMONTE BASINS DRAIN TO THE WESTERN PERIMETER DITCH

417 KK A4
 * KK DR 6
 418 BA 0.017
 419 LS 90
 420 UD .197
 *
 *

421 KK A23
 422 BA 0.004
 423 LS 85
 424 UD 0.531
 *

425 KK A1
 * KK DR 8
 426 BA 0.014
 * BA 0.051
 427 LS 90
 428 UD .289
 *
 *
 *

1

HEC-1 INPUT

PAGE 15

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

429 KK A22
 * KK DR 1
 430 BA 0.004
 431 LS 91
 432 UD 0.531
 *
 *

433 KK A5
 * KK DR 4
 434 BA 0.047
 * BA 0.045
 435 LS 83
 436 UD .313
 *

437 KK CARAT1
 438 KM CARAT DR. CULVERT #1
 439 HC 2
 *
 *
 *
 *
 *
 *

440 KK CHNL-A
 441 KM CHNL-A DAMONTE WESTERN PERIMETER DITCH

442 HC 4
 *
 *
 *
 *
 * DAMONTE PHASE V: ON-SITE AREAS A16, A19, A20
 *
 443 KK A16
 * KK DR 20
 444 KM NODE FOR SIZING INLET TO CHANNEL F UNDER CARAT DR
 445 BA 0.018
 * BA 0.021
 446 LS 90
 447 UD .222
 *
 448 KK A19
 * KK DR 21
 449 BA 0.036
 450 LS 83
 451 UD .269
 *

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HEC-1 INPUT

PAGE 16

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

452 KK A20
 * KK DR 22
 453 BA 0.023
 454 LS 85
 455 UD .355
 *
 *
 *
 456 KK CHNL-F CHANNEL F
 457 KM OUTLET 3
 458 HC 3
 *
 *
 *
 459 KK STM+AF
 460 KM COMBINE CHANNEL A & F INTO STEAMBOAT CRK
 461 HC 3
 *
 *
 *
 462 KK APTS-9
 463 KM FUTURE APARTMENTS / PARK SITE - - PREVIOUSLY KNOWN IN
 464 KM NIMBUS MODELS AS PRE-DEV BASINS "W-4", "W-5", & "W-6"
 * PLANS CURRENTLY CALL FOR AN 18" STUB UNDER STEAMBOAT PKY
 * DRAINS TO CHANNEL B
 465 BA 0.032
 466 LS 87
 467 UD .279
 *
 *
 *
 468 KK A8
 * KK DR 10
 469 BA 0.071
 470 LS 88
 471 UD .338
 *
 *
 *
 472 KK CHNL-B UPSTREAM SECTION OF CHANNEL B
 473 HC 2
 *
 *
 *
 474 KK D12&13
 475 KM EXISTING DAMONTE RANCH 12 & 13
 * KK EX 11 EXISTING BASIN #11 (D.R. 12&13)
 476 BA 0.057
 477 LS 84
 478 UD .312
 *
 *
 *

1

HEC-1 INPUT

PAGE 17

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

479 KK A9
 * KK DR 12
 480 BA 0.050
 481 LS 83
 482 UD .286
 *
 *
 *
 483 KK CHNL-C
 484 KM CHANNEL C
 485 HC 2
 *
 *
 *
 486 KK B&C
 487 KM COMBINE CHANNEL B & C
 488 HC 2
 *
 *
 *

489 KK A14
 * KK DR 13
 490 BA 0.055
 491 LS 83
 492 UD .295
 *
 *
 493 KK A13
 * KKDR 14A
 494 BA 0.045
 * BA 0.047
 495 LS 83
 496 UD .295
 *
 *
 497 KK A15
 * KK DR 15
 498 BA 0.018
 * BA 0.019
 499 LS 87
 500 UD .308
 * *
 *
 501 KK CHNL-D CHANNEL D
 502 KM CHANNEL D
 503 HC 4
 *
 *
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

504 KK A11
 * KK DR 17
 505 BA 0.014
 * BA 0.016
 506 LS 90
 507 UD .275
 * *
 *
 508 KK A12
 * KKDR 14B
 509 BA 0.020
 * BA 0.043
 510 LS 90
 511 UD .475
 * *
 *
 512 KK 11+12 ROADSIDE DITCH ALONG CARAT DR
 513 KM ROADSIDE DITCH ALONG CARAT DR DRAINING A11 & A12
 514 HC 2
 *
 *
 *
 515 KK CHNL D CHANNEL D CROSSES CARAT DR
 516 KM CROSSING AT CARAT DR AND CHANNEL D
 517 HC 2
 *
 *
 *
 518 KK X12+13 EXISTING DAMONTE RANCH 12 & 13 (AREA 16)
 519 KM WAS DEVELOPED PRIOR TO DAMONTE RANCH PHASE V
 520 KM PREVIOUSLY KNOWN IN NIMBUS MODELS AS PRE-DEV BASIN "W-7"
 521 BA 0.076
 522 LS 86
 523 UD .733
 *
 *
 *
 524 KK A10
 * KK DR 24
 525 BA 0.012
 526 LS 89
 527 UD .206
 *
 *
 *
 528 KK
 529 HC 2
 *
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

530 KK A21 FUTURE SCHOOL
 * KK DR 23 FUTURE SCHOOL SITE
 531 BA 0.015
 532 LS 93
 533 UD .212
 *
 *
 *
 534 KK WTLNDS DISCHARGE TO WETLANDS
 535 KO 3
 536 HC 3
 * *
 *

```

*
*
*
537 KK RC BAS RECALL DIVERSION FROM STEAMBOAT
538 KM OVERFLOW FROM DIV. STRUCTURE 1
539 DR BAS 1
*

540 KK BAS 1 STAGE, STORAGE, AND DISCHARGE FROM BASIN 1
541 KM MODIFY BASIN 1 MAKE IT 5 FT DEEPER TO REDUCE PEAK FLOWS TO EAST
542 KO 3
543 RS 1 ELEV 4473
* *** BAS 1 OUTLET 7 PIPE ARCHES W/1-36" RCP *****
544 SA 19 26.26 30.61 32.63 33.7 34.10 34.47 34.82 35.18 35.54
545 SA 35.97
546 SE 4475 4476 4477 4478 4479 4480 4481 4482 4483 4484
547 SE 4485
548 SQ 5 7 10 515 1021 1523 2027 2537 3059 3561
549 SE 4475.4 4475.92 4476.6 4477.64 4478.54 4479.28 4479.95 4480.59 4481.25 4481.87
* Updated based on AS-BUILT data
* SQ 5 7 10 515 1021 1527 2031 2537 3059 35
* SE4475.4 4475.92 4476.6 4477.64 4478.54 4479.28 4479.95 4480.59 4481.25 4481.
* previous data
* SQ 5 7 10 515 1521 2027 2533 3038 3059 35
* SE4475.4 4475.92 4476.6 4477.6 4478.5 4479.3 4480.1 4480.7 4481.3 4481

550 KK BASIDS
551 DT 36DIVQ 130
* ***** 100' WEIR *****
552 DI 10 515 1521 2027 2533 3038 3059 3562 4065
553 DQ 10 15 21 27 33 38 59 62 65
*

554 KK POND2
555 KM POND 2 WILL OUTFLOW OVER NATURAL GROUND WITH NO DETENTION. THE FLOW
556 KM WILL BE ROUTED OVERLAND TO THE FIRST COMBINATION POINT IN THE WETLANDS.
557 RM 1 0.2 0.2
*

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HEC-1 INPUT

PAGE 20

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

558 KK T-1
559 BA 0.036
560 PB 2.5
561 LS 74 68
562 UD 0.20
*

563 KK RT T2 ROUTING POD T-1 THRU CHANNEL T-1 TO CPT2
564 RD 300 0.01 0.030 TRAP 10 3
*

565 KK T-2
566 BA 0.065
567 PB 2.5
568 LS 73 70
569 UD 0.21
*

570 KK CPT2 COMBINING PODS T1 AND T2
571 HC 2

572 KK RT T3 ROUTING CPT2 THRU CHANNEL T-2 TO CPT3
573 RD 970 0.01 0.030 TRAP 10 3
*

574 KK T-3
575 BA 0.061
576 PB 2.5
577 LS 79 78
578 UD 0.22
*

579 KK CPT3
580 HC 2
*

581 KK CPD1A COMBINING TAHOE AND CPT3 AND SPLIT FROM STEAMBOAT
582 HC 2
*

583 KK RT WT ROUTE TO CPWET
584 RM 3 0.2621 0.1
*
* East side drainages

585 KK WSF1 East side watershed F1
586 BA 0.775
587 PB 2.80
588 LS 77
589 UD .24
*

```

1

HEC-1 INPUT

PAGE 21

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

590 KK WSE1 East side watershed E
591 BA 2.1
592 PB 2.8
593 LS 78
594 UD .53

```

```

*
595 KK F1E1 COMBINE F1 & E1
596 HC 2
*
597 KK C-2
598 BA 0.034
599 PB 2.5
600 LS 62 20
601 UD 0.17
*
602 KK RT C3 ROUTING C-2 THRU CHANNEL C-3 TO CPC3
603 RD 1050 0.005 0.030 TRAP 65 3
*
604 KK C-1C
605 BA 0.070
606 PB 2.5
607 LS 63 50
608 UD 0.20
*
609 KK RT C3 ROUTING C-1C THRU CHANNEL C-3 TO CPC3
610 RD 1050 0.005 0.030 TRAP 65 3
*
611 KK C-3
612 BA 0.034
613 PB 2.5
614 LS 63 20
615 UD 0.18
*
616 KK CPC3
617 HC 4
*
618 KK RT C4 ROUTING CPC3 THRU CHANNEL C-4 TO CPC4
619 RD 550 0.005 0.030 TRAP 65 3
*
620 KK C-4
621 BA 0.040
622 PB 2.5
623 LS 65 64
624 UD 0.19
*

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HEC-1 INPUT

PAGE 22

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

625 KK CPC4 COMBINE CPC3 AND POD C-4
626 HC 2
*
627 KK RT C7 ROUTING CPC4 THRU CHANNEL C-5 TO CHANNEL C-7
628 RD 1700 0.005 0.030 TRAP 70 3
*
629 KK RT C7 ROUTING CPC4 THRU CHANNEL C-7 TO CPC7
630 RD 1400 0.0045 0.030 TRAP 75 3
*
631 KK C-5
632 BA 0.068
633 PB 2.5
634 LS 70 63
635 UD 0.20
*
636 KK RT C7 ROUTING POD C-5 THRU CHANNEL C-5 TO CHANNEL C-7
637 RD 100 0.005 0.030 TRAP 70 3
*
638 KK RT C7 ROUTING POD C-5 THRU CHANNEL C-7 TO CPC7
639 RD 1400 0.0045 0.030 TRAP 75 3
*
640 KK C-7
641 BA 0.026
642 PB 2.5
643 LS 81 70
644 UD 0.16
*
645 KK C-6
646 BA 0.125
647 PB 2.5
648 LS 64 20
649 UD 0.23
*
650 KK RT C7 ROUTING POD C-6 THRU CHANNEL C-6 TO CHANNEL C5
651 RD 2000 0.0120 0.030 TRAP 10 3
*
652 KK RT C7 ROUTING POD C-6 THRU CHANNEL C-5 TO CHANNEL C-7
653 RD 100 0.005 0.030 TRAP 3
*
654 KK RT C7 ROUTING POD C-6 THRU CHANNEL C-7 TO CPC7
655 RD 1400 0.0045 0.030 TRAP 75 3
*
656 KK CPC7 COMBINING CPC4 AND PODS C-5, C-7, C-6
657 HC 4
*
658 KK RT WT ROUTING CPC7 TO CPNET
659 RM 2 0.1804 0.1
*

```

1

HEC-1 INPUT

PAGE 23

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

660 KK W-1
661 BA 0.065
662 PB 2.5
663 LS 81 65
664 UD 0.22

665 KK RT W1 ROUTING POD W-1 TO CPWET
666 RM 1 .1 .1

667 KK CPWET COMBINE CPC7, POD W-1, AND D1B (CET #1)
668 HC 3

669 KK RT W1 ROUTING CPWET TO CPWET1
670 RM 3 0.2708 0.1
* East side drainages

671 KK E2A
672 KM THIS IS A COMBINED WATERSHED (E2 & A)
673 BA 2.1
674 PB 2.8
675 LS 78
676 UD 0.53
*

677 KK SE-2
678 BA 0.06
679 PB 2.5
680 LS 72
681 UD 0.19

682 KK RT S3 ROUTING POD SE-2 THRU CHANNEL SE-4B TO CPSE3
683 RD 1300 0.045 0.035 TRAP 20 3
*

684 KK SE-3
685 BA 0.053
686 PB 2.5
687 LS 62 23
688 UD 0.21
*

689 KK SE-1
690 BA 0.106
691 PB 2.5
692 LS 62 23
693 UD 0.22

694 KK RT S3 ROUTING POD SE-1 THRU CHANNEL SE-4A TO CPSE3
695 RD 1450 0.0186 0.030 TRAP 15 3
*

1

HEC-1 INPUT

PAGE 24

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

696 KK CPSE3
697 HC 3

698 KK RT S5 ROUTING CPSE3 THRU CHANNEL SE-5 TO CPSE5
699 RD 920 0.006 0.030 TRAP 50 3
*

700 KK SE-4
701 BA 0.016
702 PB 2.5
703 LS 65 20
704 UD 0.16
*

705 KK SE-5
706 BA 0.021
707 PB 2.5
708 LS 63 5
709 UD 0.15

710 KK CPSE5 COMBINE CPSE5 CPSE5 AND PODS SE-4 AND SE-5
711 HC 3

712 KK RT S7 ROUTING CPSE5 THRU CHANNEL SE-6 TO CPSE7
713 RD 1025 0.006 0.030 TRAP 50 3
*

714 KK SE-6
715 BA 0.004
716 PB 2.5
717 LS 66
718 UD 0.12

719 KK RT S7 ROUTING POD SE-6 THRU CHANNEL SE-7 TO CHANNEL SE-8
720 RD 800 0.019 0.030 TRAP 18 3
*

721 KK SE-7
722 BA 0.10
723 PB 2.5
724 LS 76 65
725 UD 0.14

726 KK CPSE7 COMBINE CPSE5 AND PODS SE-6 AND SE-7
727 HC 3

728 KK RT W1 ROUTING CPSE-7 THRU CHANNEL SE-8 TO CHANNEL SE-9
729 RD 620 0.0060 0.030 TRAP 65 3
*

1

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

798 BA 0.36
 799 PB 2.8
 800 LS 76
 801 UD .18

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

802 KK CPB12 COMBINE WATERSHEDS B1 & B2
 803 HC 2

804 KK RT E3 ROUTING WSB12 THRU CHANNEL E-3A TO CHANNEL E-3B
 805 RD 1350 0.046 0.035 TRAP 15 3

806 KK RT E3 ROUTING WSB12 THRU CHANNEL E-3B TO CPE3
 807 RD 1300 0.0063 0.030 TRAP 15 3

808 KK RT E4 ROUTING CPE3 THRU CHANNEL E-4 TO CPE-4
 809 RD 970 0.0035 0.030 TRAP 15 3

810 KK E-4
 811 KM MODIFY E-4, INCLUDE OLD E-3. THESE 2 ARE NOW THE HIGH SCHOOL SITE
 812 BA 0.1
 813 PB 2.5
 814 LS 86
 815 UD 0.2

816 KK RT E4 ROUTING POD E-4 THRU CHANNEL E-4 TO CPE-4
 817 RD 430 0.0035 0.030 TRAP 15 3

818 KK CPE4 COMBINE CPE3 AND POD E-4
 819 HC 3
 *

820 KK W-8
 821 BA 0.063
 822 PB 2.5
 823 LS 81 63
 824 UD 0.19

825 KK CPWETO
 826 HC 3

827 KK RS DT2 ROUTE THRU DET #2
 828 KM BELOW IS DATA FOR THE RESERVOIR ABOVE TRAPEZ WEIR, CALLED DT2 OR POND 3
 829 KM DT2 INCLUDES PORTION OF WETLAND AS STORAGE
 830 RS 1 FLOW -1
 831 SA 0 3.1 10.4 20 27.3 32.8 37.7 43.2 48.4 53.4
 832 SA 58.0
 833 SE 4452 4453 4454 4455 4456 4457 4458 4459 4460 4461
 834 SE 4462
 835 KM INSERT TRAPEZOIDAL WEIR, CREST LENGT=65', ELEV=4454, Z=.25H:1V
 836 KM LOW FLOW OUTLET IS 24" RCP AT IE=4451.3, ASSUMED TO BE INEFFECTUAL AFTER
 837 KM WATER ELEVATION OVER WEIR REACHES 4455
 838 SQ 0 3 8 110 285 567 941 1409 1975 2645
 839 SQ 3421
 * SQ 0 6 15 168 378 693 1076 1509 1991 25
 * SQ 3089
 * SQ 0 7 16 189.5 496 888 1344 1796 2336 29
 * SQ 3626
 * Updated with AS-BUILT data (using weir coefficient C=2.8)
 * SQ 0 3 8 110 285 567 941 1409 1975 26
 * SQ 3421
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

840 KK W-9
 841 BA 0.041
 842 PB 2.5
 843 LS 81 64
 844 UD 0.19
 *

845 KK CW-9
 846 KM COMBINE W-9 & CPWETO
 847 HC 2
 *

848 KK POND4
 849 KO 3
 850 KM ROUTE THRU POND 4 JUST UPSTREAM OF DAMONTE PKWY CULVERT
 851 KM OUTLET MODELED AS 5 BOX CULVERTS 4' X 12'
 852 RS 1 STOR 0
 853 SA 0.02 2.93 6.18 9.21 13.70 17.95 22.95 25.19 25.84
 854 SE 4450 4451 4452 4453 4454 4455 4456 4457 4458
 855 SQ 0 200 500 950 1450 2000 2500 2800
 856 SE 4450 4451.08 4452 4453.07 4454.06 4455.04 4456.01 4456.7
 *
 *

857 KK WET-IN
 858 KM COMBINE OFFSITE FLOW IN THE WETLANDS FROM THE SOUTH W/ ONSITE DRAINAGE
 859 HC 2
 *
 * East side drainage
 *

860 KK D1
 861 BA 1.72
 862 PB 2.8
 863 LS 78
 864 UD .45

865 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-2 TO CHANNEL NE-4A
866 RD 1150 .030 .035 TRAP 25 3
867 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-4A TO CHANNEL NE-5
868 RD 2500 .0236 .035 TRAP 25 3
869 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-5 TO CPNE-1
870 RD 800 0.0040 0.030 TRAP 80 3
+
871 KK WSC
872 BA 3.31
873 PB 2.8
874 LS 79
875 UD .65
+

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

876 KK RT N1 ROUTING BASIN WSC THRU CHANNEL NE-4A TO CHANNEL NE-5
877 RD 2500 0.0236 0.035 TRAP 25 3
878 KK RT N1 ROUTING BASIN WSC THRU CHANNEL NE-5 TO CPNE1
879 RD 800 0.0040 0.030 TRAP 80 3
+
880 KK NE-1
881 BA 0.044
882 PB 2.5
883 LS 63 34
884 UD 0.24

885 KK RT N1 ROUTING POD NE-1 THRU CHANNEL NE-5 TO CPNE1
886 RD 100 0.004 0.03 TRAP 80 3
+

887 KK CPNE1 COMBINE OFFSITE FLOW WSC AND D1 WITH NE-1
888 HC 3
+

889 KK RT W3 ROUTING CPNE1 THRU CHANNEL NE-6
890 RD 670 .004 .03 TRAP 80 3

891 KK RT W3 ROUTING CPNE1 TO CPWET3
892 RM 3 1 0.1
+

893 KK D2
894 BA 0.15
895 PB 2.6
896 LS 78
897 UD 0.06
+

898 KK RT N4 ROUTING BASIN D2 THRU CHANNEL NE-1 TO CHANNEL NE-3A
899 RD 1300 0.0192 0.035 TRAP 5 3
+

900 KK RT N4 ROUTING BASIN D2 THRU CHANNEL NE-3A TO CHANNEL NE-3B
901 RD 1100 0.03 0.035 TRAP 5 3
+

902 KK RT N4 ROUTING BASIN D2 THRU CHANNEL NE-3B TO CPNE4
903 RD 2050 0.0143 0.030 TRAP 15 3
+

* * * NOTE: THE FLOWPATHS OF NE-2 THRU 5 HAVE BEEN CORRECTED
* * * AS PER THE 4/2005 SITE PLAN, HOWEVER WERE COMBINED
* * * INTO NE2345. TO SUBDIVIDE IT AGAIN, CHECK THE
* * * ROUTING CARDS- APPEARS TO BE MUSKINGUM OVERLAND FLOW
* * *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

904 KK NE2345
905 KM COMPOSITE WATERSHED, INCLUDES BASINS FORMERLY KNOWN AS
906 KM NE-2, NE-3, NE-4, & NE-5
907 BA 0.2320
908 PB 2.5
909 LS 65 30
910 UD 0.21
+

* KK NE-3
* BA 0.054
* PB 2.5
* LS 68 34
* UD 0.25
* KK RT N5 ROUTING POD NE-3 OVERLAND TO CPNE5
* RM 3 0.2566 0.1
* * *
* * *

* KK NE-2
* BA 0.057
* PB 2.5
* LS 69 34
* UD 0.24
* * *

* KKICHLH (CENTRAL) CHANNEL H DRAINING OFFSITE BASIN D2, NE-3, NE-2
* KM UPSTREAM SECTION OF CHANNEL H

```

* HC      3
* *
* KK RT N1 ROUTING POD NE-2 THRU CHANNEL NE-5 TO CPNE-1
* RD      800 0.0040 0.030          TRAP      80      3
* *
* *
* KK NE-5
* BA 0.051
* PB 2.5
* LS          44      38
* UD 0.23
* *
* KK NE-4
* BA 0.070
* PB 2.5
* LS          43      64
* UD 0.21
* *
* *
* KK2CHNLH (CENTRAL) CHANNEL H
* KM DOWNSTREAM SECTION OF CHANNEL H
* KO      3
* HC      3
* *
* KK RT DN ROUTING CPNE5 OVERLAND THRU THE WETLANDS TO CPDN
* RM      2 0.1741 0.1
* *

```

1

HEC-1 INPUT

PAGE 31

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

911 KK CPNE4 COMBINE BSIN D2 AND POD NE-4
912 KO      3
913 HC      2

```

```

914 KK RT W3 ROUTING CPNE4 TO CPWET3
915 RM      10      1      .1
*

```

```

916 KK CPWET3 COMBINE CPWETO AND CPNE4
917 KO      3
918 HC      2
*

```

```

919 KK RT DN ROUTING CPWET3 TO CPDN OFFSITE
920 RM      6 0.4830 0.1
*

```

```

921 KK DMNTE DOWNSTREAM CP TO SUM DAMONTE FLOW
922 KO      3
923 HC      2
*

```

* [FOLLOWING IS PRE-DEV. BASINS THAT ARE PLANNED FOR DEVELOPMENT]

```

* KK W-4
* BA 0.038
* PB 2.5
* LS          79      68
* UD 0.18
* KK RT W6 ROUTING POD W-4 THRU CHANNEL NW-1 TO CHANNEL NW-2
* RD      650 0.0038 0.030          TRAP      5      3
* KK RT W6 ROUTING POD W-4 THRU CHANNEL NW-2 TO CPW6
* RD      700 0.0021 0.030          TRAP      5      3
* *

```

```

* KK W-5
* BA 0.013
* PB 2.5
* LS          77      65
* UD 0.14
* KK RT W6 ROUTING POD W-5 THRU CHANNEL NW-2 TO CPW6
* RD      700 0.0021 0.030          TRAP      5      3
* *

```

```

* KK W-6
* BA 0.017
* PB 2.5
* LS          77      5
* UD 0.15
* KK CPW6 COMBINE PODS W-4, W-5 AND W-6
* HC      3
* *

```

```

* KKRT DT2 ROUTING CPW6 THRU CHANNEL NW-3A TO CHANNEL NW-4
* RD      350 0.0086 0.030          TRAP      5      3
* KKRT DT2 ROUTING CPW6 THRU CHANNEL NW-4 TO CPDT2
* RD      1200 0.005 0.030          TRAP      5      3
* *

```

* NW-2 IS BEING DEVELOPED UNDER PHASE V

```

* KK NW-2
* BA 0.066
* PB 2.5
* LS          78      50
* UD 0.26
* *

```

```

* KKRT DT2 ROUTING POD NW-2 THRU CHANNEL NW-3B TO CHANNEL NW-4
* RD      285 0.006 0.030          TRAP      0      3
* *

```

```

* KK W-7
* KM USED TO DRAIN TO WETLANDS, NOW IS ROUTED UNDER STEAMBOAT PKWY TO A10
* KM WAS DEVELOPED BY OTHERS, NOW KNOWN AS "EXIST. DAMONTE RANCH 12&13 (AREA 16)
* BA 0.053
* PB 2.5

```

```

* LS          76      70
* UD 0.17
* KK CPDT2      COMBINE CPW6 AND PODS NW-2 AND W-7
* HC          3
*
* KK RT N1 ROUTING CPDT2 THRU CHANNEL NW-5 TO CHANNEL NW-6
* RD 2275 0.0022 0.030 TRAP 5 3
* KK RT N1 ROUTING CPDT2 THRU CHANNEL NW-6 TO CPN1
* RD 1650 0.0014 0.030 TRAP 15 3
*
*
* * NW-3 IS BEING DEVELOPED UNDER PHASE V
* KK NW-3
* BA 0.076
* PB 2.5
* LS          73      65
* UD 0.22
* KK RT N1 ROUTING POD NW-3 THRU CHANNEL NW-6 TO CPN1
* RD 1650 0.0014 0.030 TRAP 15 3
*
*
* * NW-1 IS PARTIALLY BEING DEVELOPED UNDER PHASE V
* HEC-1 INPUT

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1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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924 KK N-1
925 BA 0.02
* BA 0.104
926 PB 2.5
927 LS          76      68
928 UD 0.29
*
* KK CPN1 COMBINE CPDT2 AND PODS NW-3 , N-1
* HC 3
*

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929 KK RT N13 ROUT CPN1 THRU CHANNEL NW-7 TO CPN13
930 RD 800 .001 .03 TRAP 18 3
*
*

```

```

* * S-6 & S-7 ARE BEING DEVELOPED UNDER PHASE V
* KK S-6
* BA 0.038
* PB 2.5
* LS          73      64
* UD 0.24
*
* KKRT ST2 ROUTING POD S-6 THRU STEAMBOAT TO CPSTM2
* RM 8 0.6266 .4
*
* KK S-7
* BA 0.046
* PB 2.5
* LS          73      64
* UD 0.23
*
*

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931 KK RT N13 ROUTING CPN4STM2 TO CPN13
932 RM 10 0.8647 .4
*
*

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```

* * N-2 & N-3 ARE BEING DEVELOPED UNDER PHASE V
*
* KK N-2
* BA 0.047
* PB 2.5
* LS          75      68
* UD 0.21
*
* KK N-3
* BA 0.030
* PB 2.5
* LS          80      5
* UD 0.11
*
* KK CPN13 COMBINE CPN1, CPNST AND PODS N-2 AND N-3
* HC 2
* KK CPDN CPN13, CPWET3, CPNE5 AND OUTDN ROUTED TO CPDN, NORTH BNDRY OF DAMONTE
* HC 3
*

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[END 443LOMR.dat]

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*****
* Routing flow from Damonte property line to Bella Vista Ranch model
* *****
* HEC-1 INPUT

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1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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933 KK RT01 ROUTING OF FLOW FROM DAMONTE
934 RM 8 1.25 0.1

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935 KK D4 BELLA VISTA RANCH WATERSHED 4
 936 KM CALCULATE RUNOFF FROM WATERSHED 4
 937 BA 0.80
 938 PB 2.5
 939 LS 73
 940 UD .77

 941 KK PT01 COMBINE FLOW FROM DAMONTE (RT01) WITH WATERSHED 4
 942 HC 3
 *
 *
 943 KK RT02 ROUTE TO CONFLUENCE WITH WATERSHED 3
 944 RM 3 0.57 .1

 945 KK D3 BELLA VISTA RANCH WATERSHED 3
 946 KM CALCULATE RUNOFF FROM WATERSHED 3
 947 BA 0.7
 948 PB 2.5
 949 LS 79
 950 UD 0.77

 951 KK PT02 COMBINE FLOWS FROM WATERSHED 3 WITH RT02
 952 HC 2

 953 KK RT03 ROUTE TOTAL FLOW TO CONFLUENCE WITH WATERSHED 2
 954 RM 9 1.47 .1
 *
 *
 *
 *

 * File name : 028AS-PH1.DAT (NOV 2000) - Includes only the section of this
 * model that starts at "Begin Double Diamond Model" with watershed W18RB.
 * This model was modified from AS-PH1.DAT (MAY 1995); Whites Creek Branches
 * 3 & 4 were diverted to Steamboat Creek.
 * DOUBLE DIAMOND SUBDIVISION-PROJECT #0028 HYDROLOGIC & HYDRAULIC ANALYSIS
 * SOUTH MEADOWS PARKWAY & CENTRAL CHANNEL
 * SOUTH MEADOW/DOUBLE DIAMOND
 * BY NIMBUS ENGINEERS, RENO, NV
 * 100-Year, 24 hour model
 * WHITES CREEK MODEL COPIED FROM WHITECN.DAT
 * FIS THOMAS CREEK 100-YEAR PEAK = 2544 CFS @ S. VIRGINIA STREET.
 * WHITES CREEK SUBBASIN W18RB-NORTH OF WHITES CREEK BRANCH #3 DIVERSION
 * ADD PHASE I, PHASE VI AND PHASE V TO CENTRAL CHANNEL
 * FROM CARAT AVE TO END OF CENTRAL CHANNEL
 * MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE I (PORTIONS OF VILLAGES 11 AN
 * , PHASE I (VILLAGES 1, 2, 3 AND 4), PHASE VI)PARK, K-6 SCHOOL, AND VILLAGE 29
 * AND PHASE V (VILLAGES 24 AND 25)
 * 100-YEAR,24-HOUR MODEL
 * MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE II (VILLAGES 5 & 6 AND PARKS)
 * , PHASE III (VILLAGES 16, 17, 18, AND 19), AND PHASE IV (VILLAGES 7, 8, 9,
 * 20, 21, 22, AND 23) PLUS WETLAND BETWEEN VILLAGES 18/19 & 20.
 * USE SUBBASIN AREAS FROM MACKAY & SOMPS
 * NIMBUS ENGINEERS, RENO, NEVADA
 * MODEL MODIFIED FROM CARATDD.DAT (#9908)
 * *****

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

 955 KK W18RB WHITES CREEK SUBBASIN W18RB-NORTH BOUNDARY OF WHITES CK MEADOW SUBDIV.
 956 KM DAMONTE RANCH NORTH OF WHITES CK. BRANCH #3 AND SOUTH OF DOUBLE DIAMOND
 957 KM W18RB AREA REDUCED DUE TO ROUTING OF A PORTION OF IT TO STEAMBOAT CREE
 958 KM NEW WATERSHED DRAINING TO STEAMBOAT CREEK, HD IS UPSTREAM OF DIVSTR
 * BA .2344
 959 BA .133
 960 PB 2.6
 * LS 85
 * UD 0.30
 961 LS 95
 962 UD .24
 *

 963 KK V18-19 DOUBLE DIAMOND VILLAGES 18 & 19
 964 BA .0548
 965 LS 92
 966 UD 0.24

 967 KK V20 DOUBLE DIAMOND VILLAGE 20
 968 BA 0.0450
 969 LS 92
 970 UD 0.21

 971 KK WET WETLANDS # 5 & #6 BETWEEN VILLAGES 18/19 AND VILLAGE 20
 972 BA .0153
 973 LS 80
 974 UD 0.26

 975 KK CB WET COMBINE W18RB, V18-19, V20, & WET RUNOFF HYDROGRAPHS IN THE WETLAND
 976 KM BETWEEN VILLAGES 18/19 AND VILLAGE 20
 977 HC 4

 978 KK PH-IV PHASE IV DOUBLE DIAMOND DEVELOPMENT (VILLAGES 7,8,9,21,22,&23).
 979 KM VILLAGE 20 WAS MODELED ABOVE WITH FLOW ENTERING THE WETLAND SOUTH
 980 KM OF WILBUR MAY BLVD. DETAILED DRAINAGE PLANS WERE NOT AVAILABLE
 981 KM AND AS A RESULT THE PHASE IV VILLAGES LIST FOR PH-IV WERE COMBINED.
 982 KM AS PLANS ARE DEVELOPED, THE VILLAGES CAN BE MODELED SEPARATELY.
 983 BA 0.1931
 984 LS 92
 985 UD 0.31

 986 KK E14 HYDROGRAPH FROM VILLAGE 6 DRAINAGE POINT E14
 987 KM CALCULATE RUNOFF FROM SUBBASIN E14
 988 BA .025

989 LS 92
 990 UD .225
 991 KK C14
 992 KM COMBINE RUNOFF FROM E14 WITH CENTRAL CHANNEL FLOW (FLOW FROM RT1617 & PH-IV)
 993 HC 3

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

994 KK E14-E1
 995 KM ROUTE FLOW TO E1 ALONG CENTRAL CHANNEL
 996 RD 400 .004 .030 TRAP 100 3

997 KK E1
 998 KM CALCULATE RUNOFF FROM SUBBASIN E1-VILLAGE 5
 999 BA .0058
 1000 LS 92
 1001 UD .135

1002 KK C1
 1003 KM COMBINE RUNOFF FROM E1 WITH CENTRAL CHANNEL FLOW
 1004 HC 2

1005 KK E1-E2
 1006 KM ROUTE FLOW TO E2 ALONG CENTRAL CHANNEL
 1007 RD 300 .004 .030 TRAP 100 3

1008 KK E2
 1009 KM CALCULATE RUNOFF FROM SUBBASIN E2-VILLAGE 5
 1010 BA .003
 1011 LS 92
 1012 UD .118

1013 KK C2
 1014 KM COMBINE RUNOFF FROM E2 WITH CENTRAL CHANNEL FLOW
 1015 HC 2

1016 KK E2-E3
 1017 KM ROUTE FLOW TO E3 ALONG CENTRAL CHANNEL
 1018 RD 300 .004 .030 TRAP 100 3

1019 KK E3
 1020 KM CALCULATE RUNOFF FROM SUBBASIN E3-VILLAGE 5
 1021 BA .0025
 1022 LS 92
 1023 UD .119

1024 KK C3
 1025 KM COMBINE RUNOFF FROM E3 WITH CENTRAL CHANNEL FLOW
 1026 HC 2

1027 KK E3-E4
 1028 KM ROUTE FLOW TO E4 ALONG CENTRAL CHANNEL
 1029 RD 360 .004 .030 TRAP 100 3

1030 KK E4
 1031 KM CALCULATE RUNOFF FROM SUBBASIN E4-VILLAGE 5
 1032 BA .003
 1033 LS 92
 1034 UD .113

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1035 KK C4
 1036 KM COMBINE RUNOFF FROM E4 WITH CENTRAL CHANNEL FLOW
 1037 HC 2

1038 KK D10
 1039 KM CALCULATE RUNOFF FROM SUBBASIN D10
 1040 KM SUBBASIN D10 IS LOCATED ALONG DOUBLE DIAMOND PKWY. THE AREA DRAINED IS
 1041 KM COMPRISED OF PORTIONS OF VILLAGES 5, 6, 13, 14, 15, 16 & 17 THAT BORDER THE PKWY.
 1042 KM THE D10 SYSTEM IS A PARALLEL STORM DRAIN SYSTEM
 1043 KM ALONG DOUBLE DIAMOND PARKWAY THAT DRAINS TO AN OPEN
 1044 KM CHANNEL ALONG THE SOUTH EDGE OF THE PARK LOCATED IMMEDIATELY SOUTHEAST OF
 1045 KM THE INTERSECTION OF CARAT AV. AND DOUBLE DIAMOND PKWY.
 1046 BA .122
 1047 LS 92
 1048 UD .277

1049 KK D12
 1050 KM CALCULATE RUNOFF FROM SUBBASIN D12-VILLAGE 5
 1051 BA 0.0166
 1052 LS 92
 1053 UD 0.173

1054 KK PARK
 1055 KM CALCULATE RUNOFF FROM PARK JUST SOUTH OF CARAT AVE
 1056 BA .0078
 1057 LS 80
 1058 UD .14

1059 KK C10PRK
 1060 KM COMBINE HYDROGRAPHS FROM PARK, D10, D12 AND CENTRAL CHANNEL
 1061 HC 4

1062 KK PK-CAR
 1063 KM ROUTE FLOW TO STATION ~62+20 ALONG CENTRAL CHANNEL
 1064 RD 720 .004 .030 TRAP 100 3

1065 KK PHVa PHASE V SUB-BASIN a
 1066 BA 0.011
 1067 LS 92
 1068 UD 0.16

1069 KK V4 DOUBLE DIAMOND VILLAGE 4 OF PHASE I
1070 BA 0.026
1071 LS 86
1072 UD 0.16

1073 KK CB 1 COMBINE PhVa AND V4 AT STATION ~62+20
1074 HC 3

HEC-1 INPUT

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1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1075 KK RT1-2
1076 KM ROUTE TO CB 2 AT STATION ~74+65
1077 RD 1245 .004 0.04 TRAP 100 3

1078 KK PhVb DOUBLE DIAMOND PHASE V AREA PhVb
1079 BA 0.028
1080 LS 92
1081 UD 0.23

1082 KK CB2 COMBINE PhVb WITH CENTRAL CHANNEL FLOW AT STATION ~74+65
1083 HC 2

1084 KK RT2-3 ROUTE CB2 DOWN CENTRAL CHANNEL TO CB 3 AT STATION ~79+00
1085 RD 435 .00204 0.04 TRAP 100 3

1086 KK V12 PORTION OF VILLAGE 12 THAT DRAINS TO CENTRAL CHANNEL
1087 BA 0.015
1088 LS 86
1089 UD 0.16

1090 KK V11 PORTION OF VILLAGE 11 THAT DRAINS TO CENTRAL CHANNEL
1091 BA 0.008
1092 LS 86
1093 UD 0.12

1094 KK V3 PHASE I VILLAGE 3
1095 BA 0.026
1096 LS 86
1097 UD 0.19

1098 KK CB3 COMBINE PORTIONS OF VILLAGES 11&12 WITH VILLAGE 3 AT STA 79+00
1099 HC 4

1100 KK RT3-4
1101 KM ROUTE CB3 DOWN CENTRAL CHANNEL TO CB4 AT STATION ~82+00
1102 RD 300 0.00204 0.04 TRAP 100 3

1103 KK PhVc PHASE V SUB-AREA PhVc
1104 BA 0.022
1105 LS 92
1106 UD 0.19

1107 KK V2 VILLAGE 2 OF PHASE I
1108 BA 0.04
1109 LS 86
1110 UD 0.20

1111 KK CB4 COMBINE PhVc WITH VILLAGE 2
1112 HC 3

HEC-1 INPUT

PAGE 38

1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1113 KK RT4-5 ROUTE CB4 DOWN CENTRAL CHANNEL TO CB5 AT STATION ~83+65
1114 RD 165 0.00204 0.04 TRAP 100 3

1115 KK PARKVI PHASE VI PARK
1116 BA 0.004
1117 LS 80
1118 UD 0.14

1119 KK CB5 COMBINE PHASE VI PARK WITH CENTRAL CHANNEL FLOW AT CB5
1120 HC 2

1121 KK RT5-6 ROUTE CB5 DOWN CENTRAL CHANNEL TO CB6 AT STATION ~87+50
1122 RD 385 0.00204 0.04 TRAP 100 3

1123 KK K6SCHL PHASE VI K-6 SCHOOL
1124 BA 0.013
1125 LS 85
1126 UD 0.15

1127 KK CB6 COMBINE K-6 SCHOOL WITH CENTRAL CHANNEL FLOW AT CB6
1128 HC 2

1129 KK RT6-7 ROUTE CB6 DOWN CENTRAL CHANNEL TO CB7 AT STATION ~101+00
1130 KM END OF CENTRAL CHANNEL
1131 RD 1350 .00204 0.04 TRAP 100 3

1132 KK V1 PHASE I VILLAGE 1
1133 BA 0.037
1134 LS 86
1135 UD 0.21

1136 KK V29 PHASE VI VILLAGE 29
1137 BA 0.065
1138 LS 92
1139 UD 0.20

1140 KK CB7 COMBINATION POINT 7; END OF CENTRAL CHANNEL
1141 HC 3

* WHITES CREEK BRANCHES 1 & 2

1142	KK	DR 1	Recall Channel 1 Hydrograph (@ Difffluence)
1143	DR	CH 1	
1144	KK	RT Z1	Route Channel 1 to Zolezzi Lane (approx. 2800' West of Virginia St.)
1145	RM	4	.34 .3
1146	KK	W13R	Whites Creek No. 13
1147	BA	1.3	
1148	PB	2.8	
1149	LS		61
1150	UD	0.52	

HEC-1 INPUT

PAGE 39

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1151	KK	CP Z1	Combine channel 1 w/ W13R at Zolezzi Lane
1152	HC	2	
1153	KK	DV 1B	Divert flows to the north of Zolezzi (Channel 1A)
1154	KM		Hydrograph is for flows along Zolezzi (Channel 1B, Ea. to Virginia)
1155	DT	CH 1A	
1156	DI	0	200 1500
1157	DQ	0	200 200
1158	KK	RT V12	Route Channel 1B to Virginia St.
1159	RM	1	0.12 .25
1160	KK	W12R	Whites Creek No. 12
1161	BA	0.6	
1162	PB	2.8	
1163	LS		61
1164	UD	0.45	
1165	KK	CP V12	Combine Channel 1B and W12R at int. of Virginia and Zolezzi
1166	HC	2	
1167	KK	DR CH2	Recall Channel 2 Hydrograph
1168	DR	CH 2	
1169	KK	RT V12	Route Flows to int. of Virginia and Zolezzi
1170	RM	3	.221 .2
1171	KK	CP V12	Combine channels 1B and 2 at int. of Virginia and Zolezzi
1172	HC	2	
1173	KK	RT F12	Route flows to proposed RCB at 580 (Channels 1B and 2)
1174	RM	2	0.201 0.2
1175	KK	W15R	Whites Creek No. 15
1176	BA	0.21	
1177	PB	2.7	
1178	LS		79
1179	UD	0.21	
1180	KK	CP F12	Combine flows at proposed RCB at 580 (Channels 1B and 2)
1181	HC	2	
1182	KK	DR 1A	Recall Channel 1A Hydrograph
1183	DR	CH 1A	
1184	KK	RT F1A	Route flows to proposed RCB at 580 (Channel 1A)
1185	RM	4	0.306 0.2
1186	KK	W14R	Whites Creek No. 14
1187	BA	0.18	
1188	PB	2.7	
1189	LS		77
1190	UD	0.26	

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1191	KK	CP F1A	Combine flows at proposed RCB at 580 (Channel 1A)
1192	HC	2	
1193	KK	CB 1&2	COMBINE WHITES CREEK BRANCHES 1 & 2 @ I-580
1194	HC	2	
	*		ROUTE WHITES CREEK BRANCHES 1 & 2 TO THE CONFLUENCE W/ LUMBERJACK CHANNEL
1195	KK	RT WT2	ROUTE WHITES 1&2 THRU WS WT2P - CHANNEL "A"
1196	RD	3040	0.0026 0.035 TRAP 135 5
1197	KK	RT WT2	ROUTE WHITES 1&2 THRU WS WT2P- PARK AND OPEN SPACE
1198	RM	5	0.44 0.20
1199	KK	RT WT2	ROUTE WHITES CREEK 1&2 THRU WS WT2P - CHANNEL "B"
1200	RD	1914	0.0028 0.035 TRAP 151 3
1201	KK	WT 6P1	PORTION OF PHASE I VILLAGES 11, 12, & 13 DRAINING TO "B" CHANNEL
1202	BA	0.07	
1203	PB	2.7	
1204	LS		83
1205	UD	0.38	
1206	KK	W WT2P	ON-SITE WATERSHED WT2P
	*		EXISTING CONDITION(NO ON-SITE DETENTION)
1207	BA	0.59	
1208	PB	2.7	
1209	LS		79
1210	UD	0.73	
1211	KK	CB WT2	COMBINE WHITES CREEK 1&2 & WT2P
1212	HC	3	
1213	KK	WS WT1	WATERSHED WT1 - AREAS BETWEEN WHITES CREEK AND THOMAS CREEK

1214 BA 1.93
 1215 PB 2.75
 1216 LS 66
 1217 UD 0.97

1218 KK RT WT3 ROUTE TO CONFLUENCE
 1219 RM 3 0.29 0.25

1220 KK THOMAS
 1221 KO 3
 1222 KM HYDROGRAPH FROM FIS HYDROLOGY MODEL - THOM100.901
 1223 KM THOMAS CREEK PEAK FLOW @ S. VIRGINIA STREET
 1224 BA 11.54
 1225 QI 0 0 0 0 0 0 0 0 0 0
 1226 QI 0 0 0 0 0 0 0 0 0 0
 1227 QI 0 0 0 0 0 0 0 0 0 0
 1228 QI 0 0 0 0 0 0 0 0 2 6
 1229 QI 20 29 41 54 70 89 112 144 203 385
 1230 QI 790 1223 1828 2544 2447 1943 1462 1170 1019 933
 1231 QI 873 825 786 756 729 698 665 636 613 594
 1232 QI 577 562 549 535 521 504 481 445 407 379

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1233 QI 362 350 341 334 327 321 316 310 305 300
 1234 QI 295 291 287 282 278 275 271

1235 KK DV HOL
 1236 KO 3
 1237 KM SPLIT FLOW ACROSS HOLCOME LANE TO NORTH.
 1238 KM REFER TO FIS HEC-2 MODEL FOR THOMAS CREEK - THOMAS A.DAT
 1239 KM SPLIT FLOW RATING CALCULATED USING THOMAS A.DAT
 1240 DT HOLCOM
 1241 DI 0 1000 2000 2550 3000 4000
 1242 DQ 0 274 955 1385 1746 2562

1243 KK RT WT3 ROUTE TO OPEN SPACE/WETLAND
 1244 RM 2 0.167 0.25

1245 KK DV THO THOMAS CREEK DIVERSION AT WETLAND/OPEN SPACE
 1246 DT THOM
 1247 DI 0 500 1000 1465
 1248 DQ 0 0 0 159

1249 KK RT WT3 ROUTE TO CONFLUENCE
 1250 RM 1 0.083 0.25

1251 KK WT3P WATERSHED WT3P - EXISTING CONDITION (NO ON-SITE DETENTION)
 1252 BA 0.49
 1253 PB 2.7
 1254 LS 79
 1255 UD 0.33

1256 KK CB WT3 COMBINE OFFSITE FLOWS -WT1 & THOMAS CREEK & WT3P
 * KO 1
 1257 HC 3

1258 KK CB OFF COMBINE WHITES CREEK 1&2 & THOMAS CREEK
 1259 HC 2

1260 KK RT WHC ROUTE THRU WHITES CHANNEL "C"
 1261 RD 1689 0.0021 0.035 TRAP 150 3

1262 KK D2 BELLA VISTA RANCH WATERSHED 2
 1263 KM CALCULATE RUNOFF FROM WATERSHED 2
 1264 BA 0.36
 1265 PB 2.5
 1266 LS 70
 1267 UD 0.49

1268 KK CB WHC COMBINE WHITES CREEK BRANCHES 1,2,3,&4 & THOMAS CREEK
 1269 HC 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1270 KK RT DET ROUTE TO DETENTION BASIN THRU PROPOSED CHANNEL
 1271 RD 1985 0.00275 0.035 TRAP 170 3
 * ROUTE THRU DETENTION BASIN

1272 KK RT DET
 1273 RS 1 FLOW -1
 * AS-BUILT VOLUME - PHASE 1
 1274 SV 0 16.64 41.62 72.60 123.04 170.39 216.38 238.26
 * PHASE 2 VOLUME - W/O ARCHEOLOGICAL SITE
 1275 SE 4422.7 4424.09 4425.20 4426.25 4427.55 4428.60 4429.52 4429.94
 1276 SQ 0 200 500 1000 2000 3000 4000 4500

1277 KK RT WT ROUTE TO CP WT
 1278 RM 1 0.06 0.15

1279 KK THOMAS RECALL DIVERSION FROM THOMAS CREEK
 1280 DR THOM

1281 KK RT WT ROUTE TO NORTHEAST PROP
 1282 RM 19 1.59 0.2

1283 KK WT4P ON-SITE WATERSHED WP4P
 * EXISTING CONDITION (NO ON-SITE DETENTION)
 1284 BA 1.73
 1285 PB 2.7
 1286 LS 82

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1287      UD      1.62
1288      KK
1289      HC        2
          *
1290      KK      WT7P  ON-SITE WATERSHED WT7P
          * EXISTING CONDITIONS
1291      BA      0.16
1292      PB      2.7
1293      LS              80
1294      UD      1.48
1295      KK      RT WT  ROUTE TO CP WT
1296      RM      8      0.65  0.15
1297      KK      WS WTS  WATERSHED WTS
1298      BA      0.49
1299      PB      2.65
1300      LS              83
1301      UD      0.28

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HEC-1 INPUT

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1
LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1302      KK      RT WT  ROUTE TO CP WT
1303      RM      6      0.47  0.15
1304      KK      CB WT  COMBINE FLOWS AT NORTHEAST PROPERTY CORNER
1305      HC              3
1306      KK      CP WT  COMBINE ALL FLOWS @ CP WT
1307      HC              2
          *
          * FLOW FROM DOUBLE DIAMOND ONTO BELLA VISTA RANCH NORTH OF THE NARROWS
          *
1308      KK      PT03  COMBINE FLOW FROM WATERSHED 2 WITH RT03 AND DOUBLE DIAMOND FLOWS
1309      HC              4
1310      KK      RT04  ROUTE TOTAL FLOW TO CONFLUENCE WITH WATERSHEDS 1 & 5, & DD
1311      RM      11     1.77  0.1
1312      KK      D1    BELLA VISTA RANCH WATERSHED 1
1313      KM      CALCULATE RUNOFF FROM WATERSHED 1
1314      BA      0.44
1315      PB      2.5
1316      LS              77
1317      UD      0.60
1318      KK      D5    BELLA VISTA RANCH WATERSHED 5
1319      KM      CALCULATE RUNOFF FROM WATERSHED 5
1320      BA      1.21
1321      PB      2.4
1322      LS              74
1323      UD      5.36
1324      KK      PT04  COMBINE FLOWS FROM WSD 1 & 5 WITH ROUTED FLOW FROM PT03
1325      KO      3
1326      HC      3
          *
1327      ZZ

```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

1
INPUT LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW
50      W1R
      .
      .
65      .      W2R
      .
      .
70      W1+W2.....
      V
      V
72      RT-A
      .
      .
74      .      W3R
      .      V
      .      V
79      .      RT-A
      .
      .
81      .      W4R
      .
      .
86      W1234.....
      V
      V
88      RT-B
      .
      .
90      .      W5R
      .
      .
95      W5+CH.....
      V
      V
97      RT-C
      .
      .
99      .      W6R

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104 W6+CH .....
      V
      V
106 RT-D
      .
      .
108 W7R
      .
      .
113 W7+CH .....
      V
      V
115 RT-DIF
      .
      .
117 W8R
      .
      .
122 CP DIF .....
      .
      .
126 -----> CH 123
124 DV 4
      V
      V
129 RT W4
      .
      .
131 W17R
      .
      .
136 CP W4 .....
      V
      V
138 RT F4
      .
      .
140 W19R
      .
      .
145 W9R
      V
      V
150 RT F4
      .
      .
152 CP F4 .....
      V
      V
154 RT V4
      .
      .
156 W20R
      .
      .
161 CP V4 .....
      V
      V
163 RT SIM
      .
      .
165 G1G2
      V
      V
170 OUTJ1
      .
      .
172 J1
      .
      .
177 OUTJ1 .....
      V
      V
179 OUTG3
      .
      .
181 G3
      .
      .
186 OUTG3 .....
      V
      V
188 OUT30
      .
      .
190 15
      V
      V
195 OUT30
      .
      .
197 30
      .
      .
203 OUT30 .....
      V
      V
205 OUT40
      .
      .
207 35
      .
      .
213 40
      .
      .

```

```

218 . . . . . OUT40 .....
      . . . . . V
220 . . . . . OUT341
      . . . . . V
225 . . . . . C-1B
      . . . . .
230 . . . . . C-1A
      . . . . . V
234 . . . . . RT C1
      . . . . . V
236 . . . . . RT C1
      . . . . . V
238 . . . . . CPC1B .....
      . . . . .
240 . . . . . CB CUR .....
      . . . . . V
242 . . . . . OUTDS
      . . . . . V
244 . . . . . CB DS .....
      . . . . . V
246 . . . . . RT WHT
      . . . . . V
249 . . . . . <----- CH 123
248 . . . . . DR 123
      . . . . .
252 . . . . . -----> CH 1
250 . . . . . DV 2&3
      . . . . . V
255 . . . . . RT 2&3
      . . . . . V
257 . . . . . W10R
      . . . . .
262 . . . . . CP 23 .....
      . . . . .
266 . . . . . -----> CH 2
264 . . . . . DV 23A
      . . . . . V
269 . . . . . RT V3
      . . . . .
271 . . . . . W11R
      . . . . .
276 . . . . . CP V24 .....
      . . . . . V
278 . . . . . RT F3
      . . . . . V
280 . . . . . W16R
      . . . . .
285 . . . . . CP F3 .....
      . . . . . V
287 . . . . . RT DSW
      . . . . . V
289 . . . . . W16RA
      . . . . .
294 . . . . . CB DSW .....
      . . . . .
296 . . . . . S-1
      . . . . . V
301 . . . . . RT S3
      . . . . . V
303 . . . . . S-2
      . . . . . V
307 . . . . . RT S3
      . . . . . V
309 . . . . . S-3A
      . . . . . V
313 . . . . . RT S3
      . . . . . V
315 . . . . . CPS3A .....
      . . . . . V
317 . . . . . RT S5
      . . . . . V
319 . . . . . S-3B

```



```

448 . . . . . A19
452 . . . . . A20
456 . . . . . CHNL-F
459 . . . . . STM+AF
462 . . . . . APTS-9
468 . . . . . A8
472 . . . . . CHNL-B
474 . . . . . D12&13
479 . . . . . A9
483 . . . . . CHNL-C
486 . . . . . B&C
489 . . . . . A14
493 . . . . . A13
497 . . . . . A15
501 . . . . . CHNL-D
504 . . . . . A11
508 . . . . . A12
512 . . . . . 11+12
515 . . . . . CHNL D
518 . . . . . X12+13
524 . . . . . A10
528 . . . . .
530 . . . . . A21
534 . . . . . WTLNDS
539 . . . . . <----- BAS 1
537 . . . . . RC BAS
. . . . . V
. . . . . V
540 . . . . . BAS 1
. . . . .
551 . . . . . -----> 36DIVQ
550 . . . . . BAS1DS
. . . . . V
. . . . . V
554 . . . . . POND2
. . . . .
558 . . . . . T-1
. . . . . V
. . . . . V
563 . . . . . RT T2
. . . . .
565 . . . . . T-2
. . . . .
570 . . . . . CPT2
. . . . . V
. . . . . V
572 . . . . . RT T3
. . . . .
574 . . . . . T-3
. . . . .
579 . . . . . CPT3

```

581	CPDIA				
	V				
583	RT WT				
585		WSF1			
590			WSE1		
595		FIE1			
597			C-2		
			V		
602			RT C3		
604				C-1C	
				V	
609				RT C3	
611					C-3
616	CPC3				
	V				
618	RT C4				
620			C-4		
625	CPC4				
	V				
627	RT C7				
	V				
629	RT C7				
631			C-5		
			V		
636			RT C7		
			V		
638			RT C7		
640				C-7	
645					C-6
					V
650					RT C7
					V
652					RT C7
					V
654					RT C7
					V
656	CPC7				
	V				
658	RT WT				
660			W-1		
			V		
665			RT W1		
667	CPWET				
	V				
669	RT W1				
671		E2A			
677			SE-2		
			V		
682			RT S3		
684				SE-3	
689					SE-1
					V
694					RT S3

802	.	.	.	CPB12.....	.
	.	.	.	V	.
	.	.	.	V	.
804	.	.	.	RT E3	.
	.	.	.	V	.
	.	.	.	V	.
806	.	.	.	RT E3	.
	.	.	.	V	.
	.	.	.	V	.
808	.	.	.	RT E4	.

810	E-4
	V
816	V
	.	.	.	RT E4	.

818	.	.	.	CPE4.....	.

820	.	.	.	W-8	.

825	.	.	.	CPWETO.....	.
	.	.	.	V	.
	.	.	.	V	.
827	.	.	.	RS DT2	.

840	.	.	.	W-9	.

845	.	.	.	CW-9.....	.
	.	.	.	V	.
	.	.	.	V	.
848	.	.	.	POND4	.

857	.	.	.	WET-IN.....	.

860	.	.	.	D1	.
	.	.	.	V	.
	.	.	.	V	.
865	.	.	.	RT N1	.
	.	.	.	V	.
	.	.	.	V	.
867	.	.	.	RT N1	.
	.	.	.	V	.
	.	.	.	V	.
869	.	.	.	RT N1	.

871	.	.	.	WSC	.
	.	.	.	V	.
	.	.	.	V	.
876	.	.	.	RT N1	.
	.	.	.	V	.
	.	.	.	V	.
878	.	.	.	RT N1	.

880	NE-1
	V
	V
885	.	.	.	RT N1	.

887	.	.	.	CPNE1.....	.
	.	.	.	V	.
	.	.	.	V	.
889	.	.	.	RT W3	.
	.	.	.	V	.
	.	.	.	V	.
891	.	.	.	RT W3	.

893	.	.	.	D2	.
	.	.	.	V	.
	.	.	.	V	.
898	.	.	.	RT N4	.
	.	.	.	V	.
	.	.	.	V	.
900	.	.	.	RT N4	.
	.	.	.	V	.
	.	.	.	V	.
902	.	.	.	RT N4	.

904	NE2345

911	.	.	.	CPNE4.....	.
	.	.	.	V	.
	.	.	.	V	.
914	.	.	.	RT W3	.

916	.	.	.	CPWET3.....	.
	.	.	.	V	.
	.	.	.	V	.
919	.	.	.	RT DN	.

921	.	.	.	DMNTE.....	.

924	.	.	N-1	.	.
	.	.	V	.	.
	.	.	V	.	.
929	.	.	RT N13	.	.
	.	.	V	.	.
	.	.	V	.	.
931	.	.	RT N13	.	.
	.	.	V	.	.
	.	.	V	.	.
933	.	.	RT01	.	.

935	.	.	.	D4	.

941	.	.	PT01.....	.	.
	.	.	V	.	.
	.	.	V	.	.
943	.	.	RT02	.	.

945	.	.	.	D3	.

951	.	.	PT02.....	.	.
	.	.	V	.	.
	.	.	V	.	.
953	.	.	RT03	.	.

955	.	.	#18RB	.	.

963	.	.	.	V18-19	.

967	V20

971	WET

975	.	.	CB WET.....	.	.

978	.	.	.	PH-IV	.

986	E14

991	.	.	C14.....	.	.
	.	.	V	.	.
	.	.	V	.	.
994	.	.	E14-E1	.	.

997	.	.	.	E1	.

1002	.	.	C1.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1005	.	.	E1-E2	.	.

1008	.	.	.	E2	.

1013	.	.	C2.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1016	.	.	E2-E3	.	.

1019	.	.	.	E3	.

1024	.	.	C3.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1027	.	.	E3-E4	.	.

1030	.	.	.	E4	.

1035	.	.	C4.....	.	.

1038	.	.	.	D10	.

1049	D12

1054	PARK

1059	.	.	C10PRK.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1062	.	.	PK-CAR	.	.

1065	.	.	.	PhVa	.

1069	V4
1073
1075	.	.	CB 1
	.	.	V	.	.
1078	.	.	V	.	.
	.	.	RT1-2	.	.
1082	PhVb
1084
	.	.	CB2
	.	.	V	.	.
1086	.	.	V	.	.
	.	.	RT2-3	.	.
1090	V12
1094
	V11
1098
	.	.	CB3	V3
	.	.	V	.	.
1100	.	.	V	.	.
	.	.	RT3-4	.	.
1103	PhVc
1107
	V2
1111	.	.	CB4
	.	.	V	.	.
1113	.	.	V	.	.
	.	.	RT4-5	.	.
1115	PARKVI
1119
	.	.	CB5
	.	.	V	.	.
1121	.	.	V	.	.
	.	.	RT5-6	.	.
1123	K6SCHL
1127
	.	.	CB6
	.	.	V	.	.
1129	.	.	V	.	.
	.	.	RT6-7	.	.
1132	V1
1136
	V29
1140
	.	.	CB7
1143
1142	<----- CH 1
	.	.	DR 1	.	.
	.	.	V	.	.
1144	.	.	V	.	.
	.	.	RT Z1	.	.
1146	W13R
1151
	.	.	CP Z1
1155
1153	-----> CH 1A
	.	.	DV 1B	.	.
	.	.	V	.	.
1158	.	.	V	.	.
	.	.	RT V12	.	.
1160	W12R
1165
	.	.	CP V12
1168
1167	<----- CH 2
	.	.	DR CH2	.	.
	.	.	V	.	.
1169	.	.	V	.	.
	.	.	RT V12	.	.

1171	CP V12.....		
	V		
1173	RT F12		
	V		
1175		W15R	
	V		
1180	CP F12.....		
	V		
1183			<----- CH 1A
1182	DR 1A		
	V		
1184	RT F1A		
	V		
1186		W14R	
	V		
1191	CP F1A.....		
	V		
1193	CB 1&2.....		
	V		
1195	RT WT2		
	V		
1197	RT WT2		
	V		
1199	RT WT2		
	V		
1201		WT 6P1	
	V		
1206			W WT2P
	V		
1211	CB WT2.....		
	V		
1213	WS WT1		
	V		
1218	RT WT3		
	V		
1220		THOMAS	
	V		
1240			>----- HOLCOM
1235	DV HOL		
	V		
1243	RT WT3		
	V		
1246			>----- THOM
1245	DV THO		
	V		
1249	RT WT3		
	V		
1251			WT3P
	V		
1256	CB WT3.....		
	V		
1258	CB OFF.....		
	V		
1260	RT WHC		
	V		
1262		D2	
	V		
1268	CB NHC.....		
	V		
1270	RT DET		
	V		
1272	RT DET		
	V		
1277	RT WT		
	V		
1280			<----- THOM
1279	THOMAS		
	V		
1281	RT WT		
	V		
1283			WT4P
	V		
1288			

QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 27JUL 0 STARTING DATE
ITIME 0005 STARTING TIME
NQ 288 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 28JUL 0 ENDING DATE
NDTIME 0000 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 23.92 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.94

*** **

350 KK *****
* DIVSTR * STAGE, STORAGE, AND DISCHARGE FROM DIVERSION POND
* *

352 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

353 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 4475.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

Table with 12 columns: AREA, ELEVATION, DISCHARGE, and 9 unlabeled columns. Rows include 354 SA, 356 SE, and 358 SQ.

COMPUTED STORAGE-ELEVATION DATA

Table with 12 columns: STORAGE, ELEVATION, and 10 unlabeled columns. Rows show computed values for storage and elevation.

*** WARNING *** MODIFIED PULS ROUTING MAY BE NUMERICALLY UNSTABLE FOR OUTFLOWS BETWEEN 0. TO 10364.
THE ROUTED HYDROGRAPH SHOULD BE EXAMINED FOR OSCILLATIONS OR OUTFLOWS GREATER THAN PEAK INFLOWS.
THIS CAN BE CORRECTED BY DECREASING THE TIME INTERVAL OR INCREASING STORAGE (USE A LONGER REACH.)

*** **

HYDROGRAPH AT STATION DIVSTR
FOR PLAN 1, RATIO = .94

Table with 5 columns: PEAK FLOW, TIME, 6-HR, 24-HR, 72-HR, 23.92-HR. Rows include peak flow, storage, and stage data.

CUMULATIVE AREA = 71.27 SQ MI

*** **

```

*****
*           *
534 KK      * WTLNDS * DISCHARGE TO WETLANDS
*           *
*****

```

```

535 KO      OUTPUT CONTROL VARIABLES
            IPRNT      3 PRINT CONTROL
            IPLOT      0 PLOT CONTROL
            QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

536 HC      HYDROGRAPH COMBINATION
            ICOMP      3 NUMBER OF HYDROGRAPHS TO COMBINE

```

HYDROGRAPH AT STATION WTLNDS
FOR PLAN 1, RATIO = .94

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	23.92-HR	
272.	12.17	107.	42.	42.	42.	
		(INCHES)	2.144	3.351	3.351	3.351
		(AC-FT)	53.	83.	83.	83.

CUMULATIVE AREA = .47 SQ MI

```

*****
*           *
540 KK      * BAS 1 * STAGE, STORAGE, AND DISCHARGE FROM BASIN 1
*           *
*****

```

```

542 KO      OUTPUT CONTROL VARIABLES
            IPRNT      3 PRINT CONTROL
            IPLOT      0 PLOT CONTROL
            QSCAL      0. HYDROGRAPH PLOT SCALE

```

HYDROGRAPH ROUTING DATA

```

543 RS      STORAGE ROUTING
            NSTPS      1 NUMBER OF SUBREACHES
            ITYP      ELEV TYPE OF INITIAL CONDITION
            RSVRIC     4473.00 INITIAL CONDITION
            X          .00 WORKING R AND D COEFFICIENT

```

AREA	19.0	26.3	30.6	32.6	33.7	34.1	34.5	34.8	35.2	35.5	
544 SA	36.0										
546 SE	ELEVATION	4475.00	4476.00	4477.00	4478.00	4479.00	4480.00	4481.00	4482.00	4483.00	4484.00
548 SQ	DISCHARGE	5.	7.	10.	515.	1021.	1523.	2027.	2537.	3059.	3561.
549 SE	ELEVATION	4475.40	4475.92	4476.60	4477.64	4478.54	4479.28	4479.95	4480.59	4481.25	4481.87

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	22.53	50.94	82.55	115.72	149.62	183.90	218.55	253.55	288.91
ELEVATION	4475.00	4476.00	4477.00	4478.00	4479.00	4480.00	4481.00	4482.00	4483.00	4484.00
STORAGE	324.66									
ELEVATION	4485.00									

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	8.14	20.45	22.53	39.06	50.94	70.94	82.55	100.33	115.72
OUTFLOW	5.00	5.00	7.00	7.35	10.00	204.18	515.00	717.35	1021.00	1333.13
ELEVATION	4475.00	4475.40	4475.92	4476.00	4476.60	4477.64	4478.00	4478.54	4479.00	4479.00
STORAGE	125.16	147.92	149.62	169.80	183.90	192.53	214.03	218.55	253.55	288.91
OUTFLOW	1523.00	2027.00	2066.71	2537.00	2861.32	3059.00	3561.00	3666.14	4475.67	5285.19
ELEVATION	4479.28	4479.95	4480.00	4480.59	4481.00	4481.25	4481.87	4482.00	4483.00	4484.00
STORAGE	324.66									
OUTFLOW	6094.72									
ELEVATION	4485.00									

HYDROGRAPH AT STATION BAS 1
FOR PLAN 1, RATIO = .94

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	23.92-HR	
3412.	15.33	1542.	393.	393.	393.	
		(INCHES)	.000	.000	.000	.000

```

              (AC-FT)    765.    776.    776.    776.
PEAK STORAGE  TIME
+ (AC-FT)      (HR)
  208.    15.33
              6-HR    24-HR    72-HR    23.92-HR
              120.    37.    37.    37.
PEAK STAGE    TIME
+ (FEET)      (HR)
  4481.69    15.33
              6-HR    24-HR    72-HR    23.92-HR
              4479.10  4476.31  4476.31  4476.31
CUMULATIVE AREA = .00 SQ MI

```

*** **

```

*****
*
*   POND4
*
*****

```

```

849 KO      OUTPUT CONTROL VARIABLES
            IPRNT      3 PRINT CONTROL
            IPLOT      0 PLOT CONTROL
            QSCAL      0. HYDROGRAPH PLOT SCALE
            ROUTE THRU POND 4 JUST UPSTREAM OF DAMONTE PKWY CULVERT
            OUTLET MODELED AS 5 BOX CULVERTS 4' X 12'

```

HYDROGRAPH ROUTING DATA

```

852 RS      STORAGE ROUTING
            NSTPS      1 NUMBER OF SUBREACHES
            ITYP        STOR TYPE OF INITIAL CONDITION
            RSVRIC      .00 INITIAL CONDITION
            X           .00 WORKING R AND D COEFFICIENT
853 SA      AREA      .0    2.9    6.2    9.2    13.7    18.0    23.0    25.2    25.8
854 SE      ELEVATION  4450.00  4451.00  4452.00  4453.00  4454.00  4455.00  4456.00  4457.00  4458.00
855 SQ      DISCHARGE  0.    200.    500.    950.    1450.    2000.    2500.    2800.
856 SE      ELEVATION  4450.00  4451.08  4452.00  4453.07  4454.06  4455.04  4456.01  4456.70

```

COMPUTED STORAGE-ELEVATION DATA

```

STORAGE      .00    1.06    5.52    13.16    24.54    40.32    60.72    84.78    110.30
ELEVATION    4450.00  4451.00  4452.00  4453.00  4454.00  4455.00  4456.00  4457.00  4458.00

```

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

```

STORAGE      .00    1.06    1.31    5.52    13.16    13.82    24.54    25.37    40.32    41.04
OUTFLOW      .00    185.17  200.00  500.00  920.63  950.00  1419.67  1450.00  1977.53  2000.00
ELEVATION    4450.00  4451.00  4451.08  4452.00  4453.00  4453.07  4454.00  4454.06  4455.00  4455.04

```

```

STORAGE      60.72    77.33    84.78    110.30
OUTFLOW      2494.96  2800.00  2930.27  3364.78
ELEVATION    4456.00  4456.70  4457.00  4458.00

```

*** **

HYDROGRAPH AT STATION POND4
FOR PLAN 1, RATIO = .94

```

PEAK FLOW    TIME
+ (CFS)      (HR)
              6-HR    24-HR    72-HR    23.92-HR
+ 2652.    17.83
              (CFS)
              1686.    522.    522.    522.
              (INCHES)
              2,234    2,759    2,759    2,759
              (AC-FT)
              836.    1032.    1032.    1032.
PEAK STORAGE  TIME
+ (AC-FT)      (HR)
              6-HR    24-HR    72-HR    23.92-HR
+ 69.    17.83
              36.    10.    10.    10.
PEAK STAGE    TIME
+ (FEET)      (HR)
              6-HR    24-HR    72-HR    23.92-HR
+ 4456.36    17.83
              4454.45  4451.53  4451.53  4451.53
CUMULATIVE AREA = 7.01 SQ MI

```

*** **

```

*****
*
*   CPNE4
*
*****
911 KK      COMBINE BSIN D2 AND POD NE-4

```

```

912 KO      OUTPUT CONTROL VARIABLES
            IPRNT      3 PRINT CONTROL

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I PLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

913 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CPNE4
 FOR PLAN 1, RATIO = .94

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	23.92-HR
+ 168.	12.08	25.	25.	10.	10.	10.
		(INCHES)	.616	.968	.968	.968
		(AC-FT)	13.	20.	20.	20.

CUMULATIVE AREA = .38 SQ MI

 * *
 * CPWET3 * COMBINE CPWETO AND CPNE4
 * *

917 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

918 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CPWET3
 FOR PLAN 1, RATIO = .94

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	23.92-HR
+ 811.	13.42	240.	240.	68.	68.	68.
		(INCHES)	.409	.460	.460	.460
		(AC-FT)	119.	134.	134.	134.

CUMULATIVE AREA = 5.46 SQ MI

 * *
 * DMNTE * DOWNSTREAM CP TO SUM DAMONTE FLOW
 * *

922 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

923 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION DMNTE
 FOR PLAN 1, RATIO = .94

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	23.92-HR
+ 2762.	17.83	1885.	1885.	632.	632.	632.
		(INCHES)	1.355	1.810	1.810	1.810
		(AC-FT)	935.	1249.	1249.	1249.

CUMULATIVE AREA = 12.94 SQ MI

1220 KK * THOMAS *

1221 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
HYDROGRAPH FROM FIS HYDROLOGY MODEL - THOM100.901
THOMAS CREEK PEAK FLOW @ S. VIRGINIA STREET

48 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 15 TIME INTERVAL IN MINUTES
JXDATE 27JUL 0 STARTING DATE
JXTIME 5 STARTING TIME

SUBBASIN RUNOFF DATA

1224 BA SUBBASIN CHARACTERISTICS
TAREA 11.54 SUBBASIN AREA

HYDROGRAPH AT STATION THOMAS
FOR PLAN 1, RATIO = .00
PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 23.92-HR
+ 2544. 13.25 1030. 352. 352. 352.
(INCHES) .829 1.131 1.131 1.131
(AC-FT) 511. 696. 696. 696.
CUMULATIVE AREA = 11.54 SQ MI

HYDROGRAPH AT STATION THOMAS
FOR PLAN 1, RATIO = .94
PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 23.92-HR
+ 2544. 13.25 1030. 352. 352. 352.
(INCHES) .829 1.131 1.131 1.131
(AC-FT) 511. 696. 696. 696.
CUMULATIVE AREA = 11.54 SQ MI

1235 KK * DV HOL *

1236 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
SPLIT FLOW ACROSS HOLCOM LANE TO NORTH.
REFER TO FIS HEC-2 MODEL FOR THOMAS CREEK - THOMAS A.DAT
SPLIT FLOW RATING CALCULATED USING THOMAS A.DAT

DT DIVERSION
ISTAD HOLCOM DIVERSION HYDROGRAPH IDENTIFICATION
DI INFLOW .00 1000.00 2000.00 2550.00 3000.00 4000.00
DQ DIVERTED FLOW .00 274.00 955.00 1385.00 1746.00 2562.00

DIVERSION HYDROGRAPH HOLCOM
FOR PLAN 1, RATIO = .94
PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 23.92-HR
+ 1380. 13.25 381. 121. 121. 121.
(INCHES) .307 .389 .389 .389
(AC-FT) 189. 240. 240. 240.
CUMULATIVE AREA = 11.54 SQ MI

HYDROGRAPH AT STATION DV HOL
FOR PLAN 1, RATIO = .94
PEAK FLOW TIME MAXIMUM AVERAGE FLOW

(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	23.92-HR
1164.	13.25		649.	231.	231.	231.
		(INCHES)	.523	.741	.741	.741
		(AC-FT)	322.	456.	456.	456.

CUMULATIVE AREA = 11.54 SQ MI

*** WARNING *** UNIT HYDROGRAPH TRUNCATED FROM 324 TO 300 INTERVALS

*** WARNING *** UNIT HYDROGRAPH TRUNCATED FROM 324 TO 300 INTERVALS

*** **

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*
1324 KK * PT04 * COMBINE FLOWS FROM WSD 1 & 5 WITH ROUTED FLOW FROM PT03
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1325 KO OUTPUT CONTROL VARIABLES
        IPRNT 3 PRINT CONTROL
        IPLOT 0 PLOT CONTROL
        QSCAL 0. HYDROGRAPH PLOT SCALE

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1326 HC HYDROGRAPH COMBINATION
        ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION PT04
FOR PLAN 1, RATIO = .94

PEAK FLOW	TIME	(CFS)	6-HR	24-HR	72-HR	23.92-HR
7126.	17.42		6393.	2504.	2504.	2504.
		(INCHES)	.549	.857	.857	.857
		(AC-FT)	3170.	4949.	4949.	4949.

CUMULATIVE AREA = 108.26 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.94	
HYDROGRAPH AT					
+	W1R	1.36	1	FLOW	809.
				TIME	12.42
HYDROGRAPH AT					
+	W2R	.84	1	FLOW	507.
				TIME	12.42
2 COMBINED AT					
+	W1+W2	2.20	1	FLOW	1317.
				TIME	12.42
ROUTED TO					
+	RT-A	2.20	1	FLOW	1302.
				TIME	12.50
HYDROGRAPH AT					
+	W3R	1.38	1	FLOW	762.
				TIME	12.50
ROUTED TO					
+	RT-A	1.38	1	FLOW	758.
				TIME	12.58
HYDROGRAPH AT					
+	W4R	1.47	1	FLOW	336.
				TIME	12.75
3 COMBINED AT					
+	W1234	5.05	1	FLOW	2361.
				TIME	12.58
ROUTED TO					
+	RT-B	5.05	1	FLOW	2348.
				TIME	12.67
HYDROGRAPH AT					
+	W5R	1.27	1	FLOW	249.
				TIME	12.92
2 COMBINED AT					
+	W5+CH	6.32	1	FLOW	2573.
				TIME	12.67

ROUTED TO					
+	RT-C	6.32	1	FLOW TIME	2536. 12.83
HYDROGRAPH AT					
+	W6R	1.43	1	FLOW TIME	117. 13.50
2 COMBINED AT					
+	W6+CH	7.75	1	FLOW TIME	2617. 12.83
ROUTED TO					
+	RT-D	7.75	1	FLOW TIME	2603. 13.00
HYDROGRAPH AT					
+	W7R	.85	1	FLOW TIME	129. 13.00
2 COMBINED AT					
+	W7+CH	8.60	1	FLOW TIME	2731. 13.00
ROUTED TO					
+	RT-DIF	8.60	1	FLOW TIME	2719. 13.08
HYDROGRAPH AT					
+	W8R	.75	1	FLOW TIME	49. 13.42
2 COMBINED AT					
+	CP DIF	9.35	1	FLOW TIME	2764. 13.08
DIVERSION TO					
+	CH 123	9.35	1	FLOW TIME	2209. 13.08
HYDROGRAPH AT					
+	DV 4	9.35	1	FLOW TIME	555. 13.08
ROUTED TO					
+	RT W4	9.35	1	FLOW TIME	537. 13.25
HYDROGRAPH AT					
+	W17R	.58	1	FLOW TIME	87. 12.25
2 COMBINED AT					
+	CP W4	9.93	1	FLOW TIME	562. 13.25
ROUTED TO					
+	RT F4	9.93	1	FLOW TIME	546. 13.33
HYDROGRAPH AT					
+	W19R	.33	1	FLOW TIME	16. 12.25
HYDROGRAPH AT					
+	W9R	2.39	1	FLOW TIME	335. 12.50
ROUTED TO					
+	RT F4	2.39	1	FLOW TIME	326. 12.67
3 COMBINED AT					
+	CP F4	12.65	1	FLOW TIME	725. 13.33
ROUTED TO					
+	RT V4	12.65	1	FLOW TIME	710. 13.42
HYDROGRAPH AT					
+	W20R	.22	1	FLOW TIME	13. 12.25
2 COMBINED AT					
+	CP V4	12.87	1	FLOW TIME	715. 13.42
ROUTED TO					
+	RT STM	12.87	1	FLOW TIME	714. 13.50
HYDROGRAPH AT					
+	G1G2	8.00	1	FLOW TIME	2018. 14.00
ROUTED TO					
+	OUTJ1	8.00	1	FLOW TIME	2018. 14.08
HYDROGRAPH AT					
+	J1	6.40	1	FLOW TIME	313. 13.67
2 COMBINED AT					
+	OUTJ1	14.40	1	FLOW	2307.

				TIME	14.00
ROUTED TO					
+	OUTG3	14.40	1	FLOW TIME	2306. 14.17
HYDROGRAPH AT					
+	G3	3.90	1	FLOW TIME	285. 13.42
2 COMBINED AT					
+	OUTG3	18.30	1	FLOW TIME	2531. 14.08
ROUTED TO					
+	OUT30	18.30	1	FLOW TIME	2505. 14.67
HYDROGRAPH AT					
+	15	4.20	1	FLOW TIME	410. 14.00
ROUTED TO					
+	OUT30	4.20	1	FLOW TIME	401. 15.33
HYDROGRAPH AT					
+	30	16.70	1	FLOW TIME	2494. 13.92
3 COMBINED AT					
+	OUT30	39.20	1	FLOW TIME	5072. 14.50
ROUTED TO					
+	OUT40	39.20	1	FLOW TIME	5053. 14.75
HYDROGRAPH AT					
+	35	15.30	1	FLOW TIME	2158. 14.33
HYDROGRAPH AT					
+	40	2.50	1	FLOW TIME	416. 13.17
3 COMBINED AT					
+	OUT40	57.00	1	FLOW TIME	7318. 14.58
ROUTED TO					
+	OUT341	57.00	1	FLOW TIME	7314. 14.67
				** PEAK STAGES IN FEET **	
			1	STAGE	4560.87
				TIME	14.67
HYDROGRAPH AT					
+	C-1B	.07	1	FLOW TIME	60. 12.08
HYDROGRAPH AT					
+	C-1A	.06	1	FLOW TIME	4. 12.17
ROUTED TO					
+	RT C1	.06	1	FLOW TIME	4. 12.33
ROUTED TO					
+	RT C1	.06	1	FLOW TIME	4. 12.58
2 COMBINED AT					
+	CPC1B	.13	1	FLOW TIME	60. 12.08
2 COMBINED AT					
+	CB CUR	57.13	1	FLOW TIME	7326. 14.67
ROUTED TO					
+	OUTDS	57.13	1	FLOW TIME	7319. 14.83
2 COMBINED AT					
+	CB DS	70.00	1	FLOW TIME	7546. 14.83
ROUTED TO					
+	RT WHT	70.00	1	FLOW TIME	7538. 14.92
HYDROGRAPH AT					
+	DR 123	.00	1	FLOW TIME	2209. 13.08
DIVERSION TO					
+	CH 1	.00	1	FLOW TIME	452. 13.08
HYDROGRAPH AT					
+	DV 2&3	.00	1	FLOW TIME	1757. 13.08
ROUTED TO					

+	RT 2&3	.00	1	FLOW TIME	1723. 13.33
	HYDROGRAPH AT				
+	W10R	.30	1	FLOW TIME	3. 12.92
	2 COMBINED AT				
+	CP 23	.30	1	FLOW TIME	1727. 13.33
	DIVERSION TO				
+	CH 2	.30	1	FLOW TIME	863. 13.33
	HYDROGRAPH AT				
+	DV 23A	.30	1	FLOW TIME	863. 13.33
	ROUTED TO				
+	RT V3	.30	1	FLOW TIME	851. 13.50
	HYDROGRAPH AT				
+	W11R	.32	1	FLOW TIME	108. 12.17
	2 COMBINED AT				
+	CP V24	.62	1	FLOW TIME	867. 13.50
	ROUTED TO				
+	RT F3	.62	1	FLOW TIME	847. 13.75
	HYDROGRAPH AT				
+	W16R	.11	1	FLOW TIME	65. 12.08
	2 COMBINED AT				
+	CP F3	.73	1	FLOW TIME	856. 13.75
	ROUTED TO				
+	RT DSW	.73	1	FLOW TIME	853. 13.83
	HYDROGRAPH AT				
+	W18RA	.21	1	FLOW TIME	92. 12.25
	2 COMBINED AT				
+	CB DSW	.94	1	FLOW TIME	864. 13.83
	HYDROGRAPH AT				
+	S-1	.04	1	FLOW TIME	14. 7.08
	ROUTED TO				
+	RT S3	.04	1	FLOW TIME	13. 7.25
	HYDROGRAPH AT				
+	S-2	.06	1	FLOW TIME	15. 7.08
	ROUTED TO				
+	RT S3	.06	1	FLOW TIME	13. 7.17
	HYDROGRAPH AT				
+	S-3A	.04	1	FLOW TIME	11. 7.08
	ROUTED TO				
+	RT S3	.04	1	FLOW TIME	10. 7.25
	3 COMBINED AT				
+	CPS3A	.14	1	FLOW TIME	35. 7.25
	ROUTED TO				
+	RT S5	.14	1	FLOW TIME	34. 7.58
	HYDROGRAPH AT				
+	S-3B	.02	1	FLOW TIME	5. 7.08
	ROUTED TO				
+	RT S5	.02	1	FLOW TIME	5. 7.50
	HYDROGRAPH AT				
+	S-4	.02	1	FLOW TIME	6. 7.08
	ROUTED TO				
+	RT S5	.02	1	FLOW TIME	6. 7.25
	HYDROGRAPH AT				
+	S-5	.03	1	FLOW TIME	21. 6.25

ROUTED TO					
+	RT S5	.03	1	FLOW TIME	18. 6.33
	4 COMBINED AT				
+	CPS5	.21	1	FLOW TIME	54. 7.58
ROUTED TO					
+	RT WHT	.21	1	FLOW TIME	54. 7.75
	3 COMBINED AT				
+	CB WHT	71.15	1	FLOW TIME	7986. 14.83
HYDROGRAPH AT					
+	HD	.11	1	FLOW TIME	113. 6.33
	2 COMBINED AT				
+	CP HD	71.27	1	FLOW TIME	7992. 14.83
ROUTED TO					
+	DIVSTR	71.27	1	FLOW TIME	7993. 14.83
				** PEAK STAGES IN FEET **	
			1	STAGE	4488.00
				TIME	14.83
DIVERSION TO					
+	BAS 1	71.27	1	FLOW TIME	3838. 14.83
HYDROGRAPH AT					
+	STEAM	71.27	1	FLOW TIME	4154. 14.83
ROUTED TO					
+	OUTDM	71.27	1	FLOW TIME	4153. 15.00
ROUTED TO					
+	OUTDN	71.27	1	FLOW TIME	4150. 15.17
HYDROGRAPH AT					
+	A7	.04	1	FLOW TIME	16. 12.42
	2 COMBINED AT				
+	STM+7	71.31	1	FLOW TIME	4158. 15.17
HYDROGRAPH AT					
+	A6	.02	1	FLOW TIME	16. 12.17
	2 COMBINED AT				
+	STM+6	71.32	1	FLOW TIME	4166. 15.17
HYDROGRAPH AT					
+	A3	.00	1	FLOW TIME	6. 12.08
	2 COMBINED AT				
+	STM+3	71.33	1	FLOW TIME	4170. 15.17
HYDROGRAPH AT					
+	A2	.02	1	FLOW TIME	22. 12.08
	2 COMBINED AT				
+	STM+2	71.35	1	FLOW TIME	4177. 15.17
HYDROGRAPH AT					
+	A17	.03	1	FLOW TIME	19. 12.08
HYDROGRAPH AT					
+	A18	.04	1	FLOW TIME	20. 12.17
	2 COMBINED AT				
+	CHNL-E	.06	1	FLOW TIME	38. 12.17
	2 COMBINED AT				
+	STM+E	71.41	1	FLOW TIME	4193. 15.17
ROUTED TO					
+	RT NST	71.41	1	FLOW TIME	4191. 15.58
HYDROGRAPH AT					
+	A4	.02	1	FLOW TIME	18. 12.08
HYDROGRAPH AT					
+	A23	.00	1	FLOW TIME	2. 12.33

HYDROGRAPH AT					
+	A1	.01	1	FLOW	12.
				TIME	12.17
HYDROGRAPH AT					
+	A22	.00	1	FLOW	2.
				TIME	12.33
HYDROGRAPH AT					
+	A5	.05	1	FLOW	26.
				TIME	12.17
2 COMBINED AT					
+	CARAT1	.05	1	FLOW	28.
				TIME	12.17
4 COMBINED AT					
+	CHNL-A	.09	1	FLOW	57.
				TIME	12.17
HYDROGRAPH AT					
+	A16	.02	1	FLOW	18.
				TIME	12.08
HYDROGRAPH AT					
+	A19	.04	1	FLOW	22.
				TIME	12.17
HYDROGRAPH AT					
+	A20	.02	1	FLOW	13.
				TIME	12.25
3 COMBINED AT					
+	CHNL-F	.08	1	FLOW	51.
				TIME	12.17
3 COMBINED AT					
+	STM+AF	71.58	1	FLOW	4238.
				TIME	15.58
HYDROGRAPH AT					
+	APTS-9	.03	1	FLOW	24.
				TIME	12.17
HYDROGRAPH AT					
+	A8	.07	1	FLOW	50.
				TIME	12.17
2 COMBINED AT					
+	CHNL-B	.10	1	FLOW	74.
				TIME	12.17
HYDROGRAPH AT					
+	D12&13	.06	1	FLOW	34.
				TIME	12.17
HYDROGRAPH AT					
+	A9	.05	1	FLOW	30.
				TIME	12.17
2 COMBINED AT					
+	CHNL-C	.11	1	FLOW	64.
				TIME	12.17
2 COMBINED AT					
+	B&C	.21	1	FLOW	138.
				TIME	12.17
HYDROGRAPH AT					
+	A14	.05	1	FLOW	32.
				TIME	12.17
HYDROGRAPH AT					
+	A13	.05	1	FLOW	26.
				TIME	12.17
HYDROGRAPH AT					
+	A15	.02	1	FLOW	13.
				TIME	12.17
4 COMBINED AT					
+	CHNL-D	.33	1	FLOW	209.
				TIME	12.17
HYDROGRAPH AT					
+	A11	.01	1	FLOW	12.
				TIME	12.17
HYDROGRAPH AT					
+	A12	.02	1	FLOW	12.
				TIME	12.33
2 COMBINED AT					
+	11+12	.03	1	FLOW	23.
				TIME	12.17
2 COMBINED AT					
+	CHNL D	.36	1	FLOW	232.
				TIME	12.17
HYDROGRAPH AT					
+	X12+13	.08	1	FLOW	27.
				TIME	12.58
HYDROGRAPH AT					
+	A10	.01	1	FLOW	12.

				TIME	12.08
2 COMBINED AT					
+		.09	1	FLOW	37.
				TIME	12.58
HYDROGRAPH AT	A21	.01	1	FLOW	17.
+				TIME	12.08
3 COMBINED AT					
+	WTLNDS	.47	1	FLOW	272.
				TIME	12.17
HYDROGRAPH AT	RC BAS	.00	1	FLOW	3838.
+				TIME	14.83
ROUTED TO					
+	BAS 1	.00	1	FLOW	3412.
				TIME	15.33
				** PEAK STAGES IN FEET **	
			1	STAGE	4481.69
				TIME	15.33
DIVERSION TO					
+	36DIVQ	.00	1	FLOW	61.
				TIME	15.33
HYDROGRAPH AT	BAS1DS	.00	1	FLOW	3351.
+				TIME	15.33
ROUTED TO					
+	POND2	.00	1	FLOW	3319.
				TIME	15.58
HYDROGRAPH AT	T-1	.04	1	FLOW	34.
+				TIME	12.08
ROUTED TO					
+	RT T2	.04	1	FLOW	33.
				TIME	12.08
HYDROGRAPH AT	T-2	.06	1	FLOW	61.
+				TIME	12.08
2 COMBINED AT					
+	CPT2	.10	1	FLOW	95.
				TIME	12.08
ROUTED TO					
+	RT T3	.10	1	FLOW	89.
				TIME	12.17
HYDROGRAPH AT	T-3	.06	1	FLOW	63.
+				TIME	12.08
2 COMBINED AT					
+	CPT3	.16	1	FLOW	152.
				TIME	12.08
2 COMBINED AT					
+	CPD1A	.16	1	FLOW	3341.
				TIME	15.58
ROUTED TO					
+	RT WT	.16	1	FLOW	3316.
				TIME	15.83
HYDROGRAPH AT	WSF1	.77	1	FLOW	335.
+				TIME	12.17
HYDROGRAPH AT	WSE1	2.10	1	FLOW	568.
+				TIME	12.42
2 COMBINED AT					
+	FIE1	2.88	1	FLOW	766.
				TIME	12.25
HYDROGRAPH AT	C-2	.03	1	FLOW	10.
+				TIME	12.08
ROUTED TO					
+	RT C3	.03	1	FLOW	10.
				TIME	12.25
HYDROGRAPH AT	C-1C	.07	1	FLOW	46.
+				TIME	12.08
ROUTED TO					
+	RT C3	.07	1	FLOW	45.
				TIME	12.17
HYDROGRAPH AT	C-3	.03	1	FLOW	10.
+				TIME	12.08
4 COMBINED AT					

+	CPC3	3.01	1	FLOW TIME	828. 12.25
ROUTED TO					
+	RT C4	3.01	1	FLOW TIME	819. 12.25
HYDROGRAPH AT					
+	C-4	.04	1	FLOW TIME	34. 12.08
2 COMBINED AT					
+	CPC4	3.05	1	FLOW TIME	837. 12.25
ROUTED TO					
+	RT C7	3.05	1	FLOW TIME	825. 12.33
ROUTED TO					
+	RT C7	3.05	1	FLOW TIME	811. 12.42
HYDROGRAPH AT					
+	C-5	.07	1	FLOW TIME	59. 12.08
ROUTED TO					
+	RT C7	.07	1	FLOW TIME	58. 12.08
ROUTED TO					
+	RT C7	.07	1	FLOW TIME	57. 12.25
HYDROGRAPH AT					
+	C-7	.03	1	FLOW TIME	28. 12.08
HYDROGRAPH AT					
+	C-6	.13	1	FLOW TIME	34. 12.08
ROUTED TO					
+	RT C7	.13	1	FLOW TIME	34. 12.25
ROUTED TO					
+	RT C7	.13	1	FLOW TIME	34. 12.25
ROUTED TO					
+	RT C7	.13	1	FLOW TIME	34. 12.42
4 COMBINED AT					
+	CPC7	3.27	1	FLOW TIME	892. 12.33
ROUTED TO					
+	RT WT	3.27	1	FLOW TIME	829. 12.58
HYDROGRAPH AT					
+	W-1	.06	1	FLOW TIME	62. 12.08
ROUTED TO					
+	RT W1	.06	1	FLOW TIME	56. 12.17
3 COMBINED AT					
+	CPWET	3.50	1	FLOW TIME	3393. 15.83
ROUTED TO					
+	RT W1	3.50	1	FLOW TIME	3366. 16.08
HYDROGRAPH AT					
+	E2A	2.10	1	FLOW TIME	568. 12.42
HYDROGRAPH AT					
+	SE-2	.06	1	FLOW TIME	14. 12.08
ROUTED TO					
+	RT S3	.06	1	FLOW TIME	14. 12.17
HYDROGRAPH AT					
+	SE-3	.05	1	FLOW TIME	16. 12.08
HYDROGRAPH AT					
+	SE-1	.11	1	FLOW TIME	32. 12.08
ROUTED TO					
+	RT S3	.11	1	FLOW TIME	32. 12.17
3 COMBINED AT					
+	CPSE3	.22	1	FLOW TIME	59. 12.17

ROUTED TO					
+	RT S5	.22	1	FLOW TIME	60. 12.25
HYDROGRAPH AT					
+	SE-4	.02	1	FLOW TIME	5. 12.08
HYDROGRAPH AT					
+	SE-5	.02	1	FLOW TIME	1. 12.00
3 COMBINED AT					
+	CPSE5	.26	1	FLOW TIME	66. 12.25
ROUTED TO					
+	RT S7	.26	1	FLOW TIME	67. 12.33
HYDROGRAPH AT					
+	SE-6	.00	1	FLOW TIME	1. 12.08
ROUTED TO					
+	RT S7	.00	1	FLOW TIME	1. 12.42
HYDROGRAPH AT					
+	SE-7	.10	1	FLOW TIME	104. 12.00
3 COMBINED AT					
+	CPSE7	.36	1	FLOW TIME	123. 12.08
ROUTED TO					
+	RT WI	.36	1	FLOW TIME	121. 12.08
ROUTED TO					
+	RT WI	.36	1	FLOW TIME	123. 12.25
HYDROGRAPH AT					
+	SE-8	.06	1	FLOW TIME	59. 12.08
ROUTED TO					
+	RTWI	.06	1	FLOW TIME	58. 12.08
ROUTED TO					
+	RT WI	.06	1	FLOW TIME	57. 12.25
HYDROGRAPH AT					
+	W-2	.03	1	FLOW TIME	9. 12.08
HYDROGRAPH AT					
+	W-3	.04	1	FLOW TIME	40. 12.08
2 COMBINED AT					
+	CPW2	.07	1	FLOW TIME	49. 12.08
ROUTED TO					
+	RTG WI	.07	1	FLOW TIME	45. 12.08
3 COMBINED AT					
+	PWETIN	.49	1	FLOW TIME	215. 12.25
2 COMBINED AT					
+	CPWETA	2.59	1	FLOW TIME	746. 12.33
ROUTED TO					
+	RT WI	2.59	1	FLOW TIME	712. 12.50
2 COMBINED AT					
+	CPWET1	6.09	1	FLOW TIME	3430. 16.08
ROUTED TO					
+	RTWET1	6.09	1	FLOW TIME	3399. 16.33
HYDROGRAPH AT					
+	WET	.12	1	FLOW TIME	42. 12.25
2 COMBINED AT					
+	CPWETB	6.21	1	FLOW TIME	3406. 16.33
ROUTED TO					
+	RTWETB	6.21	1	FLOW TIME	3375. 16.50
HYDROGRAPH AT					
+	E-2	.07	1	FLOW TIME	45. 12.08

ROUTED TO +	RT E3	.07	1	FLOW TIME	42. 12.17
HYDROGRAPH AT +	E-1	.05	1	FLOW TIME	2. 12.17
ROUTED TO +	RT E3	.05	1	FLOW TIME	2. 12.25
ROUTED TO +	RTE3	.05	1	FLOW TIME	2. 12.42
2 COMBINED AT +	CPE3	.12	1	FLOW TIME	42. 12.17
HYDROGRAPH AT +	WSB2	.12	1	FLOW TIME	68. 12.00
HYDROGRAPH AT +	WSB1	.36	1	FLOW TIME	174. 12.08
2 COMBINED AT +	CPB12	.48	1	FLOW TIME	213. 12.08
ROUTED TO +	RT E3	.48	1	FLOW TIME	211. 12.08
ROUTED TO +	RT E3	.48	1	FLOW TIME	197. 12.17
ROUTED TO +	RT E4	.48	1	FLOW TIME	188. 12.17
HYDROGRAPH AT +	E-4	.10	1	FLOW TIME	71. 12.08
ROUTED TO +	RT E4	.10	1	FLOW TIME	66. 12.08
3 COMBINED AT +	CPE4	.70	1	FLOW TIME	294. 12.17
HYDROGRAPH AT +	W-8	.06	1	FLOW TIME	63. 12.08
3 COMBINED AT +	CPWETO	6.97	1	FLOW TIME	3410. 16.50
ROUTED TO +	RS DT2	6.97	1	FLOW TIME	2805. 17.33
				** PEAK STAGES IN FEET **	
			1	STAGE TIME	4461.21 17.33
HYDROGRAPH AT +	W-9	.04	1	FLOW TIME	42. 12.08
2 COMBINED AT +	CW-9	7.01	1	FLOW TIME	2812. 17.33
ROUTED TO +	PONDA	7.01	1	FLOW TIME	2652. 17.83
				** PEAK STAGES IN FEET **	
			1	STAGE TIME	4456.36 17.83
2 COMBINED AT +	WET-IN	7.48	1	FLOW TIME	2724. 17.83
HYDROGRAPH AT +	D1	1.72	1	FLOW TIME	530. 12.33
ROUTED TO +	RT N1	1.72	1	FLOW TIME	524. 12.33
ROUTED TO +	RT N1	1.72	1	FLOW TIME	520. 12.42
ROUTED TO +	RT N1	1.72	1	FLOW	512.

				TIME	12.42
HYDROGRAPH AT					
+	WSC	3.31	1	FLOW TIME	820. 12.50
ROUTED TO					
+	RT N1	3.31	1	FLOW TIME	810. 12.58
ROUTED TO					
+	RT N1	3.31	1	FLOW TIME	809. 12.58
HYDROGRAPH AT					
+	NE-1	.04	1	FLOW TIME	18. 12.08
ROUTED TO					
+	RT N1	.04	1	FLOW TIME	18. 12.17
3 COMBINED AT					
+	CPNE1	5.07	1	FLOW TIME	1298. 12.50
ROUTED TO					
+	RT W3	5.07	1	FLOW TIME	1280. 12.50
ROUTED TO					
+	RT W3	5.07	1	FLOW TIME	756. 13.50
HYDROGRAPH AT					
+	D2	.15	1	FLOW TIME	102. 12.00
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	88. 12.00
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	85. 12.08
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	80. 12.17
HYDROGRAPH AT					
+	NE2345	.23	1	FLOW TIME	97. 12.08
2 COMBINED AT					
+	CPNE4	.38	1	FLOW TIME	168. 12.08
ROUTED TO					
+	RT W3	.38	1	FLOW TIME	88. 13.08
2 COMBINED AT					
+	CPWET3	5.46	1	FLOW TIME	811. 13.42
ROUTED TO					
+	RT DN	5.46	1	FLOW TIME	778. 13.92
2 COMBINED AT					
+	DMNTE	12.94	1	FLOW TIME	2762. 17.83
HYDROGRAPH AT					
+	N-1	.02	1	FLOW TIME	16. 12.17
ROUTED TO					
+	RT N13	.02	1	FLOW TIME	14. 12.25
ROUTED TO					
+	RT N13	.02	1	FLOW TIME	13. 13.17
ROUTED TO					
+	RT01	.02	1	FLOW TIME	10. 14.75
HYDROGRAPH AT					
+	D4	.80	1	FLOW TIME	70. 12.67
3 COMBINED AT					
+	PT01	13.76	1	FLOW TIME	2776. 17.83
ROUTED TO					
+	RT02	13.76	1	FLOW TIME	2739. 18.42
HYDROGRAPH AT					
+	D3	.70	1	FLOW TIME	114. 12.67
2 COMBINED AT					

+	PT02	14.46	1	FLOW TIME	2745. 18.42
	ROUTED TO				
+	RT03	14.46	1	FLOW TIME	2663. 19.83
	HYDROGRAPH AT				
+	W18RB	.13	1	FLOW TIME	141. 12.08
	HYDROGRAPH AT				
+	V18-19	.05	1	FLOW TIME	51. 12.08
	HYDROGRAPH AT				
+	V20	.05	1	FLOW TIME	46. 12.08
	HYDROGRAPH AT				
+	WET	.02	1	FLOW TIME	7. 12.17
	4 COMBINED AT				
+	CB WET	.25	1	FLOW TIME	244. 12.08
	HYDROGRAPH AT				
+	PH-IV	.19	1	FLOW TIME	158. 12.17
	HYDROGRAPH AT				
+	E14	.03	1	FLOW TIME	24. 12.08
	3 COMBINED AT				
+	C14	.47	1	FLOW TIME	412. 12.17
	ROUTED TO				
+	E14-E1	.47	1	FLOW TIME	411. 12.17
	HYDROGRAPH AT				
+	E1	.01	1	FLOW TIME	7. 12.00
	2 COMBINED AT				
+	C1	.47	1	FLOW TIME	418. 12.17
	ROUTED TO				
+	E1-E2	.47	1	FLOW TIME	413. 12.17
	HYDROGRAPH AT				
+	E2	.00	1	FLOW TIME	4. 12.00
	2 COMBINED AT				
+	C2	.47	1	FLOW TIME	417. 12.17
	ROUTED TO				
+	E2-E3	.47	1	FLOW TIME	409. 12.17
	HYDROGRAPH AT				
+	E3	.00	1	FLOW TIME	3. 12.00
	2 COMBINED AT				
+	C3	.48	1	FLOW TIME	412. 12.17
	ROUTED TO				
+	E3-E4	.48	1	FLOW TIME	402. 12.17
	HYDROGRAPH AT				
+	E4	.00	1	FLOW TIME	4. 12.00
	2 COMBINED AT				
+	C4	.48	1	FLOW TIME	406. 12.17
	HYDROGRAPH AT				
+	D10	.12	1	FLOW TIME	106. 12.17
	HYDROGRAPH AT				
+	D12	.02	1	FLOW TIME	18. 12.08
	HYDROGRAPH AT				
+	PARK	.01	1	FLOW TIME	5. 12.08
	4 COMBINED AT				
+	C10PRK	.63	1	FLOW TIME	530. 12.17
	ROUTED TO				
+	PK-CAR	.63	1	FLOW TIME	515. 12.25

HYDROGRAPH AT					
+	PhVa	.01	1	FLOW TIME	12. 12.08
HYDROGRAPH AT					
+	V4	.03	1	FLOW TIME	21. 12.08
3 COMBINED AT					
+	CB 1	.66	1	FLOW TIME	535. 12.25
ROUTED TO					
+	RT1-2	.66	1	FLOW TIME	530. 12.25
HYDROGRAPH AT					
+	PhVb	.03	1	FLOW TIME	27. 12.08
2 COMBINED AT					
+	CB2	.69	1	FLOW TIME	549. 12.25
ROUTED TO					
+	RT2-3	.69	1	FLOW TIME	537. 12.33
HYDROGRAPH AT					
+	V12	.01	1	FLOW TIME	12. 12.08
HYDROGRAPH AT					
+	V11	.01	1	FLOW TIME	7. 12.00
HYDROGRAPH AT					
+	V3	.03	1	FLOW TIME	20. 12.08
4 COMBINED AT					
+	CB3	.74	1	FLOW TIME	563. 12.33
ROUTED TO					
+	RT3-4	.74	1	FLOW TIME	555. 12.33
HYDROGRAPH AT					
+	PhVc	.02	1	FLOW TIME	23. 12.08
HYDROGRAPH AT					
+	V2	.04	1	FLOW TIME	30. 12.08
3 COMBINED AT					
+	CB4	.80	1	FLOW TIME	575. 12.33
ROUTED TO					
+	RT4-5	.80	1	FLOW TIME	569. 12.33
HYDROGRAPH AT					
+	PARKVI	.00	1	FLOW TIME	2. 12.08
2 COMBINED AT					
+	CB5	.81	1	FLOW TIME	571. 12.33
ROUTED TO					
+	RT5-6	.81	1	FLOW TIME	558. 12.42
HYDROGRAPH AT					
+	K6SCHL	.01	1	FLOW TIME	10. 12.08
2 COMBINED AT					
+	CB6	.82	1	FLOW TIME	568. 12.42
ROUTED TO					
+	RT6-7	.82	1	FLOW TIME	558. 12.50
HYDROGRAPH AT					
+	V1	.04	1	FLOW TIME	27. 12.08
HYDROGRAPH AT					
+	V29	.06	1	FLOW TIME	67. 12.08
3 COMBINED AT					
+	CB7	.92	1	FLOW TIME	578. 12.50
HYDROGRAPH AT					
+	DR 1	.00	1	FLOW TIME	452. 13.08
ROUTED TO					
+	RT 21	.00	1	FLOW TIME	439. 13.42

HYDROGRAPH AT +	W13R	1.30	1	FLOW TIME	35. 12.42
2 COMBINED AT +	CP 21	1.30	1	FLOW TIME	449. 13.42
DIVERSION TO +	CH 1A	1.30	1	FLOW TIME	200. 13.00
HYDROGRAPH AT +	DV 1B	1.30	1	FLOW TIME	249. 13.42
ROUTED TO +	RT V12	1.30	1	FLOW TIME	242. 13.58
HYDROGRAPH AT +	W12R	.60	1	FLOW TIME	18. 12.42
2 COMBINED AT +	CP V12	1.90	1	FLOW TIME	251. 13.58
HYDROGRAPH AT +	DR CH2	.00	1	FLOW TIME	863. 13.33
ROUTED TO +	RT V12	.00	1	FLOW TIME	844. 13.58
2 COMBINED AT +	CP V12	1.90	1	FLOW TIME	1095. 13.58
ROUTED TO +	RT F12	1.90	1	FLOW TIME	1061. 13.75
HYDROGRAPH AT +	W15R	.21	1	FLOW TIME	106. 12.08
2 COMBINED AT +	CP F12	2.11	1	FLOW TIME	1070. 13.75
HYDROGRAPH AT +	DR 1A	.00	1	FLOW TIME	200. 13.00
ROUTED TO +	RT F1A	.00	1	FLOW TIME	200. 14.00
HYDROGRAPH AT +	W14R	.18	1	FLOW TIME	69. 12.17
2 COMBINED AT +	CP F1A	.18	1	FLOW TIME	209. 13.75
2 COMBINED AT +	CB 142	2.29	1	FLOW TIME	1279. 13.75
ROUTED TO +	RT WT2	2.29	1	FLOW TIME	1271. 13.92
ROUTED TO +	RT WT2	2.29	1	FLOW TIME	1219. 14.42
ROUTED TO +	RT WT2	2.29	1	FLOW TIME	1215. 14.50
HYDROGRAPH AT +	WT 6P1	.07	1	FLOW TIME	32. 12.25
HYDROGRAPH AT +	W WT2P	.59	1	FLOW TIME	122. 12.58
3 COMBINED AT +	CB WT2	2.95	1	FLOW TIME	1233. 14.50
HYDROGRAPH AT +	WS WT1	1.93	1	FLOW TIME	73. 12.83
ROUTED TO +	RT WT3	1.93	1	FLOW TIME	72. 13.17
HYDROGRAPH AT +	THOMAS	11.54	1	FLOW	2544.

				TIME	13.25
DIVERSION TO					
+	HOLCOM	11.54	1	FLOW TIME	1380. 13.25
HYDROGRAPH AT					
+	DV HOL	11.54	1	FLOW TIME	1164. 13.25
ROUTED TO					
+	RT WT3	11.54	1	FLOW TIME	1151. 13.50
DIVERSION TO					
+	THOM	11.54	1	FLOW TIME	52. 13.50
HYDROGRAPH AT					
+	DV THO	11.54	1	FLOW TIME	1099. 13.50
ROUTED TO					
+	RT WT3	11.54	1	FLOW TIME	1097. 13.58
HYDROGRAPH AT					
+	WT3P	.49	1	FLOW TIME	185. 12.25
3 COMBINED AT					
+	CB WT3	13.96	1	FLOW TIME	1163. 13.58
2 COMBINED AT					
+	CB OFF	16.91	1	FLOW TIME	2055. 14.42
ROUTED TO					
+	RT WHC	16.91	1	FLOW TIME	2050. 14.50
HYDROGRAPH AT					
+	D2	.36	1	FLOW TIME	31. 12.42
2 COMBINED AT					
+	CB WHC	17.27	1	FLOW TIME	2058. 14.50
ROUTED TO					
+	RT DET	17.27	1	FLOW TIME	2055. 14.58
ROUTED TO					
+	RT DET	17.27	1	FLOW TIME	1743. 15.08
				** PEAK STAGES IN FEET **	
			1	STAGE	4427.22
				TIME	15.08
ROUTED TO					
+	RT WT	17.27	1	FLOW TIME	1741. 15.17
HYDROGRAPH AT					
+	THOMAS	.00	1	FLOW TIME	52. 13.50
ROUTED TO					
+	RT WT	.00	1	FLOW TIME	32. 15.08
HYDROGRAPH AT					
+	WT4P	1.73	1	FLOW TIME	220. 13.42
2 COMBINED AT					
+		1.73	1	FLOW TIME	220. 13.42
HYDROGRAPH AT					
+	WT7P	.16	1	FLOW TIME	19. 13.33
ROUTED TO					
+	RT WT	.16	1	FLOW TIME	18. 14.00
HYDROGRAPH AT					
+	WS WT5	.49	1	FLOW TIME	266. 12.17
ROUTED TO					
+	RT WT	.49	1	FLOW TIME	202. 12.58
3 COMBINED AT					
+	CB WT	2.38	1	FLOW TIME	327. 12.67
2 COMBINED AT					
+	CP WT	19.65	1	FLOW TIME	1852. 15.08
4 COMBINED AT					

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+          PT03   106.61   1   FLOW      7307.
          TIME      15.58
ROUTED TO
+          RT04   106.61   1   FLOW      7104.
          TIME      17.42
HYDROGRAPH AT
+          D1     .44     1   FLOW      74.
          TIME     12.50
HYDROGRAPH AT
+          D5     1.21   1   FLOW      16.
          TIME     17.25
  3 COMBINED AT
+          PT04   108.26   1   FLOW      7126.
          TIME      17.42
1

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SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)
							PEAK (CFS)	TIME TO PEAK (MIN)	
FOR PLAN = 1 RT STM	RATIO= .94 MANE	1.51	714.59	808.24	.23	5.00	713.88	810.00	.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1609E+03 EXCESS= .0000E+00 OUTFLOW= .1602E+03 BASIN STORAGE= .8542E+00 PERCENT ERROR= -.1									
FOR PLAN = 1 OUTJ1	RATIO= .00 MANE	5.00	2017.57	845.00	1.64	5.00	2017.57	845.00	1.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7027E+03 EXCESS= .0000E+00 OUTFLOW= .6995E+03 BASIN STORAGE= .4234E+01 PERCENT ERROR= -.1									
FOR PLAN = 1 OUTG3	RATIO= .00 MANE	5.00	2305.58	850.00	1.06	5.00	2305.58	850.00	1.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8204E+03 EXCESS= .0000E+00 OUTFLOW= .8146E+03 BASIN STORAGE= .7346E+01 PERCENT ERROR= -.2									
FOR PLAN = 1 RT C1	RATIO= .00 MANE	1.25	4.32	736.25	.77	5.00	4.25	740.00	.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2549E+01 EXCESS= .0000E+00 OUTFLOW= .2532E+01 BASIN STORAGE= .1746E-01 PERCENT ERROR= .0									
FOR PLAN = 1 RT C1	RATIO= .00 MANE	1.75	4.35	747.25	.75	5.00	4.22	755.00	.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2533E+01 EXCESS= .0000E+00 OUTFLOW= .2492E+01 BASIN STORAGE= .4446E-01 PERCENT ERROR= -.1									
FOR PLAN = 1 RT DSW	RATIO= .00 MANE	5.00	853.15	830.00	4.91	5.00	853.15	830.00	4.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1933E+03 EXCESS= .0000E+00 OUTFLOW= .1915E+03 BASIN STORAGE= .2393E+01 PERCENT ERROR= -.3									
FOR PLAN = 1 RT S3	RATIO= .00 MANE	1.50	10.23	433.50	3.62	5.00	10.19	435.00	3.62
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7578E+01 EXCESS= .0000E+00 OUTFLOW= .7537E+01 BASIN STORAGE= .4286E-01 PERCENT ERROR= .0									
FOR PLAN = 1 RT T2	RATIO= .00 MANE	1.22	33.64	726.53	4.06	5.00	33.35	725.00	4.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7811E+01 EXCESS= .0000E+00 OUTFLOW= .7799E+01 BASIN STORAGE= .1283E-01 PERCENT ERROR= .0									
FOR PLAN = 1 RT T3	RATIO= .00 MANE	2.92	92.71	727.83	3.21	5.00	89.30	730.00	3.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1737E+02 EXCESS= .0000E+00 OUTFLOW= .1731E+02 BASIN STORAGE= .6834E-01 PERCENT ERROR= -.1									
FOR PLAN = 1 RT C3	RATIO= .00 MANE	5.00	10.26	735.00	3.41	5.00	10.26	735.00	3.41
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6284E+01 EXCESS= .0000E+00 OUTFLOW= .6188E+01 BASIN STORAGE= .1120E+00 PERCENT ERROR= -.3									
FOR PLAN = 1 RT C3	RATIO= .00 MANE	5.00	44.83	730.00	2.29	5.00	44.83	730.00	2.29
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8628E+01 EXCESS= .0000E+00 OUTFLOW= .8549E+01 BASIN STORAGE= .1145E+00 PERCENT ERROR= -.4									
FOR PLAN = 1 RT C4	RATIO= .00 MANE	1.42	822.95	736.19	.52	5.00	819.35	735.00	.52

CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.8381E+02	EXCESS=	.0000E+00	OUTFLOW=	.8371E+02	BASIN STORAGE=	.1696E+00	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	4.45	832.02	738.88	.56	5.00	825.00	740.00	.56	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9168E+02	EXCESS=	.0000E+00	OUTFLOW=	.9137E+02	BASIN STORAGE=	.6082E+00	PERCENT ERROR=	-.3
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	3.88	815.34	741.08	.56	5.00	810.91	745.00	.56	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9140E+02	EXCESS=	.0000E+00	OUTFLOW=	.9111E+02	BASIN STORAGE=	.5375E+00	PERCENT ERROR=	-.3
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	.69	58.04	725.43	2.57	5.00	57.69	725.00	2.58	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9343E+01	EXCESS=	.0000E+00	OUTFLOW=	.9339E+01	BASIN STORAGE=	.1118E-01	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	5.00	56.55	735.00	2.54	5.00	56.55	735.00	2.54	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9352E+01	EXCESS=	.0000E+00	OUTFLOW=	.9242E+01	BASIN STORAGE=	.1689E+00	PERCENT ERROR=	-.6
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	5.00	33.94	735.00	1.17	5.00	33.94	735.00	1.17	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7894E+01	EXCESS=	.0000E+00	OUTFLOW=	.7825E+01	BASIN STORAGE=	.8120E-01	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	.24	33.82	734.87	1.17	5.00	33.82	735.00	1.17	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7814E+01	EXCESS=	.0000E+00	OUTFLOW=	.7811E+01	BASIN STORAGE=	.3499E-02	PERCENT ERROR=	.0
FOR PLAN = 1	RATIO=	.00								
RT C7	MANE	5.00	33.92	745.00	1.15	5.00	33.92	745.00	1.15	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7824E+01	EXCESS=	.0000E+00	OUTFLOW=	.7696E+01	BASIN STORAGE=	.1709E+00	PERCENT ERROR=	-.6
FOR PLAN = 1	RATIO=	.00								
RT S3	MANE	1.50	13.80	730.50	1.90	5.00	13.65	730.00	1.90	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6124E+01	EXCESS=	.0000E+00	OUTFLOW=	.6084E+01	BASIN STORAGE=	.4591E-01	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RT S3	MANE	5.00	31.51	730.00	1.36	5.00	31.51	730.00	1.36	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7771E+01	EXCESS=	.0000E+00	OUTFLOW=	.7724E+01	BASIN STORAGE=	.5686E-01	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RT S5	MANE	5.00	59.58	735.00	1.75	5.00	59.58	735.00	1.75	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2057E+02	EXCESS=	.0000E+00	OUTFLOW=	.2044E+02	BASIN STORAGE=	.1706E+00	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00								
RT S7	MANE	5.00	66.58	740.00	1.79	5.00	66.58	740.00	1.79	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2471E+02	EXCESS=	.0000E+00	OUTFLOW=	.2454E+02	BASIN STORAGE=	.2175E+00	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00								
RT S7	MANE	1.00	.55	736.00	1.39	5.00	.50	745.00	1.39	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2995E+00	EXCESS=	.0000E+00	OUTFLOW=	.2958E+00	BASIN STORAGE=	.4227E-02	PERCENT ERROR=	-.2
FOR PLAN = 1	RATIO=	.00								
RT WI	MANE	3.02	121.38	725.34	1.88	5.00	120.52	725.00	1.88	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.3627E+02	EXCESS=	.0000E+00	OUTFLOW=	.3613E+02	BASIN STORAGE=	.1719E+00	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RT WI	MANE	5.00	122.68	735.00	1.86	5.00	122.68	735.00	1.86	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.3621E+02	EXCESS=	.0000E+00	OUTFLOW=	.3576E+02	BASIN STORAGE=	.5598E+00	PERCENT ERROR=	-.3
FOR PLAN = 1	RATIO=	.00								
RTWI	MANE	.76	58.84	725.86	2.71	5.00	58.13	725.00	2.71	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9414E+01 EXCESS= .0000E+00 OUTFLOW= .9405E+01 BASIN STORAGE= .1230E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RT WJ MANE 5.00 57.05 735.00 2.67 5.00 57.05 735.00 2.67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9419E+01 EXCESS= .0000E+00 OUTFLOW= .9284E+01 BASIN STORAGE= .2083E+00 PERCENT ERROR= -.8

FOR PLAN = 1 RATIO= .00
RT E3 MANE 3.98 43.14 727.90 2.20 5.00 42.00 730.00 2.20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8242E+01 EXCESS= .0000E+00 OUTFLOW= .8205E+01 BASIN STORAGE= .4259E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT E3 MANE 1.00 2.26 735.00 .50 5.00 2.26 735.00 .50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1343E+01 EXCESS= .0000E+00 OUTFLOW= .1335E+01 BASIN STORAGE= .8296E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RTE3 MANE 1.25 2.26 745.00 .50 5.00 2.26 745.00 .50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1336E+01 EXCESS= .0000E+00 OUTFLOW= .1323E+01 BASIN STORAGE= .1421E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT E3 MANE 2.19 214.40 723.98 .72 5.00 211.41 725.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1851E+02 EXCESS= .0000E+00 OUTFLOW= .1846E+02 BASIN STORAGE= .6918E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT E3 MANE 3.50 205.63 728.00 .72 5.00 196.52 730.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1845E+02 EXCESS= .0000E+00 OUTFLOW= .1837E+02 BASIN STORAGE= .1198E+00 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT E4 MANE 3.53 192.31 731.27 .71 5.00 187.57 730.00 .71

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1836E+02 EXCESS= .0000E+00 OUTFLOW= .1827E+02 BASIN STORAGE= .1105E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT E4 MANE 2.15 68.68 727.70 1.59 5.00 66.45 725.00 1.59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8479E+01 EXCESS= .0000E+00 OUTFLOW= .8463E+01 BASIN STORAGE= .3004E-01 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT N1 MANE 1.75 527.46 741.36 .40 5.00 524.16 740.00 .40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3716E+02 EXCESS= .0000E+00 OUTFLOW= .3714E+02 BASIN STORAGE= .5565E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N1 MANE 4.13 524.45 744.13 .40 5.00 520.20 745.00 .40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3715E+02 EXCESS= .0000E+00 OUTFLOW= .3711E+02 BASIN STORAGE= .1322E+00 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT N1 MANE 2.78 514.77 747.09 .40 5.00 511.73 745.00 .40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3711E+02 EXCESS= .0000E+00 OUTFLOW= .3706E+02 BASIN STORAGE= .1116E+00 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT N1 MANE 3.56 815.58 752.02 .41 5.00 810.13 755.00 .41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7198E+02 EXCESS= .0000E+00 OUTFLOW= .7193E+02 BASIN STORAGE= .1395E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N1 MANE 2.36 809.53 754.46 .41 5.00 808.79 755.00 .41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7195E+02 EXCESS= .0000E+00 OUTFLOW= .7189E+02 BASIN STORAGE= .1172E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N1 MANE 1.20 17.99 727.21 2.95 5.00 17.57 730.00 2.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6939E+01 EXCESS= .0000E+00 OUTFLOW= .6929E+01 BASIN STORAGE= .1264E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RT W3 MANE 1.66 1291.37 751.31 .43 5.00 1279.89 750.00 .43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1159E+03 EXCESS= .0000E+00 OUTFLOW= .1158E+03 BASIN STORAGE= .1849E+00 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO= .00								
RT N4	MANE	3.20	95.23	722.71	1.01	5.00	88.38	720.00	1.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8099E+01 EXCESS= .0000E+00 OUTFLOW= .8067E+01 BASIN STORAGE= .4219E-01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RT N4	MANE	2.39	87.38	722.64	1.00	5.00	85.32	725.00	1.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8053E+01 EXCESS= .0000E+00 OUTFLOW= .8029E+01 BASIN STORAGE= .3054E-01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RT N4	MANE	4.00	84.88	728.00	1.00	5.00	80.39	730.00	1.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8045E+01 EXCESS= .0000E+00 OUTFLOW= .7986E+01 BASIN STORAGE= .8840E-01 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO= .00								
RT N13	MANE	5.00	14.11	735.00	6.33	5.00	14.11	735.00	6.33
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6837E+01 EXCESS= .0000E+00 OUTFLOW= .6763E+01 BASIN STORAGE= .9067E-01 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO= .00								
E14-E1	MANE	1.62	412.48	728.62	2.22	5.00	411.06	730.00	2.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5538E+02 EXCESS= .0000E+00 OUTFLOW= .5527E+02 BASIN STORAGE= .1670E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
E1-E2	MANE	1.21	413.41	731.11	2.36	5.00	413.31	730.00	2.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5942E+02 EXCESS= .0000E+00 OUTFLOW= .5936E+02 BASIN STORAGE= .1343E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
E2-E3	MANE	1.21	411.54	730.41	2.43	5.00	409.39	730.00	2.43
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6164E+02 EXCESS= .0000E+00 OUTFLOW= .6158E+02 BASIN STORAGE= .1392E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
E3-E4	MANE	1.46	408.98	731.46	2.49	5.00	402.02	730.00	2.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6347E+02 EXCESS= .0000E+00 OUTFLOW= .6334E+02 BASIN STORAGE= .1720E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
PK-CAR	MANE	2.65	520.86	732.14	2.57	5.00	515.01	735.00	2.58
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8632E+02 EXCESS= .0000E+00 OUTFLOW= .8602E+02 BASIN STORAGE= .4259E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RT1-2	MANE	5.00	530.03	735.00	2.77	5.00	530.03	735.00	2.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9902E+02 EXCESS= .0000E+00 OUTFLOW= .9834E+02 BASIN STORAGE= .9926E+00 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO= .00								
RT2-3	MANE	2.34	539.29	738.46	2.84	5.00	536.73	740.00	2.84
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1053E+03 EXCESS= .0000E+00 OUTFLOW= .1050E+03 BASIN STORAGE= .4521E+00 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO= .00								
RT3-4	MANE	1.60	556.29	740.48	3.08	5.00	554.78	740.00	3.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1220E+03 EXCESS= .0000E+00 OUTFLOW= .1218E+03 BASIN STORAGE= .3505E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RT4-5	MANE	.87	569.85	740.54	3.16	5.00	568.79	740.00	3.16
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1354E+03 EXCESS= .0000E+00 OUTFLOW= .1353E+03 BASIN STORAGE= .2078E+00 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RT5-6	MANE	2.04	562.72	741.73	3.17	5.00	557.94	745.00	3.17
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1367E+03 EXCESS= .0000E+00 OUTFLOW= .1364E+03 BASIN STORAGE= .4902E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RT6-7	MANE	5.00	557.74	750.00	3.23	5.00	557.74	750.00	3.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1427E+03 EXCESS= .0000E+00 OUTFLOW= .1414E+03 BASIN STORAGE= .1791E+01 PERCENT ERROR= -.3									
FOR PLAN = 1 RATIO= .00									

RT WT2	MANE	5.00	1271.33	835.00	2.36	5.00	1271.33	835.00	2.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2918E+03 EXCESS= .0000E+00 OUTFLOW= .2881E+03 BASIN STORAGE= .5190E+01 PERCENT ERROR= -.5									
FOR PLAN = 1 RATIO= .00									
RT WT2	MANE	5.00	1215.49	870.00	2.31	5.00	1215.49	870.00	2.31
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2843E+03 EXCESS= .0000E+00 OUTFLOW= .2824E+03 BASIN STORAGE= .3325E+01 PERCENT ERROR= -.5									
FOR PLAN = 1 RATIO= .00									
RT WHC	MANE	5.00	2049.74	870.00	.86	5.00	2049.74	870.00	.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7837E+03 EXCESS= .0000E+00 OUTFLOW= .7786E+03 BASIN STORAGE= .6366E+01 PERCENT ERROR= -.2									
FOR PLAN = 1 RATIO= .00									
RT DET	MANE	5.00	2054.69	875.00	.85	5.00	2054.69	875.00	.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7858E+03 EXCESS= .0000E+00 OUTFLOW= .7804E+03 BASIN STORAGE= .7286E+01 PERCENT ERROR= -.2									

1

HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
	+
	+
	+

*** NORMAL END OF HEC-1 ***


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*****
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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
* JUN 1998 *
*
* VERSION 4.1 *
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* RUN DATE 04JAN08 TIME 13:39:39 *
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*
*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
*DIAGRAM
1 ID DRph5+BV1 THE PROPOSED MODEL FOR DAMONTE PHASE 5 LOMR (CASE No. 07-09-1667P)
2 ID IS ALSO THE MODEL USED FOR THE SUBSTANTIALLY COMPLETE HYDRAULIC MODEL FOR
3 ID STEAMBOAT CREEK THROUGH BELLA VISTA PHASE 1.
4 ID IT WAS RE-RUN ON JANUARY 4, 2008. ONLY THE ID INFORMATION WAS UPDATED
5 ID FOR THIS RUN. JANUARY 2008 - Model Run date is 01/04/2008
6 ID *****
7 ID CLOMR MODEL WAS USED WITHOUT CHANGE FOR THE LOMR MODEL FOR DAMONTE RANCH
8 ID PHASE 5 (CASE No. 07-09-1667P). SUBMITTED MAY 5, 2007 AND NOT RERUN. IT
9 ID DEFINED THE CHANNEL FLOWS FOR THE SUBSTANTIALLY COMPLETE STEAMBOAT CHANNEL
10 ID HYDRAULIC MODEL THROUGH BELLA VISTA PHASE 1.
11 ID LOMR AS-BUILT PLANS DID NOT CHANGE THE HYDROLOGIC PARAMETERS USED IN THE CLO
12 ID MARCH 2007 - Model Run date is 3/12/2007
13 ID *****
14 ID UPDATED MODEL FOR DAMONTE RANCH PHASE V and BELLA VESTA PHASE 1 CLOMR
15 ID USED FOR THE SUBSTANTIALLY COMPLETED MODEL THROUGH BELLA VISTA PHASE 1
16 ID MARCH 2007 - Model Run date is 3/12/2007
17 ID *****
18 ID BELLA VESTA RANCH PHASE 1
19 ID FILE NAME: DRph5+BV1.dat - DECEMBER 2005 (UPDATED: JANUARY 2005)
20 ID *****
21 ID DAMONTE RANCH PHASE V - MARCH 2005
22 ID
23 ID * * INCLUDES DEVELOPMENT OF VILLAGE 11-B * *
24 ID
25 ID UPDATED MODEL FROM LOMR SUBMITTAL FILE NAME 0243AB.DAT (Orig. 128CLOMR.DAT)
26 ID TO REFLECT GRADING PLANS AS OF 3/2005
27 ID 100-Year HEC-1 for AS BUILT conditions. Includes Steamboat Creek &
28 ID tributaries (i.e. Galena, Jones, Browns, Bailey, 30, & 40 watersheds);
29 ID Damonte Ranch with refined watersheds, detention structures, & refined
30 ID east range watersheds; Whites Creek watersheds collected by Branch 3 & 4
31 ID with routing onto Damonte; the remainder of the Whites Creek & split flow
32 ID from Thomas Creeks watersheds routed through Double Diamond;
33 ID & Bella Vista Ranch with the remaining east range watersheds.
34 ID
35 ID File Name: DRph5+bv1.dat
36 ID Quad Knopf formerly Nimbus Engineers
37 ID
38 ID
39 ID
40 ID REVISIONS REFLECT PHASE V DEVELOPMENT PER GRADING PLAN DATED 2/2005
41 ID The model also includes the previous changes at the Diversion structure:
42 ID a) box culverts replaced the RCPs; b) an overflow weir was added to control
43 ID a major flood event
44 ID
45 ID
46 ID *****
47 ID
48 ID * * MODIFIED 5-2005 TO REFLECT GRADING PLAN CHANGES AFFECTING EASTERN * *
49 ID * * BASINS NE-2, NE-3, NE-4, & NE-5. THESE HAVE ALL BEEN COMBINED AS * *
50 ID * * THE REMOVAL OF MIRA LOMA RD. MAKES SEPARATION UNNECESSARY * *
51 ID *****
52 ID
Legend :
* W(No.)R = Subbasin
* CP XX = Combine flows at point XX
* RT XX = Route to CP XX
* DV XX = Divert hydrograph XX
* DR XX = Recall hydrograph XX

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116 BA 0.85
 117 PB 3.4
 118 LS 68
 119 UD 0.96
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

120 KK W7+CH Combine W7 and channel
 121 HC 2
 *

122 KK RT-DIF Route flows to Difffluence
 123 RM 1 0.104 0.4
 *

124 KK W8R Whites Creek No. 8
 125 BA 0.75
 126 PB 3.0
 127 LS 65
 128 UD 1.19
 *

129 KK CP DIF Combine flows at Difffluence
 130 HC 2
 *

131 KK DV 4 Divert flows into channel #4 - south branch
 132 KM Hydrograph at this station is flow in channel 4
 133 DT CH 123
 134 DI 0 2000 3500 5100
 135 DQ 0 1700 2700 3750
 *

136 KK RT W4 Route flows in channel #4 to Wedge Parkway
 137 RM 2 .178 .3
 *

138 KK W17R Whites Creek No. 17
 139 BA 0.58
 140 PB 2.8
 141 LS 67
 142 UD 0.31
 *

143 KK CP W4 Combine flows at Wedge Parkway
 144 HC 2
 *

145 KK RT F4 Route flows to proposed RCB at 580
 146 RM 1 0.111 .3
 *

147 KK W19R Whites Creek No. 19
 148 BA 0.33
 149 PB 2.75
 150 LS 60
 151 UD 0.22
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

152 KK W9R Whites Creek No. 9 (Steamboat Hills Area, above Mt. Rose Hwy)
 153 BA 2.39
 154 PB 2.8
 155 LS 69
 156 UD 0.51
 *

157 KK RT F4 Route flows to proposed RCB at 580 (Channel 4)
 158 RM 2 0.181 0.3
 *

159 KK CP F4 Combine flows at proposed I-580 RCB (Channel 4)
 160 HC 3
 *

161 KK RT V4 Route flows to Virginia Street (Channel 4 near Browns School)
 162 RM 1 0.121 .3

163 KK W20R Whites Creek No. 20
 164 BA 0.22
 165 PB 2.73
 166 LS 61
 167 UD 0.22
 *

168 KK CP V4 Combine flows at Channel #4 and Virginia St. (near Browns School)
 169 HC 2
 *

170 KK RT STM ROUTE BRACH 4 TO STEAMBOAT CREEK - THRU PROPOSED CHANNEL
 171 RK 2250 0.013 .035 TRAP 75 3
 *
 *
 * *****
 * STEAMBOAT CREEK MODEL
 * *****
 *
 *
 172 KK G1G2 Upper Galena Creek - G1 & G2 COMBINED
 173 BA 8.0
 174 PB 4.89

175 LS 70
 176 UD 1.9
 *
 177 KK OUTJ1 Route to Confluence with Jones Creek
 178 RD 5280 .046 0.07 TRAP 15 0.5
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

179 KK J1 Jones Creek Watershed
 180 BA 6.4
 181 PB 3.51
 182 LS 58
 183 UD 1.3
 *
 184 KK OUTJ1 Combine Jones and Galena Creek
 185 HC 2
 *
 186 KK OUTG3 Route Galena to Pleasant Valley foothill
 187 RD 7392 0.043 0.07 TRAP 15 1
 *
 188 KK G3 Lower Galena Creek
 189 BA 3.9
 190 PB 3.4
 191 LS 62
 192 UD 1.2
 *
 193 KK OUTG3 Combine Galena flows at Pleasant Valley foothill
 194 HC 2
 *
 195 KK OUT30 Route Galena Creek watershed to Steamboat Gage (use COE routing)
 196 RM 7 0.61 0.2
 *
 197 KK 15 Browns Creek
 198 BA 4.2
 199 PB 4.10
 200 LS 61
 201 UD 1.7
 *
 202 KK OUT30 Route Browns Creek to Steamboat Gage (use COE routing)
 203 RM 16 1.34 0.2
 *
 204 KK 30 COE Watershed No. 30
 205 BA 16.7
 206 BF 500 0 1
 207 PB 2.8
 208 LS 77
 209 UD 1.8
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

210 KK OUT30 Combine
 211 HC 3
 212 KK OUT40 Route flows to HWY 341 (use COE routing)
 213 RM 3 0.23 0.2
 *
 214 KK 35 Bailey Canyon
 215 BA 15.3
 216 BF 0 10 1.1
 217 PB 2.95
 218 LS 80
 219 UD 2.2
 *
 220 KK 40 Watershed No.40
 221 BA 2.5
 222 PB 2.77
 223 LS 77
 224 UD 1.1
 *
 225 KK OUT40 Combine Steamboat Ck with areas 35 and 40 at HWY 341
 226 HC 3
 *
 227 KK OUT341 ROUTE STEAMBOAT THROUGH HWY 341 USING MODIFIED PULS
 228 RS 1 STOR 0
 229 SA .31 9.48 46.1
 230 SE 4550 4560 4570
 231 SQ 300 2475 58000
 *
 232 KK C-1B
 233 BA 0.072
 234 PB 2.5
 235 LS 69 64
 236 UD 0.22
 *
 237 KK C-1A
 238 BA 0.062

239 LS 64
 240 UD 0.20
 *
 241 KK RT C1 ROUTING POD C-1A THRU CHANNEL C-1C TO CHANNEL C-1E
 242 RD 1000 0.014 0.030 TRAP 5 3
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

243 KK RT C1 ROUTING POD C-1A THRU CHANNEL C-1E TO CULVERT C-C2C
 244 RD 1800 0.0056 0.030 TRAP 5 3
 *
 245 KK CPC1B
 246 HC 2
 *
 247 KK CB CUR Combine flows just north of SR 341 (Steamboat Ck)
 248 HC 2
 *
 249 KK OUTDS Route Steamboat to just north of south Damonte property line
 250 RM 2 0.153 .35
 *
 251 KK CB DS COMBINE STEAMBOAT & WHITES BRANCH 4 @ DAMONTE SOUTH BOUNDARY
 252 HC 2
 *
 253 KK RT WHT ROUTE TO SOUTH BOUNDARY OF WHITE'S CREEK MEADOW SUBDIVISION
 254 RM 1 0.084 0.2
 * WHITES CREEK BRANCH3
 *

255 KK DR 123 Recall channel 1, 2, and 3 flows
 256 DR CH 123
 *

257 KK DV 2&3 Divert flows into channels 2 and 3 - two middle branches
 258 KM Hydrograph at this station is flow in channels 2 and 3
 259 DT CH 1
 260 DI 0 1700 2700 3750
 261 DQ 0 350 550 700
 *

262 KK RT 2&3 Route flows to pt where channels 2 and 3 combine (2000' u/s Virginia)
 263 RM 3 .245 .3

264 KK W10R Whites Creek No. 10
 265 BA 0.3
 266 PB 2.8
 267 LS 55
 268 UD .32
 *

269 KK CP 23 Combine local flows with channels 2 and 3
 270 HC 2
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

271 KK DV 23A Divert flows at CP 23 (Channels 2 and 3 Diverge)
 272 KM Hydrograph at this station is in channel 3 (Channel 2 is diverted)
 273 DT CH 2
 274 DI 0 2000 3500
 275 DQ 0 1000 1750
 *

276 KK RT V3 Route flow to Virginia St. (CP V3)
 277 RM 2 0.136 .2

278 KK W11R Whites Creek No. 11
 279 BA 0.32
 280 PB 2.7
 281 LS 75
 282 UD 0.27
 *

283 KK CP V24 Combine Subbasin W11R, and Channel 3 at Virginia Street
 284 HC 2

285 KK RT F3 Route flow to F3 (Channel 3 at 580)
 286 RM 3 0.234 0.2
 *

287 KK W16R Whites Creek No. 16
 288 BA 0.11
 289 PB 2.7
 290 LS 81
 291 UD 0.21
 *

292 KK CP F3 Combine flows at proposed RCB on 580 (Channel 3)
 293 HC 2
 *

294 KK RT DSW ROUTE THRU DRAINAGE DITCH TO STEAMBOAT CREEK
 * USED CHANNEL DESIGN PARAMETERS
 295 RD 2700 0.003 0.035 TRAP 50 3
 *

296 KK W18RA

* Basin W18R - subdivided - area south of Channel #3 = W18RA
 297 BA 0.21
 298 PB 2.7
 299 LS 80
 300 UD 0.33
 *

301 KK CB DSW COMBINE WHITES CREEK BRANCHES 3 & W18RA @ STEAMBOAT CREEK
 302 HC 2
 *

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

303 KK S-1
 304 BA 0.041
 305 PH 1 0.001 0.478 0.869 0.145 1.52 1.58 2.11 2.53
 306 LS 66
 307 UD 0.17
 *

308 KK RT S3 ROUTING POD S-1 THRU STEAMBOAT TO CPS3A
 309 RM 2 .2 .4
 *

310 KK S-2
 311 BA 0.062
 312 LS 62
 313 UD 0.20
 *

314 KK RT S3 ROUTING POD S-2 THRU STEAMBOAT TO CPS3A
 315 RM 1 .1 .1
 *

316 KK S-3A
 317 BA 0.039
 318 LS 63
 319 UD 0.17
 *

320 KK RT S3 ROUTING POD S-3A THRU CHANNEL ST-1 TO CPS3A
 321 RD 1000 0.0025 0.030 TRAP 5 3

322 KK CPS3A
 323 HC 3
 *

324 KK RT S5 ROUTING CPS3A THRU STEAMBOAT TO CPS5
 325 RM 4 0.3311 0.4
 *

326 KK S-3B
 327 BA 0.016
 328 LS 63
 329 UD 0.14
 *

330 KK RT S5 ROUTING POD S-3B THRU STEAMBOAT TO CPS5
 331 RM 3 0.2837 0.4
 *

332 KK S-4
 333 BA 0.021
 334 LS 63
 335 UD 0.16
 *

HEC-1 INPUT

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

336 KK RT S5 ROUTING POD S-4 THRU STEAMBOAT TO CPS5
 337 RM 2 0.1497 0.4
 *

338 KK S-5
 339 BA 0.032
 340 LS 76
 341 UD 0.16
 *

342 KK RT S5 ROUTING POD S-5 OVERLAND TO CPS5
 343 RM 2 0.1230 0.1
 *

344 KK CPS5
 345 HC 4
 *

346 KK RT WHT ROUTINT CPS5 TO WHT THRU STEAMBOAT
 347 RM 2 0.1775 .4

348 KK CB WHT COMBINE STEAMBOAT CREEK W/ WHITES CREEK BRANCHES 3&4
 349 HC 3
 *

350 KK HD WATERSHED TO ACCOUNT FOR COM & IND AREA IN WHITES CK MEADOWS
 351 KM DISCHARGES TO STEAMBOAT CREEK
 352 BA .114
 353 LS 95
 354 UD .32
 *

355 KK CP HD COMBINE HD WITH STEAMBOAT CREEK UPSTREAM OF DIVERSION STRUCTURE
 356 HC 2
 *

* DIVERSION FROM STEAMBOAT TO EAST

357 KK DIVSTR STAGE, STORAGE, AND DISCHARGE FROM DIVERSION POND
 358 KM BACKWATER FROM THE 4 8'X10' RCBS
 * KO 1
 359 RS 1 ELEV 4475
 * DIVERSION POND AREAS FOR ELEVATION 4475 TO 4490; 4 8'x 10' RCBS, I.E.4475
 * WEIR WIDTH = 240' @ CREST 4485'
 * ADDITIONAL ELEVATIONS ADDED TO RESERVOIR , AREAS IN THESE 2 ARE
 * KEPT CLOSE TO THE AREA AT ELEVATION 4488
 360 SA .07 0.25 0.35 0.72 1.13 2.93 3.23 3.51 3.83 4.11
 361 SA 4.34 4.69
 362 SE 4475 4476 4477 4479 4480 4483 4484 4485 4486 4487
 363 SE 4488 4489
 364 SQ 0 124 336 920 1272 2512 2976 3272 4222 5914
 365 SQ 8003 10364
 *
 *

HEC-1 INPUT

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 366 KK STEAM DIVERSION
 * DI=CULVERT+WEIR FLOW, DQ=WEIR FLOW INTO DETENTION BASIN 1
 367 DT BAS 1
 * DI CARDS FOR 5-108" RCP CULVERTS AND WEIR
 368 DI 0 124 336 920 1272 2512 2976 3272 4222 5914
 369 DI 8003 10364
 * DQ CARDS INDICATE FLOW OVER WEIR INTO BASIN 1
 370 DQ 0 0 0 0 0 0 0 0 726 2074
 371 DQ 3847 5980
 *

372 KK OUTDM Route Steamboat to DM (near middle of Damonte property)
 373 RM 2 0.15 0.25

374 KK OUTDN ROUTE STEAMBOAT TO DN -DAMONTE NORTH BOUNDARY
 375 RM 2 0.2 0.25

 DAMONTE RANCH PHASE V

* NOTE: Basins denoted "* DR" correspond to Nimbus Model
 443Post.dat (1/2005)
 *
 *

* PHASE V: ON-SITE AREA DRAINING TO STEAMBOAT CREEK
 *

376 KK A7
 * KK DR 2
 377 BA 0.037
 378 PB 2.8
 379 LS 85
 380 UD 0.531
 *

381 KK STM+7
 382 KM COMBINE A7 INTO STEAMBOAT CRK
 383 HC 2
 *

384 KK A6
 * KK DR 8
 385 BA .019
 386 LS 90
 387 UD .289
 *

HEC-1 INPUT

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

388 KK STM+6
 389 KM COMBINE A6 INTO STEAMBOAT CRK
 390 HC 2
 *

391 KK A3
 392 BA .005
 393 LS 90
 394 UD .167
 *

395 KK STM+3
 396 KM COMBINE A3 INTO STEAMBOAT CRK
 397 HC 2
 *

398 KK A2
 399 BA .020
 400 LS 90
 401 UD .167
 *

402 KK STM+2
 403 KM COMBINE A2 INTO STEAMBOAT CRK
 404 HC 2
 *

```

*
405 KK A17
406 KM CHANNEL E CROSSING AT CARAT DR.
* KK DR 18
407 BA 0.029
* BA 0.031
408 LS 83
409 UD .235
*
*
410 KK A18
* KK DR 19
411 BA 0.036
* BA 0.021
412 LS 83
413 UD .319
*

```

1

HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

414 KK CHNL-E
415 KM CHNL-E CHANNEL E
416 HC 2
*
*
417 KK STM+E
418 KM COMBINE CHANNEL E WITH STEAMBOAT CRK
419 KM DOWNSTREAM DAMONTE BNDRY
420 HC 2
421 KO 3
*

```

```

422 KK RT NST ROUTING CPSTM2 TO CPN4STM2
423 RM 5 0.3916 .4
*
*
*

```

* * NW-4 IS BEING DEVELOPED UNDER PHASE V

```

* *
* KK NW-4
* BA 0.129
* PB 2.5
* LS 73 68
* UD 0.33
*

```

* * FOLLOWING DAMONTE BASINS DRAIN TO THE WESTERN PERIMETER DITCH

```

* KK A4
* KK DR 6
* BA 0.017
* LS 90
* UD .197
*

```

```

* KK A23
* BA 0.004
* LS 85
* UD 0.531
*

```

```

* KK A1
* KK DR 8
* BA 0.014
* BA 0.051
* LS 90
* UD .289
*

```

```

* KK A22
* KK DR 1
* BA 0.004
* LS 91
* UD 0.531
*

```

```

* KK A5
* KK DR 4
* BA 0.047
* BA 0.045
* LS 83
* UD .313
*

```

```

* KKCARAT1
* KM CARAT DR. CULVERT #1
* HC 2
*

```

```

* KKCHNL-A
* KMCHNL-A DAMONTE WESTERN PERIMETER DITCH
* HC 4
*

```

*
*
*
* DAMONTE PHASE V: ON-SITE AREAS A16, A19, A20
*

1

HEC-1 INPUT

PAGE 15

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
424	KK A16 * KK DR 20
425	KM NODE FOR SIZING INLET TO CHANNEL F UNDER CARAT DR
426	BA 0.018 * BA 0.021
427	LS 90
428	UD .222 *
429	KK A19 * KK DR 21
430	BA 0.036
431	LS 83
432	UD .269 *
433	KK A20 * KK DR 22
434	BA 0.023
435	LS 85
436	UD .355 * * *
437	KK CHNL-F CHANNEL F
438	KM OUTLET 3
439	HC 3 *
440	KK STM+AF
441	KM COMBINE CHANNEL A & F INTO STEAMBOAT CRK
442	HC 2 * * INSERT BELLA VISTA PHASE 1A DEVELOPED
443	KK BVW 6 UNDEVELOPED BELLA VISTA ONSITE WATERSHED
444	PB 2.4
445	BA .010
446	LS 74
447	UD 0.167 *
448	KK RT W6 ROUTE BVW6 TO 16
449	RD 910 .0024 .035 TRAP 200 3 *
450	KK BV 16 BELLA VISTA ONSITE WATERSHED
451	PB 2.4
452	BA .006
453	LS 83
454	UD 0.167 *

1

HEC-1 INPUT

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LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
455	KK Stm+16
456	HC 2 *
457	KK RT 16 ROUTE 16 TO 15
458	RD 910 .0024 .035 TRAP 200 3 *
459	KK BV 15 BELLA VISTA ONSITE WATERSHED
460	BA .018
461	LS 83
462	UD 0.167 *
463	KK Stm+15
464	HC 3 *
465	KK RT BV3 ROUTE Stm+15 TO BV3
466	* KO 2 RD 1560 .0024 .035 TRAP 200 3 * * *
467	KK APTS-9
468	KM FUTURE APARTMENTS / PARK SITE -- PREVIOUSLY KNOWN IN
469	KM NIMBUS MODELS AS PRE-DEV BASINS "W-4", "W-5", & "W-6" * PLANS CURRENTLY CALL FOR AN 18" STUB UNDER STEAMBOAT PKY * DRAINS TO CHANNEL B
470	PB 2.8
471	BA 0.032
472	LS 87
473	UD .279 * * *
474	KK A8 * KK DR 10

475 BA 0.071
 476 LS 88
 477 UD .338
 *
 *
 478 KK CHNL-B UPSTREAM SECTION OF CHANNEL B
 479 HC 2
 *
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

480 KK D12&13
 481 KM EXISTING DAMONTE RANCH 12 & 13
 * KK EX 11 EXISTING BASIN #11 (D.R. 12&13)
 482 BA 0.057
 483 LS 84
 484 UD .312
 * *
 *
 485 KK A9
 * KK DR 12
 486 BA 0.050
 487 LS 83
 488 UD .286
 *
 *

489 KK CHNL-C
 490 KM CHANNEL C
 491 HC 2
 *
 *

492 KK B&C
 493 KM COMBINE CHANNEL B & C
 494 HC 2
 *
 *

495 KK A14
 * KK DR 13
 496 BA 0.055
 497 LS 83
 498 UD .295
 *
 *

499 KK A13
 * KKDR 14A
 500 BA 0.045
 * BA 0.047
 501 LS 83
 502 UD .295
 *
 *

503 KK A15
 * KK DR 15
 504 BA 0.018
 * BA 0.019
 505 LS 87
 506 UD .308
 * *
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

507 KK CHNL-D CHANNEL D
 508 KM CHANNEL D
 509 HC 4
 *
 *

510 KK A11
 * KK DR 17
 511 BA 0.014
 * BA 0.016
 512 LS 90
 513 UD .275
 * *
 *

514 KK A12
 * KKDR 14B
 515 BA 0.020
 * BA 0.043
 516 LS 90
 517 UD .475
 * *
 *

518 KK 11+12 ROADSIDE DITCH ALONG CARAT DR
 519 KM ROADSIDE DITCH ALONG CARAT DR DRAINING A11 & A12
 520 HC 2
 *
 *

521 KK CHNL D CHANNEL D CROSSES CARAT DR
 522 KM CROSSING AT CARAT DR AND CHANNEL D

523 HC 2
*
*
*
*
524 KK X12+13 EXISTING DAMONTE RANCH 12 & 13 (AREA 16)
525 KM WAS DEVELOPED PRIOR TO DAMONTE RANCH PHASE V
526 KM PREVIOUSLY KNOWN IN NIMBUS MODELS AS PRE-DEV BASIN "W-7"
527 BA 0.076
528 LS 86
529 UD .733
*
*
530 KK A10
* KK DR 24
531 BA 0.012
532 LS 89
533 UD .206
*
*

HEC-1 INPUT

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1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

534 KK
535 HC 2
*
*
536 KK A21 FUTURE SCHOOL
* KK DR 23 FUTURE SCHOOL SITE
537 BA 0.015
538 LS 93
539 UD .212
*
*
540 KK WTLNDS DISCHARGE TO WETLANDS
541 KO 3
542 HC 3
*
*
*
*
*
*
543 KK RC BAS RECALL DIVERSION FROM STEAMBOAT
544 KM OVERFLOW FROM DIV. STRUCTURE 1
545 DR BAS 1
*
*
546 KK BAS 1 STAGE, STORAGE, AND DISCHARGE FROM BASIN 1
547 KM MODIFY BASIN 1 MAKE IT 5 FT DEEPER TO REDUCE PEAK FLOWS TO EAST
* KO 1
RS 1 ELEV 4473
* *** BAS 1 OUTLET 7 PIPE ARCHES W/1-36" RCP *****
549 SA 19 26.26 30.61 32.63 33.7 34.10 34.47 34.82 35.18 35.54
550 SA 35.97
551 SE 4475 4476 4477 4478 4479 4480 4481 4482 4483 4484
552 SE 4485
553 SQ 5 7 10 515 1021 1523 2027 2537 3059 3561
554 SE 4475.4 4475.92 4476.6 4477.64 4478.54 4479.28 4479.95 4480.59 4481.25 4481.87
* Updated based on AS-BUILT data
* SQ 5 7 10 515 1021 1527 2031 2537 3059 35
* SE4475.4 4475.92 4476.6 4477.64 4478.54 4479.28 4479.95 4480.59 4481.25 4481.
* previous data
* SQ 5 7 10 515 1521 2027 2533 3038 3059 35
* SE4475.4 4475.92 4476.6 4477.6 4478.5 4479.3 4480.1 4480.7 4481.3 4481
555 KK BAS1DS
556 DT 36DIVQ 130
* ***** 100' WEIR *****
557 DI 10 515 1521 2027 2533 3038 3059 3562 4065
558 DQ 10 15 21 27 33 38 59 62 65
*
*

HEC-1 INPUT

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1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

559 KK POND2
560 KM POND 2 WILL OUTFLOW OVER NATURAL GROUND WITH NO DETENTION. THE FLOW
561 KM WILL BE ROUTED OVERLAND TO THE FIRST COMBINATION POINT IN THE WETLANDS.
562 RM 1 0.2 0.2
*
*
563 KK T-1
564 BA 0.036
565 PB 2.5
566 LS 74 68
567 UD 0.20
*
*
568 KK RT T2 ROUTING POD T-1 THRU CHANNEL T-1 TO CPT2
569 RD 300 0.01 0.030 TRAP 10 3
*
*
570 KK T-2
571 BA 0.065
572 PB 2.5
573 LS 73 70
574 UD 0.21

```

+
575 KK CPT2 COMBINING PODS T1 AND T2
576 HC 2
577 KK RT T3 ROUTING CPT2 THRU CHANNEL T-2 TO CPT3
578 RD 970 0.01 0.030 TRAP 10 3
*
579 KK T-3
580 BA 0.061
581 PB 2.5
582 LS 79 78
583 UD 0.22
*
584 KK CPT3
585 HC 2
*
586 KK CPD1A COMBINING TAHOE AND CPT3 AND SPLIT FROM STEAMBOAT
587 HC 2
*
588 KK RT WT ROUTE TO CPWET
589 RM 3 0.2621 0.1
*
* East side drainages

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1

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
590 KK WSF1 East side watershed F1
591 BA 0.775
592 PB 2.80
593 LS 77
594 UD .24
*
595 KK WSE1 East side watershed E
596 BA 2.1
597 PB 2.8
598 LS 78
599 UD .53
*
600 KK FIE1 COMBINE F1 & E1
601 HC 2
*
602 KK C-2
603 BA 0.034
604 PB 2.5
605 LS 62 20
606 UD 0.17
*
607 KK RT C3 ROUTING C-2 THRU CHANNEL C-3 TO CPC3
608 RD 1050 0.005 0.030 TRAP 65 3
*
609 KK C-1C
610 BA 0.070
611 PB 2.5
612 LS 63 50
613 UD 0.20
*
614 KK RT C3 ROUTING C-1C THRU CHANNEL C-3 TO CPC3
615 RD 1050 0.005 0.030 TRAP 65 3
*
616 KK C-3
617 BA 0.034
618 PB 2.5
619 LS 63 20
620 UD 0.18
*
621 KK CPC3
622 HC 4

```

1

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
623 KK RT C4 ROUTING CPC3 THRU CHANNEL C-4 TO CPC4
624 RD 550 0.005 0.030 TRAP 65 3
*
625 KK C-4
626 BA 0.040
627 PB 2.5
628 LS 65 64
629 UD 0.19
*
630 KK CPC4 COMBINE CPC3 AND POD C-4
631 HC 2
632 KK RT C7 ROUTING CPC4 THRU CHANNEL C-5 TO CHANNEL C-7
633 RD 1700 0.005 0.030 TRAP 70 3
*
634 KK RT C7 ROUTING CPC4 THRU CHANNEL C-7 TO CPC7
635 RD 1400 0.0045 0.030 TRAP 75 3
*

```

636 KK C-5
 637 BA 0.068
 638 PB 2.5
 639 LS 70 63
 640 UD 0.20

 641 KK RT C7 ROUTING POD C-5 THRU CHANNEL C-5 TO CHANNEL C-7
 642 RD 100 0.005 0.030 TRAP 70 3

 643 KK RT C7 ROUTING POD C-5 THRU CHANNEL C-7 TO CPC7
 644 RD 1400 0.0045 .030 TRAP 75 3
 *

 645 KK C-7
 646 BA 0.026
 647 PB 2.5
 648 LS 81 70
 649 UD 0.16
 *

 650 KK C-6
 651 BA 0.125
 652 PB 2.5
 653 LS 64 20
 654 UD 0.23

 655 KK RT C7 ROUTING POD C-6 THRU CHANNEL C-6 TO CHANNEL C5
 656 RD 2000 0.0120 0.030 TRAP 10 3
 HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

657 KK RT C7 ROUTING POD C-6 THRU CHANNLE C-5 TO CHANNEL C-7
 658 RD 100 .005 0.03 TRAP 3

 659 KK RT C7 ROUTING POD C-6 THRU CHANNEL C-7 TO CPC7
 660 RD 1400 0.0045 0.030 TRAP 75 3

 661 KK CPC7 COMBINING CPC4 AND PODS C-5, C-7, C-6
 662 HC 4

 663 KK RT WT ROUTING CPC7 TO CPWET
 664 RM 2 0.1804 0.1
 *

 665 KK W-1
 666 BA 0.065
 667 PB 2.5
 668 LS 81 65
 669 UD 0.22

 670 KK RT W1 ROUTING POD W-1 TO CPWET
 671 RM 1 .1 .1

 672 KK CPWET COMBINE CPC7, POD W-1, AND D1B (CET #1)
 673 HC 3

 674 KK RT W1 ROUTING CPWET TO CPWET1
 675 RM 3 0.2708 0.1
 * East side drainages

 676 KK E2A
 677 KM THIS IS A COMBINED WATERSHED (E2 & A)
 678 BA 2.1
 679 PB 2.8
 680 LS 78
 681 UD 0.53
 *

 682 KK SE-2
 683 BA 0.06
 684 PB 2.5
 685 LS 72
 686 UD 0.19

 687 KK RT S3 ROUTING POD SE-2 THRU CHANNEL SE-4B TO CPSE3
 688 RD 1300 0.045 0.035 TRAP 20 3
 *

 689 KK SE-3
 690 BA 0.053
 691 PB 2.5
 692 LS 62 23
 693 UD 0.21
 *

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

694 KK SE-1
 695 BA 0.106
 696 PB 2.5
 697 LS 62 23
 698 UD 0.22

 699 KK RT S3 ROUTING POD SE-1 THRU CHANNEL SE-4A TO CPSE3
 700 RD 1450 0.0186 0.030 TRAP 15 3
 *

 701 KK CPSE3
 702 HC 3

 703 KK RT S5 ROUTING CPSE3 THRU CHANNEL SE-5 TO CPSE5
 704 RD 920 0.006 0.030 TRAP 50 3
 *

705 KK SE-4
706 BA 0.016
707 PB 2.5
708 LS 65 20
709 UD 0.16
*

710 KK SE-5
711 BA 0.021
712 PB 2.5
713 LS 63 5
714 UD 0.15

715 KK CPSE5 COMBINE CPSE5 CPSE5 AND PODS SE-4 AND SE-5
716 HC 3

717 KK RT S7 ROUTING CPSE5 THRU CHANNEL SE-6 TO CPSE7
718 RD 1025 0.006 0.030 TRAP 50 3
*

719 KK SE-6
720 BA 0.004
721 PB 2.5
722 LS 66
723 UD 0.12

724 KK RT S7 ROUTING POD SE-6 THRU CHANNEL SE-7 TO CHANNEL SE-8
725 RD 800 0.019 0.030 TRAP 18 3
*

726 KK SE-7
727 BA 0.10
728 PB 2.5
729 LS 76 65
730 UD 0.14

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

731 KK CPSE7 COMBINE CPSE5 AND PODS SE-6 AND SE-7
732 HC 3

733 KK RT WI ROUTING CPSE-7 THRU CHANNEL SE-8 TO CHANNEL SE-9
734 RD 620 0.0060 0.030 TRAP 65 3

735 KK RT WI ROUTING CPSE-7 THRU CHANNEL SE-9 TO CPWTIN
736 RD 2000 .006 .03 TRAP 65 3
*

737 KK SE-8
738 BA 0.065
739 LS 78 64
740 UD 0.22

741 KK RTWI ROUTING POD SE-8 THRU CHANNEL SE-8 TO CHANNEL SE-9
742 RD 120 0.006 0.03 TRAP 65 3

743 KK RT WI ROUTING POD SE-8 THRU CHANNEL SE-9 TO CPWTIN
744 RD 2000 0.006 0.030 TRAP 65 3
*

745 KK W-2
746 BA 0.027
747 PB 2.5
748 LS 73 5
749 UD 0.18
*

750 KK W-3
751 BA 0.04
752 PB 2.5
753 LS 73 70
754 UD 0.18
*

755 KK CPW2
756 HC 2

757 KK RTG WI
758 RM 1 0.0567 0.1

759 KK PWETIN COMBINE CPSE7 , CPW2, AND POD SE-8
760 HC 3

761 KK CPWETA COMBINE CPWTIN, OFFSITE FLOW E2A BEFORE ROUTING TO CPWET1
762 HC 2

763 KK RT W1 ROUTE CPWTIN THRU WETLANDS TO CPWET1
764 RM 2 0.1462 .1

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

765 KK CPWET1 COMBINE CPWTIN AND CPWET
766 HC 2

767 KK RTWET1
768 XM ADD ROUTING FROM CPWET1 TO CPWETB ADDED 7/2/01 DEW
769 RM 1 .2 .2
*

770 KK WET
771 BA 0.12
772 PB 2.5

773 LS 81
774 UD 0.36
775 KK CPWETB COMBINE CPWET1 AND BASIN WETR (INFLOW OF DET #1)
776 HC 2
777 KK RTWETB
778 KM ROUTE WETB TO WETO
779 RM 1 .2 .2
*
780 KK E-2
781 BA 0.07
782 LS 74 38
783 UD 0.21
784 KK RT E3 ROUTING POD E-2 THRU CHANNEL E-2 TO CPE3
785 RD 1000 0.007 0.030 TRAP 5 3
*
786 KK E-1
787 BA 0.05
788 PB 2.5
789 LS 63
790 UD 0.2
791 KK RT E3 ROUTING POD E-1 THRU CHANNEL E-1 TO CHANNEL E-2
792 RD 950 0.026 0.03 TRAP 5 3
*
793 KK RTE3
794 RD 1000 .007 .03 TRAP 5 3
795 KK CPE3 COMBINE PODS E-2 & E-1
796 HC 2
* East side drainages
797 KK WSB2
798 BA 0.12
799 PB 2.6
800 LS 76
801 UD 0.07
*

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

802 KK WSB1
803 BA 0.36
804 PB 2.8
805 LS 76
806 UD .18
807 KK CPB12 COMBINE WATERSHEDS B1 & B2
808 HC 2
809 KK RT E3 ROUTING WSB12 THRU CHANNEL E-3A TO CHANNEL E-3B
810 RD 1350 0.046 0.035 TRAP 15 3
811 KK RT E3 ROUTING WSB12 THRU CHANNEL E-3B TO CPE3
812 RD 1300 0.0063 0.030 TRAP 15 3
813 KK RT E4 ROUTING CPE3 THRU CHANNEL E-4 TO CPE-4
814 RD 970 0.0035 0.030 TRAP 15 3
815 KK E-4
816 KM MODIFY E-4, INCLUDE OLD E-3. THESE 2 ARE NOW THE HIGH SCHOOL SITE
817 BA 0.1
818 PB 2.5
819 LS 86
820 UD 0.2
821 KK RT E4 ROUTING POD E-4 THRU CHANNEL E-4 TO CPE-4
822 RD 430 0.0035 0.030 TRAP 15 3
823 KK CPE4 COMBINE CPE3 AND POD E-4
824 HC 3
*
825 KK W-8
826 BA 0.063
827 PB 2.5
828 LS 81 63
829 UD 0.19
830 KK CPWETO
831 HC 3
832 KK RS DT2 ROUTE THRU DET #2
833 KM BELOW IS DATA FOR THE RESERVOIR ABOVE TRAPEZ WEIR, CALLED DT2 OR POND 3
834 KM DT2 INCLUDES PORTION OF WETLAND AS STORAGE
835 RS 1 FLOW -1
836 SA 0 3.1 10.4 20 27.3 32.8 37.7 43.2 48.4 53.4
837 SA 58.0
838 SE 4452 4453 4454 4455 4456 4457 4458 4459 4460 4461
839 SE 4462
840 KM INSERT TRAPEZOIDAL WEIR, CREST LENGT=65', ELEV=4454, Z=.25H:1V
841 KM LOW FLOW OUTLET IS 24" RCP AT IE=4451.3, ASSUMED TO BE INEFFECTUAL AFTER
842 KM WATER ELEVATION OVER WEIR REACHES 4455
843 SQ 0 3 8 110 285 567 941 1409 1975 2645
844 SQ 3421
* SQ 0 6 15 168 378 693 1076 1509 1991 25
* SQ 3089
* SQ 0 7 16 189.5 496 888 1344 1796 2336 29
* SQ 3626
* SQ 0 3 8 110 285 567 941 1409 1975 26

* SQ 3421
*

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

845 KK W-9
846 BA 0.041
847 PB 2.5
848 LS 81 64
849 UD 0.19
*

850 KK CW-9
851 KM COMBINE W-9 & CPWETO
852 HC 2
*

853 KK POND4
* KO 1
854 KM ROUTE THRU POND 4 JUST UPSTREAM OF DAMONTE PKWY CULVERT
855 KM OUTLET MODELED AS 5 BOX CULVERTS 4' X 12'
856 RS 1 STOR 0
857 SA 0.02 2.93 6.18 9.21 13.70 17.95 22.95 25.19 25.84
858 SE 4450 4451 4452 4453 4454 4455 4456 4457 4458
859 SQ 0 200 500 950 1450 2000 2500 2800
860 SE 4450 4451.08 4452 4453.07 4454.06 4455.04 4456.01 4456.7
*

861 KK WET-IN
862 KM COMBINE OFFSITE FLOW IN THE WETLANDS FROM THE SOUTH W/ ONSITE DRAINAGE
863 HC 2
* East side drainage
*

864 KK D1
865 BA 1.72
866 PB 2.8
867 LS 78
868 UD .45

869 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-2 TO CHANNEL NE-4A
870 RD 1150 .030 .035 TRAP 25 3

871 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-4A TO CHANNEL NE-5
872 RD 2500 .0236 .035 TRAP 25 3

873 KK RT N1 ROUTING BASIN D1 THRU CHANNEL NE-5 TO CPNE-1
874 RD 800 0.0040 0.030 TRAP 80 3
*

875 KK WSC
876 BA 3.31
877 PB 2.8
878 LS 79
879 UD .65
*

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

880 KK RT N1 ROUTING BASIN WSC THRU CHANNEL NE-4A TO CHANNEL NE-5
881 RD 2500 0.0236 0.035 TRAP 25 3

882 KK RT N1 ROUTING BASIN WSC THRU CHANNEL NE-5 TO CPNE1
883 RD 800 0.0040 0.030 TRAP 80 3
*

884 KK NE-1
885 BA 0.044
886 PB 2.5
887 LS 63 34
888 UD 0.24

889 KK RT N1 ROUTING POD NE-1 THRU CHANNEL NE-5 TO CPNE1
890 RD 100 0.004 0.03 TRAP 80 3
*

891 KK CPNE1 COMBINE OFFSITE FLOW WSC AND D1 WITH NE-1
892 HC 3
*

893 KK RT W3 ROUTING CPNE1 THRU CHANNEL NE-6
894 RD 670 .004 .03 TRAP 80 3

895 KK RT W3 ROUTING CPNE1 TO CPWET3
896 RM 3 1 0.1
*

897 KK D2
898 BA 0.15
899 PB 2.6
900 LS 78
901 UD 0.06
*

902 KK RT N4 ROUTING BASIN D2 THRU CHANNEL NE-1 TO CHANNEL NE-3A
903 RD 1300 0.0192 0.035 TRAP 5 3
*

904 KK RT N4 ROUTING BASIN D2 THRU CHANNEL NE-3A TO CHANNEL NE-3B

```

905      RD      1100      0.03      0.035          TRAP          5          3
*
906      KK      RT N4 ROUTING BASIN D2 THRU CHANNEL NE-3B TO CPNE4
907      RD      2050      0.0143     0.030          TRAP          15         3
*
* * * NOTE: THE FLOWPATHS OF NE-2 THRU 5 HAVE BEEN CORRECTED
* * * AS PER THE 4/2005 SITE PLAN, HOWEVER WERE COMBINED
* * * INTO NE2345. TO SUBDIVIDE IT AGAIN, CHECK THE
* * * ROUTING CARDS- APPEARS TO BE MUSKINGUM OVERLAND FLOW
* * *

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1

HEC-1 INPUT

PAGE 30

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

908      KK      NE2345
909      KM      COMPOSITE WATERSHED, INCLUDES BASINS FORMERLY KNOWN AS
910      KM      NE-2, NE-3, NE-4, & NE-5
911      BA      0.2320
912      PB      2.5
913      LS          65          30
914      UD      0.21
*
*
* KK      NE-3
* BA      0.054
* PB      2.5
* LS          68          34
* UD      0.25
* KK      RT N5 ROUTING POD NE-3 OVERLAND TO CPNE5
* RM      3      0.2566     0.1
*
*
* KK      NE-2
* BA      0.057
* PB      2.5
* LS          69          34
* UD      0.24
*
* KK1CHNLH (CENTRAL) CHANNEL H DRAINING OFFSITE BASIN D2, NE-3, NE-2
* KM      UPSTREAM SECTION OF CHANNEL H
* HC      3
*
* KK      RT N1 ROUTING POD NE-2 THRU CHANNEL NE-5 TO CPNE-1
* RD      800      0.0040     0.030          TRAP          80         3
*
*
* KK      NE-5
* BA      0.051
* PB      2.5
* LS          44          38
* UD      0.23
*
* KK      NE-4
* BA      0.070
* PB      2.5
* LS          43          64
* UD      0.21
*
*
* KK2CHNLH (CENTRAL) CHANNEL H
* KM      DOWNSTREAM SECTION OF CHANNEL H
* KO      3
* HC      3
*
* KK      RT DN ROUTING CPNE5 OVERLAND THRU THE WETLANDS TO CPDN
* RM      2      0.1741     0.1
*
*

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1

HEC-1 INPUT

PAGE 31

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

915      KK      CPNE4   COMBINE BSIN D2 AND POD NE-4
916      KO      3
917      HC      2
*
918      KK      RT W3 ROUTING CPNE4 TO CPWET3
919      RM      10      1          .1
*
*
920      KK      CPWET3  COMBINE CPWETO AND CPNE4
921      KO      3
922      HC      2
*
*
923      KK      RT DN ROUTING CPWET3 TO CPDN OFFSITE
924      RM      6      0.4830     0.1
*
*
*
925      KK      DMNTE   DOWNSTREAM CP TO SUM DAMONTE FLOW
* KO      3
926      HC      2
*
*
927      KK      BV 14   BELLA VISTA ONSITE WATERSHED
928      BA      .007
929      LS          84
930      UD      0.167
*
* KKStm+14

```

* HC 2

931 KK RT 14 ROUTE 14 TO 13
 932 RD 875 .0024 .035 TRAP 200 3
 *
 933 KK BV 13 BELLA VISTA ONSITE WATERSHED
 934 BA .005
 935 LS 87
 936 UD 0.167
 *
 937 KK D4 BELLA VISTA RANCH OFFSITE WATERSHED D4
 938 KM OFFSITE WATERSHED D
 939 PB 2.5
 940 BA 0.80
 941 LS 73
 942 UD .77
 *

1

HEC-1 INPUT

PAGE 32

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

943 KK RT D4
 944 RM 3 0.57 .1
 *
 945 KK StmBV3
 946 HC 5
 947 KO 3
 *
 948 KK RT 13 ROUTE 13 TO 12
 949 RD 1300 .0024 .035 TRAP 200 3
 *
 950 KK BV 12 BELLA VISTA ONSITE WATERSHED
 951 BA .031
 952 LS 85
 953 UD 0.167
 *
 954 KK StBV33
 955 KO 3
 956 HC 2
 *
 957 KK RT 12 ROUTE 12 TO 11
 958 RD 550 .0024 .035 TRAP 200 3
 *
 959 KK BVW 7 BELLA VISTA -DEVELOPED- ONSITE WATERSHED
 960 KM USE TO SIZE CULVERT
 961 PB 2.4
 962 BA .062
 963 LS 83
 964 UD 0.283
 *
 965 KK RT W7
 966 RD 500 .0025 .035 TRAP 5
 *
 967 KK BV 8 BELLA VISTA ONSITE WATERSHED
 968 KM BEGIN EAST-WEST CHANNEL
 969 PB 2.4
 970 BA .023
 971 LS 83
 972 UD 0.167
 *

1

HEC-1 INPUT

PAGE 33

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

973 KK BV 7 BELLA VISTA ONSITE WATERSHED
 974 BA .016
 975 LS 90
 976 UD 0.167
 *
 977 KK 7+8
 978 HC 3
 *
 979 KK RT
 980 RD 600 .0025 .035 TRAP 5
 *
 981 KK BV 6 BELLA VISTA ONSITE WATERSHED
 982 BA .009
 983 LS 90
 984 UD 0.167
 *
 985 KK BV 9 BELLA VISTA ONSITE WATERSHED
 986 BA .018
 987 LS 83
 988 UD 0.167
 *
 989 KK 6+9
 990 HC 3

```

*
991 KK RT
992 RD 315 .0025 .035 TRAP 5
*
993 KK BV 5 BELLA VISTA ONSITE WATERSHED
994 BA .005
995 LS 83
996 UD 0.167
*
997 KK BV 10 BELLA VISTA ONSITE WATERSHED
998 BA .015
999 LS 83
1000 UD 0.167
*
1001 KK 5+10
1002 HC 3
*

```

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1003 KK RT
1004 RD 850 .0025 .035 TRAP 5
*
1005 KK BV 11 BELLA VISTA ONSITE WATERSHED
1006 BA .012
1007 LS 84
1008 UD 0.167
*
1009 KK EST-WST
1010 KM EAST-WEST CHANNEL OUTLET TO STEAMBOAT CRK
1011 HC 2
*
* KK BV 12 BELLA VISTA ONSITE WATERSHED
* BA .031
* LS 85
* UD 0.167
*
* KK RTto11
* RD 550 .0024 .035 TRAP 200 3
*
* KK D3 BELLA VISTA RANCH OFFSITE WATERSHED D3
* KM BELLA VISTA RANCH OFFSITE WATERSHED D3
* BA 0.7
* LS 79
* UD 0.77
*
* KK RT03
* RM 9 1.47 .1
*
* KK DR-6 PART OF BELLA VISTA PHASE 2
* BA .029
* PB 2.4
* LS 87
* UD .167
*
1012 KK StmBV2
1013 KM COMBINATION POINT APPROX. @ PT02,
1014 KM WHERE THE CENTRAL CHANNEL & OFFSITE WATERSHED D3 JOIN
1015 HC 2
*
1016 KK RTto4
1017 RD 550 .0024 .035 TRAP 200 3
*

```

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1018 KK BV 4 BELLA VISTA ONSITE WATERSHED
1019 BA .012
1020 LS 90
1021 UD 0.167
*
1022 KK Stm+ 4
1023 HC 2
*
1024 KK RTto3
1025 RD 500 .0025 .035 TRAP 200 3
*
1026 KK BV 3 BELLA VISTA ONSITE WATERSHED
1027 BA .012
1028 LS 90
1029 UD 0.167
*
* KK DR-5 PART OF BELLA VISTA PHASE 2
* BA .103
* PB 2.4
* LS 78
* UD .167
*
1030 KK Stm+ 3

```

1031 HC 2
 *
 1032 KK RTto2
 1033 RD 500 .0025 .035 TRAP 200 3
 *
 1034 KK BV 2 BELLA VISTA ONSITE WATERSHED
 1035 BA .007
 1036 LS 83
 1037 UD 0.167
 * *
 *
 * KK DR-7 PART OF BELLA VISTA PHASE 2
 * BA .096
 * LS 49
 * UD .167
 *
 1038 KK Stm+ 2
 1039 HC 2
 *
 *

HEC-1 INPUT

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1040 KK RTStBV1 ROUTE Stm+ 2 TO StBV1
 1041 RD 300 .0024 .035 TRAP 200 3
 *

1042 KK BVW 8 DEVELOPED BELLA VISTA ONSITE WATERSHED
 1043 PB 2.5
 1044 BA .0431
 1045 LS 83
 1046 UD 0.167
 *

1047 KK BV 1 BELLA VISTA ONSITE WATERSHED
 1048 BA .031
 1049 LS 90
 1050 UD 0.167
 *

1051 KK HC1+8 COMBINE BVW 8 AND BV1 IN WESTERN CHANNEL
 1052 HC 2
 * *

1053 KK StmBV1 COMBINATION POINT AT NORTH END OF BELLA VISTA PHASE 1A AND 1B
 1054 HC 2
 * *

* KKRTBVL ROUTE StmBV1 TO BVL
 * RD 1500 .0024 .035 TRAP 200 3
 *

* *****
 * DR-2, DR-3, AND DR-4 PART OF VISTA PHASE 2
 * *****

* KK DR-2
 * BA .041
 * PB 2.4
 * LS 90
 * UD .167
 *

* KK DR-3
 * BA .029
 * PB 2.4
 * LS 90
 * UD .167
 *

* KK DR-4
 * BA .070
 * PB 2.4
 * LS 75
 * UD .167
 *

* KKCPBVL
 * KM Downstream (North) Boundary of current Bella Vista Bndry
 * KM This sums all drainage on the east side of Bella Vista
 * HC 4
 *
 *

HEC-1 INPUT

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1055 KK RT03 ROUTE TOTAL FLOW TO CONFLUENCE AT PT03
 1056 RM 28 2.33 0.10
 *

1057 KK D3 BELLA VISTA RANCH OFFSITE WATERSHED D3
 1058 KM BELLA VISTA RANCH OFFSITE WATERSHED D3
 1059 BA 0.7
 1060 LS 79
 1061 UD 0.77
 *

1062 KK RT03
 1063 RM 9 1.47 .1
 *

1064 KK PT03

1065 HC 2
 *
 *
 * * FOLLOWING DAMONTE BASINS DRAIN TO THE WESTERN PERIMETER DITCH
 *
 1066 KK A22
 1067 PB 2.8
 * KK DR 1
 1068 BA 0.004
 1069 LS 91
 1070 UD 0.531
 *
 *
 1071 KK A5
 * KK DR 4
 1072 BA 0.047
 * BA 0.045
 1073 LS 83
 1074 UD .313
 *
 *
 1075 KK CARAT1
 1076 KM CARAT DR. CULVERT #1
 1077 HC 2
 *
 *
 1078 KK A4
 * KK DR 6
 1079 BA 0.017
 1080 LS 90
 1081 UD .197
 *
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1082 KK A23
 1083 BA 0.004
 1084 LS 85
 1085 UD 0.531
 *
 *
 1086 KK A1
 * KK DR 8
 1087 BA 0.014
 * BA 0.051
 1088 LS 90
 1089 UD .289
 *
 *
 1090 KK CHNL-A
 1091 KM CHNL-A DAMONTE WESTERN PERIMETER DITCH AT DAMONTE-BELLA VISTA BNDRY
 1092 HC 4
 *
 * BELLA VISTA WATERSHEDS BVW-5. -3, -2 DISCHARGE TO WESTERN CHANNEL
 1093 KK BVW-5 BELLA VISTA ONSITE SUBBASIN DISCHARGING TO WESTERN CHANNEL
 1094 PB 2.4
 1095 BA .049
 1096 LS 90
 1097 UD .167
 *
 *
 1098 KK ACHBV5 COMBINE BVW-5 WITH FLOW IN WESTERN CHANNEL FROM DAMONTE V
 1099 HC 2
 *
 *
 1100 KK RT5-3 ROUTE BVW-5 TO BVW-3
 1101 RD 1800 .0024 .035 TRAP 10 3
 *
 *
 1102 KK BVW-3
 1103 PB 2.4
 1104 BA .0501
 1105 LS 79
 1106 UD .167
 *
 *
 1107 KK CP3&5 COMBINE BVW-3 AND BVW-5
 1108 HC 2
 *
 * KK RT3-1 ROUTE FROM BVW 3 TO BVW-1
 * RD 735 .0024 .035 TRAP 10 3
 *

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1109 KK BVW-1 BELLA VISTA ONSITE WATERSHED 1
 1110 PB 2.4
 1111 BA .0271
 1112 LS 81
 1113 UD .167
 *
 *
 1114 KK WSTOUT COMBINE FLOWS AT DOWNSTREAM END OF WESTERN CHANNEL
 1115 HC 2
 *
 *
 * KK DR-1 BELLA VISTA PHASE 2 VILLAGE 1
 * BA .053

```

* LS          86
* UD   .167
*
* KKCPBVR  COMBINATION POINT AT NORTH END OF BELLA VISTA PHASE 1A AND 1B
* HC      2
1116 KK   RT03  ROUTE TOTAL FLOW TO CONFLUENCE AT PT03
1117 RM   28   2.33  0.10
*
1118 KK   PT03  COMBINATION POINT AFTER BELLA VESTA
1119 HC   2
* [FOLLOWING IS PRE-DEV. BASINS THAT ARE PLANNED FOR DEVELOPMENT]
*
* KK   W-4
* BA  0.038
* PB   2.5
* LS          79      68
* UD   0.18
* KK RT W6 ROUTING POD W-4 THRU CHANNEL NW-1 TO CHANNEL NW-2
* RD   650  0.0038  0.030      TRAP   5      3
* KK RT W6 ROUTING POD W-4 THRU CHANNEL NW-2 TO CPW6
* RD   700  0.0021  0.030      TRAP   5      3
*
* KK   W-5
* BA  0.013
* PB   2.5
* LS          77      65
* UD   0.14
* KK RT W6 ROUTING POD W-5 THRU CHANNEL NW-2 TO CPW6
* RD   700  0.0021  0.030      TRAP   5      3
*
* KK   W-6
* BA  0.017
* PB   2.5
* LS          77      5
* UD   0.15
* KK CPW6  COMBINE PODS W-4, W-5 AND W-6
* HC      3
*
*
* KKRT DT2 ROUTING CPW6 THRU CHANNEL NW-3A TO CHANNEL NW-4
* RD   350  0.0086  0.030      TRAP   5      3
* KKRT DT2 ROUTING CPW6 THRU CHANNEL NW-4 TO CPDT2
* RD  1200  0.005   0.030      TRAP   5      3
*
*
* * NW-2 IS BEING DEVELOPED UNDER PHASE V
* KK   NW-2
* BA  0.066
* PB   2.5
* LS          78      50
* UD   0.26
*
* KKRT DT2 ROUTING POD NW-2 THRU CHANNEL NW-3B TO CHANNEL NW-4
* RD   285  0.006   0.030      TRAP   0      3
*
*
* KK   W-7
* KM USED TO DRAIN TO WETLANDS, NOW IS ROUTED UNDER STEAMBOAT PKWY TO A10
* KM WAS DEVELOPED BY OTHERS, NOW KNOWN AS "EXIST. DAMONTE RANCH 12&13 (AREA 16)
* BA  0.053
* PB   2.5
* LS          76      70
* UD   0.17
* KK CPDT2  COMBINE CPW6 AND PODS NW-2 AND W-7
* HC      3
*
* KK RT N1 ROUTING CPDT2 THRU CHANNEL NW-5 TO CHANNEL NW-6
* RD  2275  0.0022  0.030      TRAP   5      3
* KK RT N1 ROUTING CPDT2 THRU CHANNEL NW-6 TO CPN1
* RD  1650  0.0014  0.030      TRAP  15      3
*
*
* * NW-3 IS BEING DEVELOPED UNDER PHASE V
* KK   NW-3
* BA  0.076
* PB   2.5
* LS          73      65
* UD   0.22
* KK RT N1 ROUTING POD NW-3 THRU CHANNEL NW-6 TO CPN1
* RD  1650  0.0014  0.030      TRAP  15      3
*
*
*
* * NW-1 IS PARTIALLY BEING DEVELOPED UNDER PHASE V
* KK   N-1
* BA  0.02
* BA  0.104
* PB   2.5
* LS          76      68
* UD   0.29
*
* KK CPN1  COMBINE CPDT2 AND PODS NW-3 , N-1
* HC      3
*
* KKRT N13 ROUT CPN1 THRU CHANNEL NW-7 TO CPN13
* RD   800  .001   .03      TRAP  18      3
*
*
*
* * S-6 & S-7 ARE BEING DEVELOPED UNDER PHASE V
* KK   S-6
* BA  0.038
* PB   2.5
* LS          73      64
* UD   0.24

```

```

* *
* KKRT ST2 ROUTING POD S-6 THRU STEAMBOAT TO CPSTM2
* RM 8 0.6266 .4
* *
* KK S-7
* BA 0.046
* PB 2.5
* LS 73 64
* UD 0.23
* *
* *
* *
* KKRT N13 ROUTING CPN4STM2 TO CPN13
* RM 10 0.8647 .4
* *
* *
* * N-2 & N-3 ARE BEING DEVELOPED UNDER PHASE V
* *
* KK N-2
* BA 0.047
* PB 2.5
* LS 75 68
* UD 0.21
* *
* *
* KK N-3
* BA 0.030
* PB 2.5
* LS 80 5
* UD 0.11
* *
* KK CPN13 COMBINE CPN1, CPNST AND PODS N-2 AND N-3
* HC 2
* KK CPDN CPN13, CPWET3, CPN5 AND OUTDN ROUTED TO CPDN, NORTH BNDY OF DAMONTE
* HC 3
* *

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[END 443LOMR.dat]

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* *
* *****
* Routing flow from Damonte property line to Bella Vista Ranch model
* *****
* KK RT01 ROUTING OF FLOW FROM DAMONTE
* RM 8 1.25 0.1
* KK D4 BELLA VISTA RANCH WATERSHED 4
* KM CALCULATE RUNOFF FROM WATERSHED 4
* BA 0.80
* PB 2.5
* LS 73
* UD .77
* KK PT01 COMBINE FLOW FROM DAMONTE (RT01) WITH WATERSHED 4
* HC 2
* *
* *
* KK RT02 ROUTE TO CONFLUENCE WITH WATERSHED 3
* RM 3 0.57 .1
* KK D3 BELLA VISTA RANCH WATERSHED 3
* KM CALCULATE RUNOFF FROM WATERSHED 3
* BA 0.7
* PB 2.5
* LS 79
* UD 0.77
* KK PT02 COMBINE FLOWS FROM WATERSHED 3 WITH RT02
* HC 2
* KK RT03 ROUTE TOTAL FLOW TO CONFLUENCE WITH WATERSHED 2
* RM 9 1.47 .1
* *

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* *
* *****
* File name : 02BAS-PH1.DAT (NOV 2000) - Includes only the section of this
* model that starts at "Begin Double Diamond Model" with watershed #18RB.
* This model was modified from AS-PH1.DAT (MAY 1995); Whites Creek Branches
* 3 & 4 were diverted to Steamboat Creek.
* DOUBLE DIAMOND SUBDIVISION-PROJECT #0028 HYDROLOGIC & HYDRAULIC ANALYSIS
* SOUTH MEADOWS PARKWAY & CENTRAL CHANNEL
* SOUTH MEADOW/DOUBLE DIAMOND
* BY NIMBUS ENGINEERS, RENO, NV
* 100-Year, 24 hour model
* WHITES CREEK MODEL COPIED FROM WHITECN.DAT
* FIS THOMAS CREEK 100-YEAR PEAK = 2544 CFS @ S. VIRGINIA STREET.
* WHITES CREEK SUBBASIN W18RB-NORTH OF WHITES CREEK BRANCH #3 DIVERSION
* ADD PHASE I, PHASE VI AND PHASE V TO CENTRAL CHANNEL
* FROM CARAT AVE TO END OF CENTRAL CHANNEL
* MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE I (PORTIONS OF VILLAGES 11 AN
* , PHASE I (VILLAGES 1, 2, 3 AND 4), PHASE VI )PARK, K-6 SCHOOL, AND VILLAGE 29
* AND PHASE V (VILLAGES 24 AND 25)
* 100-YEAR, 24-HOUR MODEL
* MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE II (VILLAGES 5 & 6 AND PARKS)
* , PHASE III (VILLAGES 16, 17, 18, AND 19), AND PHASE IV (VILLAGES 7, 8, 9,
* 20, 21, 22, AND 23) PLUS WETLAND BETWEEN VILLAGES 18/19 & 20.
* USE SUBBASIN AREAS FROM MACKAY & SOMPS
* NIMBUS ENGINEERS, RENO, NEVADA
* MODEL MODIFIED FROM CARATDD.DAT (#9908)
* *****

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1120 KK W18RB WHITES CREEK SUBBASIN W18RB-NORTH BOUNDARY OF WHITES CK MEADOW SUBDIV.
 1121 KM DAMONTE RANCH NORTH OF WHITES CK. BRANCH #3 AND SOUTH OF DOUBLE DIAMOND
 1122 KM W18RB AREA REDUCED DUE TO ROUTING OF A PORTION OF IT TO STEAMBOAT CREE
 1123 KM NEW WATERSHED DRAINING TO STEAMBOAT CREEK, HD IS UPSTREAM OF DIVSTR
 * BA .2344
 1124 BA .133
 1125 PB 2.6
 * LS 85
 * UD 0.30
 1126 LS 95
 1127 UD .24
 *
 1128 KK V18-19 DOUBLE DIAMOND VILLAGES 18 & 19
 1129 BA .0548
 1130 LS 92
 1131 UD 0.24
 1132 KK V20 DOUBLE DIAMOND VILLAGE 20
 1133 BA 0.0450
 1134 LS 92
 1135 UD 0.21
 1136 KK WET WETLANDS # 5 & #6 BETWEEN VILLAGES 18/19 AND VILLAGE 20
 1137 BA .0153
 1138 LS 80
 1139 UD 0.26
 1140 KK CB WET COMBINE W18RB, V18-19, V20, & WET RUNOFF HYDROGRAPHS IN THE WETLAND
 1141 KM BETWEEN VILLAGES 18/19 AND VILLAGE 20
 1142 HC 4
 1143 KK PH-IV PHASE IV DOUBLE DIAMOND DEVELOPMENT (VILLAGES 7,8,9,21,22,&23).
 1144 KM VILLAGE 20 WAS MODELED ABOVE WITH FLOW ENTERING THE WETLAND SOUTH
 1145 KM OF WILBUR MAY BLVD. DETAILED DRAINAGE PLANS WERE NOT AVAILABLE
 1146 KM AND AS A RESULT THE PHASE IV VILLAGES LIST FOR PH-IV WERE COMBINED.
 1147 KM AS PLANS ARE DEVELOPED, THE VILLAGES CAN BE MODELED SEPARATELY.
 1148 BA 0.1931
 1149 LS 92
 1150 UD 0.31
 1151 KK E14 HYDROGRAPH FROM VILLAGE 6 DRAINAGE POINT E14
 1152 KM CALCULATE RUNOFF FROM SUBBASIN E14
 1153 BA .025
 1154 LS 92
 1155 UD .225
 1156 KK C14
 1157 KM COMBINE RUNOFF FROM E14 WITH CENTRAL CHANNEL FLOW (FLOW FROM RT1617 & PH-IV)
 1158 HC 3

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 1159 KK E14-E1
 1160 KM ROUTE FLOW TO E1 ALONG CENTRAL CHANNEL
 1161 RD 400 .004 .030 TRAP 100 3
 1162 KK E1
 1163 KM CALCULATE RUNOFF FROM SUBBASIN E1-VILLAGE 5
 1164 BA .0058
 1165 LS 92
 1166 UD .135
 1167 KK C1
 1168 KM COMBINE RUNOFF FROM E1 WITH CENTRAL CHANNEL FLOW
 1169 HC 2
 1170 KK E1-E2
 1171 KM ROUTE FLOW TO E2 ALONG CENTRAL CHANNEL
 1172 RD 300 .004 .030 TRAP 100 3
 1173 KK E2
 1174 KM CALCULATE RUNOFF FROM SUBBASIN E2-VILLAGE 5
 1175 BA .003
 1176 LS 92
 1177 UD .118
 1178 KK C2
 1179 KM COMBINE RUNOFF FROM E2 WITH CENTRAL CHANNEL FLOW
 1180 HC 2
 1181 KK E2-E3
 1182 KM ROUTE FLOW TO E3 ALONG CENTRAL CHANNEL
 1183 RD 300 .004 .030 TRAP 100 3
 1184 KK E3
 1185 KM CALCULATE RUNOFF FROM SUBBASIN E3-VILLAGE 5
 1186 BA .0025
 1187 LS 92
 1188 UD .119
 1189 KK C3
 1190 KM COMBINE RUNOFF FROM E3 WITH CENTRAL CHANNEL FLOW
 1191 HC 2
 1192 KK E3-E4
 1193 KM ROUTE FLOW TO E4 ALONG CENTRAL CHANNEL
 1194 RD 360 .004 .030 TRAP 100 3
 1195 KK E4
 1196 KM CALCULATE RUNOFF FROM SUBBASIN E4-VILLAGE 5
 1197 BA .003
 1198 LS 92
 1199 UD .113

HEC-1 INPUT

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LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1200	KK C4
1201	KM COMBINE RUNOFF FROM E4 WITH CENTRAL CHANNEL FLOW
1202	HC 2
1203	KK D10
1204	KM CALCULATE RUNOFF FROM SUBBASIN D10
1205	KM SUBBASIN D10 IS LOCATED ALONG DOUBLE DIAMOND PKWY. THE AREA DRAINED IS
1206	KM COMPRISED OF PORTIONS OF VILLAGES 5, 6, 13, 14, 15, 16 & 17 THAT BORDER THE PKWY.
1207	KM THE D10 SYSTEM IS A PARALLEL STORM DRAIN SYSTEM
1208	KM ALONG DOUBLE DIAMOND PARKWAY THAT DRAINS TO AN OPEN
1209	KM CHANNEL ALONG THE SOUTH EDGE OF THE PARK LOCATED IMMEDIATELY SOUTHEAST OF
1210	KM THE INTERSECTION OF CARAT AV. AND DOUBLE DIAMOND PKWY.
1211	BA .122
1212	LS 92
1213	UD .277
1214	KK D12
1215	KM CALCULATE RUNOFF FROM SUBBASIN D12-VILLAGE 5
1216	BA 0.0166
1217	LS 92
1218	UD 0.173
1219	KK PARK
1220	KM CALCULATE RUNOFF FROM PARK JUST SOUTH OF CARAT AVE
1221	BA .0078
1222	LS 80
1223	UD .14
1224	KK C10PRK
1225	KM COMBINE HYDROGRAPHS FROM PARK, D10, D12 AND CENTRAL CHANNEL
1226	HC 4
1227	KK PK-CAR
1228	KM ROUTE FLOW TO STATION ~62+20 ALONG CENTRAL CHANNEL
1229	RD 720 .004 .030 TRAP 100 3
1230	KK PhVa PHASE V SUB-BASIN a
1231	BA 0.011
1232	LS 92
1233	UD 0.16
1234	KK V4 DOUBLE DIAMOND VILLAGE 4 OF PHASE I
1235	BA 0.026
1236	LS 86
1237	UD 0.16
1238	KK CB 1 COMBINE PhVa AND V4 AT STATION ~62+20
1239	HC 3

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HEC-1 INPUT

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LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1240	KK RT1-2
1241	KM ROUTE TO CB 2 AT STATION ~74+65
1242	RD 1245 .004 0.04 TRAP 100 3
1243	KK PhVb DOUBLE DIAMOND PHASE V AREA PhVb
1244	BA 0.028
1245	LS 92
1246	UD 0.23
1247	KK CB2 COMBINE PhVb WITH CENTRAL CHANNEL FLOW AT STATION ~74+65
1248	HC 2
1249	KK RT2-3 ROUTE CB2 DOWN CENTRAL CHANNEL TO CB 3 AT STATION ~79+00
1250	RD 435 .00204 0.04 TRAP 100 3
1251	KK V12 PORTION OF VILLAGE 12 THAT DRAINS TO CENTRAL CHANNEL
1252	BA 0.015
1253	LS 86
1254	UD 0.16
1255	KK V11 PORTION OF VILLAGE 11 THAT DRAINS TO CENTRAL CHANNEL
1256	BA 0.008
1257	LS 86
1258	UD 0.12
1259	KK V3 PHASE I VILLAGE 3
1260	BA 0.026
1261	LS 86
1262	UD 0.19
1263	KK CB3 COMBINE PORTIONS OF VILLAGES 11&12 WITH VILLAGE 3 AT STA 79+00
1264	HC 4
1265	KK RT3-4
1266	KM ROUTE CB3 DOWN CENTRAL CHANNEL TO CB4 AT STATION ~82+00
1267	RD 300 0.00204 0.04 TRAP 100 3
1268	KK PhVc PHASE V SUB-AREA PhVc
1269	BA 0.022
1270	LS 92
1271	UD 0.19
1272	KK V2 VILLAGE 2 OF PHASE I
1273	BA 0.04
1274	LS 86
1275	UD 0.20
1276	KK CB4 COMBINE PhVc WITH VILLAGE 2
1277	HC 3

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HEC-1 INPUT

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LINE	ID	1	2	3	4	5	6	7	8	9	10
1278	KK	RT4-5	ROUTE CB4 DOWN CENTRAL CHANNEL TO CB5 AT STATION -83+65								
1279	RD	165	0.00204	0.04	TRAP	100	3				
1280	KK	PARKVI	PHASE VI PARK								
1281	BA	0.004									
1282	LS		80								
1283	UD	0.14									
1284	KK	CB5	COMBINE PHASE VI PARK WITH CENTRAL CHANNEL FLOW AT CB5								
1285	HC	2									
1286	KK	RT5-6	ROUTE CB5 DOWN CENTRAL CHANNEL TO CB6 AT STATION -87+50								
1287	RD	385	0.00204	0.04	TRAP	100	3				
1288	KK	K6SCHL	PHASE VI K-6 SCHOOL								
1289	BA	0.013									
1290	LS		85								
1291	UD	0.15									
1292	KK	CB6	COMBINE K-6 SCHOOL WITH CENTRAL CHANNEL FLOW AT CB6								
1293	HC	2									
1294	KK	RT6-7	ROUTE CB6 DOWN CENTRAL CHANNEL TO CB7 AT STATION -101+00								
1295	KM		END OF CENTRAL CHANNEL								
1296	RD	1350	.00204	0.04	TRAP	100	3				
1297	KK	V1	PHASE I VILLAGE 1								
1298	BA	0.037									
1299	LS		86								
1300	UD	0.21									
1301	KK	V29	PHASE VI VILLAGE 29								
1302	BA	0.065									
1303	LS		92								
1304	UD	0.20									
1305	KK	CB7	COMBINATION POINT 7; END OF CENTRAL CHANNEL								
1306	HC	3									
	*		WHITES CREEK BRANCHES 1 & 2								
1307	KK	DR 1	Recall Channel 1 Hydrograph (@ Difffluence)								
1308	DR	CH 1									
1309	KK	RT Z1	Route Channel 1 to Zolezzi Lane (approx. 2800' West of Virginia St.)								
1310	RM	4	.34	.3							
1311	KK	W13R	Whites Creek No. 13								
1312	BA	1.3									
1313	PB	2.8									
1314	LS		61								
1315	UD	0.52									

HEC-1 INPUT

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LINE	ID	1	2	3	4	5	6	7	8	9	10
1316	KK	CP Z1	Combine channel 1 w/ W13R at Zolezzi Lane								
1317	HC	2									
1318	KK	DV 1B	Divert flows to the north of Zolezzi (Channel 1A)								
1319	KM		Hydrograph is for flows along Zolezzi (Channel 1B, Ea. to Virginia)								
1320	DT	CH 1A									
1321	DI	0	200	1500							
1322	DQ	0	200	200							
1323	KK	RT V12	Route Channel 1B to Virginia St.								
1324	RM	1	0.12	.25							
1325	KK	W12R	Whites Creek No. 12								
1326	BA	0.6									
1327	PB	2.8									
1328	LS		61								
1329	UD	0.45									
1330	KK	CP V12	Combine Channel 1B and W12R at int. of Virginia and Zolezzi								
1331	HC	2									
1332	KK	DR CH2	Recall Channel 2 Hydrograph								
1333	DR	CH 2									
1334	KK	RT V12	Route Flows to int. of Virginia and Zolezzi								
1335	RM	3	.221	.2							
1336	KK	CP V12	Combine channels 1B and 2 at int. of Virginia and Zolezzi								
1337	HC	2									
1338	KK	RT F12	Route flows to proposed RCB at 580 (Channels 1B and 2)								
1339	RM	2	0.201	0.2							
1340	KK	W15R	Whites Creek No. 15								
1341	BA	0.21									
1342	PB	2.7									
1343	LS		79								
1344	UD	0.21									
1345	KK	CP F12	Combine flows at proposed RCB at 580 (Channels 1B and 2)								
1346	HC	2									
1347	KK	DR 1A	Recall Channel 1A Hydrograph								
1348	DR	CH 1A									
1349	KK	RT F1A	Route flows to proposed RCB at 580 (Channel 1A)								
1350	RM	4	0.306	0.2							

1351 KK W14R Whites Creek No. 14
 1352 BA 0.18
 1353 PB 2.7
 1354 LS 77
 1355 UD 0.26

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1356 KK CP F1A Combine flows at proposed RCB at 580 (Channel 1A)
 1357 HC 2
 1358 KK CB 1&2 COMBINE WHITES CREEK BRANCHES 1 & 2 @ I-580
 1359 HC 2
 * ROUTE WHITES CREEK BRANCHES 1 & 2 TO THE CONFLUENCE W/ LUMBERJACK CHANNEL
 1360 KK RT WT2 ROUTE WHITES 1&2 THRU WS WT2P - CHANNEL "A"
 1361 RD 3040 0.0026 0.035 TRAP 135 5
 1362 KK RT WT2 ROUTE WHITES 1&2 THRU WS WT2P- PARK AND OPEN SPACE
 1363 RM 5 0.44 0.20
 1364 KK RT WT2 ROUTE WHITES CREEK 1&2 THRU WS WT2P - CHANNEL "B"
 1365 RD 1914 0.0028 0.035 TRAP 151 3
 1366 KK WT 6P1 PORTION OF PHASE I VILLAGES 11, 12, & 13 DRAINING TO "B" CHANNEL
 1367 BA 0.07
 1368 PB 2.7
 1369 LS 83
 1370 UD 0.38
 1371 KK W WT2P ON-SITE WATERSHED WT2P
 * EXISTING CONDITION(NO ON-SITE DETENTION)
 1372 BA 0.59
 1373 PB 2.7
 1374 LS 79
 1375 UD 0.73
 1376 KK CB WT2 COMBINE WHITES CREEK 1&2 & WT2P
 1377 HC 3
 1378 KK WS WT1 WATERSHED WT1 - AREAS BETWEEN WHITES CREEK AND THOMAS CREEK
 1379 BA 1.93
 1380 PB 2.75
 1381 LS 66
 1382 UD 0.97
 1383 KK RT WT3 ROUTE TO CONFLUENCE
 1384 RM 3 0.29 0.25
 1385 KK THOMAS
 * KO 1
 1386 KM HYDROGRAPH FROM FIS HYDROLOGY MODEL - THOM100.901
 1387 KM THOMAS CREEK PEAK FLOW @ S. VIRGINIA STREET
 1388 BA 11.54
 1389 QI 0 0 0 0 0 0 0 0 0 0
 1390 QI 0 0 0 0 0 0 0 0 0 0
 1391 QI 0 0 0 0 0 0 0 0 0 0
 1392 QI 0 0 0 0 0 0 0 0 2 6
 1393 QI 20 29 41 54 70 89 112 144 203 385
 1394 QI 790 1223 1828 2544 2447 1943 1462 1170 1019 933
 1395 QI 873 825 786 756 729 698 665 636 613 594
 1396 QI 577 562 549 535 521 504 481 445 407 379

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1397 QI 362 350 341 334 327 321 316 310 305 300
 1398 QI 295 291 287 282 278 275 271
 1399 KK DV HOL
 * KO 1
 1400 KM SPLIT FLOW ACROSS HOLCOMBE LANE TO NORTH.
 1401 KM REFER TO FIS HEC-2 MODEL FOR THOMAS CREEK - THOMAS A.DAT
 1402 KM SPLIT FLOW RATING CALCULATED USING THOMAS A.DAT
 1403 DT HOLCOM
 1404 DI 0 1000 2000 2550 3000 4000
 1405 DQ 0 274 955 1385 1746 2562
 1406 KK RT WT3 ROUTE TO OPEN SPACE/WETLAND
 1407 RM 2 0.167 0.25
 1408 KK DV THO THOMAS CREEK DIVERSION AT WETLAND/OPEN SPACE
 1409 DT THOM
 1410 DI 0 500 1000 1465
 1411 DQ 0 0 0 159
 1412 KK RT WT3 ROUTE TO CONFLUENCE
 1413 RM 1 0.083 0.25
 1414 KK WT3P WATERSHED WT3P - EXISTING CONDITION (NO ON-SITE DETENTION)
 1415 BA 0.49
 1416 PB 2.7
 1417 LS 79
 1418 UD 0.33
 1419 KK CB WT3 COMBINE OFFSITE FLOWS -WT1 & THOMAS CREEK & WT3P
 * KO 1
 1420 HC 3
 1421 KK CB OFF COMBINE WHITES CREEK 1&2 & THOMAS CREEK
 1422 HC 2
 1423 KK RT WHC ROUTE THRU WHITES CHANNEL "C"
 1424 RD 1689 0.0021 0.035 TRAP 150 3

*
 1425 KK D2 BELLA VISTA RANCH WATERSHED 2
 1426 KM CALCULATE RUNOFF FROM WATERSHED 2
 1427 BA 0.36
 1428 PB 2.5
 1429 LS 70
 1430 UD 0.49
 *

1431 KK CB WHC COMBINE WHITES CREEK BRANCHES 1,2,3,4 & THOMAS CREEK
 1432 HC 2
 HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1433 KK RT DET ROUTE TO DETENTION BASIN THRU PROPOSED CHANNEL
 1434 RD 1985 0.00275 0.035 TRAP 170 3
 * ROUTE THRU DETENTION BASIN

1435 KK RT DET
 1436 RS 1 FLOW -1
 * AS-BUILT VOLUME - PHASE 1
 1437 SV 0 16.64 41.62 72.60 123.04 170.39 216.38 238.26
 * PHASE 2 VOLUME - W/O ARCHEOLOGICAL SITE
 1438 SE 4422.7 4424.09 4425.20 4426.25 4427.55 4428.60 4429.52 4429.94
 1439 SQ 0 200 500 1000 2000 3000 4000 4500

1440 KK RT WT ROUTE TO CP WT
 1441 RM 1 0.06 0.15

1442 KK THOMAS RECALL DIVERSION FROM THOMAS CREEK
 1443 DR THOM

1444 KK RT WT ROUTE TO NORTHEAST PROP
 1445 RM 19 1.59 0.2
 *

1446 KK WT4P ON-SITE WATERSHED WP4P
 * EXISTING CONDITION (NO ON-SITE DETENTION)
 1447 BA 1.73
 1448 PB 2.7
 1449 LS 82
 1450 UD 1.62

1451 KK
 1452 HC 2
 *

1453 KK WT7P ON-SITE WATERSHED WT7P
 * EXISTING CONDITIONS
 1454 BA 0.16
 1455 PB 2.7
 1456 LS 80
 1457 UD 1.48

1458 KK RT WT ROUTE TO CP WT
 1459 RM 8 0.65 0.15

1460 KK WS WT5 WATERSHED WT5
 1461 BA 0.49
 1462 PB 2.65
 1463 LS 83
 1464 UD 0.28

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1465 KK RT WT ROUTE TO CP WT
 1466 RM 6 0.47 0.15

1467 KK CB WT COMBINE FLOWS AT NORTHEAST PROPERTY CORNER
 1468 HC 3

1469 KK CP WT COMBINE ALL FLOWS @ CP WT
 1470 HC 2
 *
 * FLOW FROM DOUBLE DIAMOND ONTO BELLA VISTA RANCH NORTH OF THE NARROWS
 *

1471 KK PT03 COMBINE FLOW FROM WATERSHED 2 WITH RT03 AND DOUBLE DIAMOND FLOWS
 1472 HC 3

1473 KK RT04 ROUTE TOTAL FLOW TO CONFLUENCE WITH WATERSHEDS 1 & 5, & DD
 1474 RM 11 1.77 0.1

1475 KK D1 BELLA VISTA RANCH WATERSHED 1
 1476 KM CALCULATE RUNOFF FROM WATERSHED 1
 1477 BA 0.44
 1478 PB 2.5
 1479 LS 77
 1480 UD 0.60

1481 KK D5 BELLA VISTA RANCH WATERSHED 5
 1482 KM CALCULATE RUNOFF FROM WATERSHED 5
 * BA 1.21
 1483 BA 0.75
 1484 PB 2.4
 1485 LS 74
 * UD 5.36
 1486 UD 2.68

1487 KK PT04 COMBINE FLOWS FROM WSD 1 & 5 WITH ROUTED FLOW FROM PT03
 1488 KO 3
 1489 HC 3

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
57	W1R	
	.	
72	.	W2R
	.	
77	W1+W2.....	
	V	
	V	
79	RT-A	
	.	
81	.	W3R
	.	V
	.	V
86	.	RT-A
	.	
88	.	W4R
	.	
93	W1234.....	
	V	
	V	
95	RT-B	
	.	
97	.	W5R
	.	
102	W5+CH.....	
	V	
	V	
104	RT-C	
	.	
106	.	W6R
	.	
111	W6+CH.....	
	V	
	V	
113	RT-D	
	.	
115	.	W7R
	.	
120	W7+CH.....	
	V	
	V	
122	RT-DIF	
	.	
124	.	W8R
	.	
129	CP DIF.....	
	.	
133	-----> CH 123	
131	DV 4	
	V	
	V	
136	RT W4	
	.	
138	.	W17R
	.	
143	CP W4.....	
	V	
	V	
145	RT F4	
	.	
147	.	W19R
	.	
152	.	W9R
	.	V
	.	V
157	.	RT F4
	.	
159	CP F4.....	
	V	
	V	
161	RT V4	
	.	
163	.	W20R
	.	
168	CP V4.....	
	V	
	V	
170	RT STM	

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172      .      G1G2
173      .      V
174      .      V
177      .      OUTJ1
178      .      .
179      .      .      J1
180      .      .      .
184      .      .      .      .
185      .      .      .      .
186      .      .      .      .
187      .      .      .      .
188      .      .      .      G3
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278      .      .      .      .

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283      .      CP V24.....
      .      V
      .      V
285      .      RT F3
      .      .
287      .      W16R
      .      .
292      .      CP F3.....
      .      V
294      .      RT DSW
      .      .
296      .      W18RA
      .      .
301      .      CB DSW.....
      .      .
303      .      S-1
      .      V
308      .      RT S3
      .      .
310      .      S-2
      .      V
314      .      RT S3
      .      .
316      .      S-3A
      .      V
320      .      RT S3
      .      .
322      .      CPS3A.....
      .      V
324      .      RT S5
      .      .
326      .      S-3B
      .      V
330      .      RT S5
      .      .
332      .      S-4
      .      V
336      .      RT S5
      .      .
338      .      S-5
      .      V
342      .      RT S5
      .      .
344      .      CPSS.....
      .      V
346      .      RT WHT
      .      .
348      .      CB WHT.....
      .      .
350      .      HD
      .      .
355      .      CP HD.....
      .      V
357      .      DIVSTR
      .      .
367      .      -----> BAS 1
366      .      STEAM
      .      V
372      .      OUTDM
      .      V
374      .      OUTDN
      .      .
376      .      A7
      .      .
381      .      STM+7.....
      .      .
384      .      A6
      .      .
388      .      STM+6.....
      .      .
391      .      A3
      .      .
395      .      STM+3.....

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398      .          A2
402  STM+2.....
405      .          A17
410      .          A18
414      .  CHNL-E.....
417  STM+E.....
      V
      V
422  RT NST
424      .          A16
429      .          A19
433      .          A20
437      .  CHNL-F.....
440  STM+AF.....
443      .  BVW 6
      V
      V
448      .  RT W6
450      .          BV 16
455      .  Stm+16.....
      V
      V
457      .  RT 16
459      .          BV 15
463  Stm+15.....
      V
      V
465  RT BV3
467      .  APTS-9
474      .          A8
478      .  CHNL-B.....
480      .  D12&13
485      .          A9
489      .  CHNL-C.....
492      .  B&C.....
495      .          A14
499      .          A13
503      .          A15
507      .  CHNL-D.....
510      .          A11
514      .          A12
518      .  11+12.....
521      .  CHNL D.....

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524 . . . . . X12+13
530 . . . . . A10
534 . . . . .
536 . . . . . A21
540 WTLNDS.....
545 . . . . . <----- BAS 1
543 RC BAS
544 V
545 V
546 BAS 1
547 .
556 . . . . . -----> 36DIVQ
555 BAS1DS
556 V
557 V
559 POND2
563 . . . . . T-1
564 V
565 V
566 RT T2
567 .
570 . . . . . T-2
571 .
572 .
575 CPT2.....
576 V
577 V
578 RT T3
579 .
580 . . . . . T-3
581 .
582 .
584 CPT3.....
585 .
586 CPDIA.....
587 V
588 V
589 RT WT
590 .
591 .
595 . . . . . WSE1
596 .
600 F1E1.....
601 .
602 . . . . . C-2
603 V
604 V
605 RT C3
606 .
609 . . . . . C-1C
610 V
611 V
612 RT C3
613 .
616 . . . . . C-3
617 .
621 CPC3.....
622 V
623 RT C4
624 .
625 . . . . . C-4
626 .
630 CPC4.....
631 V
632 V
633 RT C7
634 V
635 RT C7
636 .
637 . . . . . C-5
638 V
639 V
641 RT C7
642 V
643 RT C7

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645	C-7	.	.	.
650	C-6	.
655	V	.
657	V	RT C7
659	V	V
661	V	RT C7
663	V	RT C7
665
670
672
674
676
682
687
689
694
699
701
703
705
710
715
717
719
724
726
731
733
735
737
741
743
745
750
755
757

CPC7

V
V
RT WT

W-1

V
RT W1

CPWET

V
RT W1

E2A

SE-2

V
RT S3

SE-3

SE-1

V
RT S3

CPSB3

V
RT S5

SE-4

SE-5

CPSE5

V
RT S7

SE-6

V
RT S7

SE-7

CPSE7

V
RT W1

V
RT W1

SE-8

V
RT W1

V
RT W1

W-2

W-3

CPW2

V
RTG W1

759	.	.	.	PWETIN.....
761	.	.	CPWETA.....	.
763	.	.	V	.
	.	.	RT W1	.
765	.	CPWET1.....	.	.
	.	V	.	.
	.	V	.	.
767	.	RTWET1	.	.
770	.	.	WET	.
775	.	CPWETB.....	.	.
	.	V	.	.
	.	V	.	.
777	.	RTWETB	.	.
780	.	.	E-2	.
	.	.	V	.
	.	.	V	.
784	.	.	RT E3	.
786	.	.	.	E-1
	.	.	.	V
	.	.	.	V
791	.	.	RT E3	.
	.	.	V	.
	.	.	V	.
793	.	.	RTE3	.
795	.	.	CPE3.....	.
797	.	.	WSB2	.
802	.	.	.	WSB1
807	.	.	CPB12.....	.
	.	.	V	.
	.	.	V	.
809	.	.	RT E3	.
	.	.	V	.
	.	.	V	.
811	.	.	RT E3	.
	.	.	V	.
	.	.	V	.
813	.	.	RT E4	.
815	.	.	.	E-4
	.	.	.	V
	.	.	.	V
821	.	.	.	RT E4
823	.	.	CPE4.....	.
825	.	.	W-8	.
830	.	CPWETO.....	.	.
	.	V	.	.
	.	V	.	.
832	.	RS DT2	.	.
845	.	.	W-9	.
850	.	CW-9.....	.	.
	.	V	.	.
	.	V	.	.
853	.	POND4	.	.
861	WET-IN.....	.	.	.
864	.	D1	.	.
	.	V	.	.
	.	V	.	.
869	.	RT N1	.	.
	.	V	.	.
	.	V	.	.
871	.	RT N1	.	.
	.	V	.	.
	.	V	.	.
873	.	RT N1	.	.
875	.	.	WSC	.
	.	.	V	.
	.	.	V	.
880	.	.	RT N1	.

882	.	.	.	V	
	.	.	.	V	
	.	.	.	RT N1	
884	NE-1
	V
889	V
	.	.	.	RT N1	
891
	.	.	.	CPNE1
	.	.	.	V	
893	.	.	.	V	
	.	.	.	RT W3	
	.	.	.	V	
895	.	.	.	V	
	.	.	.	RT W3	
897	D2
	V
	V
902	.	.	.	RT N4	
	.	.	.	V	
904	.	.	.	RT N4	
	.	.	.	V	
906	.	.	.	RT N4	
908	NE2345
915	CPNE4
	.	.	.	V
	.	.	.	V	
918	.	.	.	RT W3	
920	CPWET3
	.	.	.	V
	.	.	.	V	
923	.	.	.	RT DN	
925	DMNTE
927	.	.	.	BV 14	
	.	.	.	V	
931	.	.	.	V	
	.	.	.	RT 14	
933	BV 13
937	D4
	V
943	V
	.	.	.	RT D4	
945	StmBV3
	.	.	.	V
	.	.	.	V	
948	.	.	.	RT 13	
950	.	.	.	BV 12	
954	StBV33
	.	.	.	V
	.	.	.	V	
957	.	.	.	RT 12	
959	.	.	.	BVW 7	
	.	.	.	V	
965	.	.	.	V	
	.	.	.	RT W7	
967	.	.	.	BV 8	
973	.	.	.	BV 7	
977	.	.	.	7+8
	.	.	.	V	
979	.	.	.	V	
	.	.	.	RT	
981	.	.	.	BV 6	
985	.	.	.	BV 9	
989	.	.	.	6+9
	.	.	.	V	
	.	.	.	V	

991	.	RT	.	.
993	.	.	BV 5	.
997	.	.	.	BV 10
1001	.	5+10
1003	.	RT	.	.
1005	.	.	BV 11	.
1009	.	EST-WS
1012	.	StmBV2
1016	.	RTto4	.	.
1018	.	.	BV 4	.
1022	.	Stm+ 4
1024	.	RTto3	.	.
1026	.	.	BV 3	.
1030	.	Stm+ 3
1032	.	RTto2	.	.
1034	.	.	BV 2	.
1038	.	Stm+ 2
1040	.	RTStBV	.	.
1042	.	.	BVW 8	.
1047	.	.	.	BV 1
1051	.	HCl+8
1053	.	StmBV1
1055	.	RT03	.	.
1057	.	.	D3	.
1062	.	.	RT03	.
1064	.	PT03
1066	.	.	A22	.
1071	.	.	.	A5
1075	.	CARAT1
1078	.	.	.	A4
1082	.	.	.	A23
1086	.	.	.	A1
1090	.	CHNL-A
1093	.	.	BVW-5	.
1098	.	ACHEV5
1100	.	RT5-3	.	.

1102	.	.	BW-3	.
1107	.	CP365	.	.
1109	.	.	BW-1	.
1114	.	WSTOUT	.	.
1116	.	V	.	.
1116	.	V	.	.
1116	.	RT03	.	.
1118	PT03	.	.	.
1120	.	W18RB	.	.
1128	.	.	V18-19	.
1132	.	.	.	V20
1136
1136	.	.	.	WET
1140	.	CB WET	.	.
1143	.	.	PH-IV	.
1151	.	.	.	E14
1156	.	C14	.	.
1156	.	V	.	.
1156	.	V	.	.
1159	.	E14-E1	.	.
1162	.	.	E1	.
1167	.	C1	.	.
1167	.	V	.	.
1167	.	V	.	.
1170	.	E1-E2	.	.
1173	.	.	E2	.
1178	.	C2	.	.
1178	.	V	.	.
1178	.	V	.	.
1181	.	E2-E3	.	.
1184	.	.	E3	.
1189	.	C3	.	.
1189	.	V	.	.
1189	.	V	.	.
1192	.	E3-E4	.	.
1195	.	.	E4	.
1200	.	C4	.	.
1203	.	.	D10	.
1214	.	.	.	D12
1219
1219	.	.	.	PARK
1224	.	C10PRK	.	.
1224	.	V	.	.
1224	.	V	.	.
1227	.	PK-CAR	.	.
1230	.	.	PhVa	.
1234	.	.	.	V4
1238	.	CB 1	.	.
1238	.	V	.	.
1238	.	V	.	.
1240	.	RT1-2	.	.
1243	.	.	PhVb	.

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1247      . . . . . CB2 .....
          . . . . . V
          . . . . . V
1249      . . . . . RT2-3
          . . . . .
1251      . . . . . V12
          . . . . .
1255      . . . . . V11
          . . . . .
1259      . . . . . V3
          . . . . .
1263      . . . . . CB3 .....
          . . . . . V
          . . . . . V
1265      . . . . . RT3-4
          . . . . .
1268      . . . . . PhVc
          . . . . .
1272      . . . . . V2
          . . . . .
1276      . . . . . CB4 .....
          . . . . . V
          . . . . . V
1278      . . . . . RT4-5
          . . . . .
1280      . . . . . PARKVI
          . . . . .
1284      . . . . . CB5 .....
          . . . . . V
          . . . . . V
1286      . . . . . RT5-6
          . . . . .
1288      . . . . . K6SCHL
          . . . . .
1292      . . . . . CB6 .....
          . . . . . V
          . . . . . V
1294      . . . . . RT6-7
          . . . . .
1297      . . . . . V1
          . . . . .
1301      . . . . . V29
          . . . . .
1305      . . . . . CB7 .....
          . . . . .
1308      . . . . . <----- CH 1
1307      . . . . . DR 1
          . . . . . V
          . . . . . V
1309      . . . . . RT 21
          . . . . .
          . . . . . W13R
          . . . . .
1311      . . . . .
          . . . . .
1316      . . . . . CP 21 .....
          . . . . .
          . . . . . -----> CH 1A
1320      . . . . . DV 1B
1318      . . . . . V
          . . . . . V
1323      . . . . . RT V12
          . . . . .
          . . . . . W12R
          . . . . .
1325      . . . . .
          . . . . .
1330      . . . . . CP V12 .....
          . . . . .
          . . . . . <----- CH 2
1333      . . . . . DR CH2
1332      . . . . . V
          . . . . . V
1334      . . . . . RT V12
          . . . . .
          . . . . .
1336      . . . . . CP V12 .....
          . . . . . V
          . . . . . V
1338      . . . . . RT F12
          . . . . .
          . . . . . W15R
          . . . . .
1340      . . . . .
          . . . . .
1345      . . . . . CP F12 .....
          . . . . .
          . . . . .

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1467      .      .      .      .      .      .      .      .      .      .
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1469      .      .      .      .      .      .      .      .      .      .
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1473      .      .      .      .      .      .      .      .      .      .
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1475      .      .      .      .      .      .      .      .      .      .
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1481      .      .      .      .      .      .      .      .      .      .
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1487      .      .      .      .      .      .      .      .      .      .
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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
* JUN 1998 *
*
* VERSION 4.1 *
*
* RUN DATE 04JAN08 TIME 13:39:39 *
*
*
*****

```

* U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

DRph5+Bv1 THE PROPOSED MODEL FOR DAMONTE PHASE 5 LOMR (CASE No. 07-09-1667P) IS ALSO THE MODEL USED FOR THE SUBSTANTIALLY COMPLETE HYDRAULIC MODEL FOR STEAMBOAT CREEK THROUGH BELLA VISTA PHASE 1. IT WAS RE-RUN ON JANUARY 4, 2008. ONLY THE ID INFORMATION WAS UPDATED FOR THIS RUN. JANUARY 2008 - Model Run date is 01/04/2008

CLOMR MODEL WAS USED WITHOUT CHANGE FOR THE LOMR MODEL FOR DAMONTE RANCH PHASE 5 (CASE No. 07-09-1667P). SUBMITTED MAY 5, 2007 AND NOT RERUN. IT DEFINED THE CHANNEL FLOWS FOR THE SUBSTANTIALLY COMPLETE STEAMBOAT CHANNEL HYDRAULIC MODEL THROUGH BELLA VISTA PHASE 1. LOMR AS-BUILT PLANS DID NOT CHANGE THE HYDROLOGIC PARAMETERS USED IN THE CLOM MARCH 2007 - Model Run date is 3/12/2007

UPDATED MODEL FOR DAMONTE RANCH PHASE V and BELLA VESTA PHASE 1 CLOMR USED FOR THE SUBSTANTIALLY COMPLETED MODEL THROUGH BELLA VISTA PHASE 1 MARCH 2007 - Model Run date is 3/12/2007

BELLA VESTA RANCH PHASE 1
 FILE NAME: DRph5+Bv1.dat - DECEMBER 2005 (UPDATED: JANUARY 2005)
 DAMONTE RANCH PHASE V - MARCH 2005

* * INCLUDES DEVELOPMENT OF VILLAGE 11-B * *

UPDATED MODEL FROM LOMR SUBMITTAL FILE NAME 0243AB.DAT (Orig. 128CLOMR.DAT) TO REFLECT GRADING PLANS AS OF 3/2005
 100-Year HEC-1 for AS BUILT conditions. Includes Steamboat Creek & tributaries (i.e. Galena, Jones, Browns, Bailey, 30, & 40 watersheds); Damonte Ranch with refined watersheds, detention structures, & refined east range watersheds; Whites Creek watersheds collected by Branch 3 & 4 with routing onto Damonte; the remainder of the Whites Creek & split flow from Thomas Creeks watersheds routed through Double Diamond; & Bella Vista Ranch with the remaining east range watersheds.

File Name: DRph5+bv1.dat
 Quad Knopf formerly Nimbus Engineers

REVISIONS REFLECT PHASE V DEVELOPMENT PER GRADING PLAN DATED 2/2005
 The model also includes the previous changes at the Diversion structure:
 a) box culverts replaced the RCPs; b) an overflow weir was added to control a major flood event

* * MODIFIED 5-2005 TO REFLECT GRADING PLAN CHANGES AFFECTING EASTERN * *
 * * BASINS NE-2, NE-3, NE-4, & NE-5. THESE HAVE ALL BEEN COMBINED AS * *
 * * THE REMOVAL OF MIRA LOMA RD. MAKES SEPARATION UNNECESSARY * *

```

54 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPILOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN       5  MINUTES IN COMPUTATION INTERVAL
          IDATE      27JUL 0  STARTING DATE

```

ITIME 0005 STARTING TIME
 NQ 288 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 28JUL 0 ENDING DATE
 NDTIME 0000 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 23.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS
 JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .94

*** **

 * *
 417 KK * STM+E *
 * *

421 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

420 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION STM+E
 FOR PLAN 1, RATIO = .94

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.92-HR
4193.	15.17	3636.	1624.	1624.	1624.
		(INCHES) .473	.843	.843	.843
		(AC-FT) 1803.	3210.	3210.	3210.
CUMULATIVE AREA =		71.41 SQ MI			

*** **

 * *
 540 KK * WTLNDS * DISCHARGE TO WETLANDS
 * *

541 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

542 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION WTLNDS
 FOR PLAN 1, RATIO = .94

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.92-HR
272.	12.17	107.	42.	42.	42.
		(INCHES) 2.144	3.351	3.351	3.351
		(AC-FT) 53.	83.	83.	83.
CUMULATIVE AREA =		.47 SQ MI			

*** **

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*****
*
915 KK * CPNE4 * COMBINE BSIN D2 AND POD NE-4
*
*****

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916 KO OUTPUT CONTROL VARIABLES
      IPRNT      3 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

```

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917 HC HYDROGRAPH COMBINATION
      ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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***
HYDROGRAPH AT STATION CPNE4
FOR PLAN 1, RATIO = .94
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)        6-HR      24-HR      72-HR      23.92-HR
+ 168.         12.08      (CFS)
      (INCHES) .616      25.        10.        10.        10.
      (AC-FT)  13.        13.        .968      .968      .968
      (AC-FT)  13.        13.        20.        20.        20.
CUMULATIVE AREA = .38 SQ MI

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*****
*
920 KK * CPWET3 * COMBINE CPWETO AND CPNE4
*
*****

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921 KO OUTPUT CONTROL VARIABLES
      IPRNT      3 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

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922 HC HYDROGRAPH COMBINATION
      ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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***
HYDROGRAPH AT STATION CPWET3
FOR PLAN 1, RATIO = .94
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)        6-HR      24-HR      72-HR      23.92-HR
+ 811.         13.42      (CFS)
      (INCHES) .409      240.       68.        68.        68.
      (AC-FT)  119.       119.       .460      .460      .460
      (AC-FT)  119.       119.       134.      134.      134.
CUMULATIVE AREA = 5.46 SQ MI

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*****
*
945 KK * StmBV3 *
*
*****

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947 KO OUTPUT CONTROL VARIABLES
      IPRNT      3 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

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946 HC HYDROGRAPH COMBINATION
      ICOMP      5 NUMBER OF HYDROGRAPHS TO COMBINE

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***
HYDROGRAPH AT STATION StmBV3
FOR PLAN 1, RATIO = .94
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)        6-HR      24-HR      72-HR      23.92-HR
+ 6407.        17.33      (CFS)
      (INCHES) .606      5560.      2249.      2249.      2249.
      (AC-FT)  2757.      2757.      .977      .977      .977
      (AC-FT)  2757.      2757.      4445.      4445.      4445.
CUMULATIVE AREA = 85.27 SQ MI

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*** **

 * StBV33 *

955 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

956 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION StBV33
 FOR PLAN 1, RATIO = .94

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.92-HR
6413.	17.42	5567.	2250.	2250.	2250.
		(INCHES) .607	.977	.977	.977
		(AC-FT) 2760.	4446.	4446.	4446.

CUMULATIVE AREA = 85.30 SQ MI

*** **

 * PT04 *

COMBINE FLOWS FROM WSD 1 & 5 WITH ROUTED FLOW FROM PT03

1488 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

1489 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION PT04
 FOR PLAN 1, RATIO = .94

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.92-HR
7106.	21.58	6406.	2234.	2234.	2234.
		(INCHES) .550	.765	.765	.765
		(AC-FT) 3176.	4415.	4415.	4415.

CUMULATIVE AREA = 108.24 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.94	
HYDROGRAPH AT					
+	W1R	1.36	1	FLOW	809.
				TIME	12.42
HYDROGRAPH AT					
+	W2R	.84	1	FLOW	507.
				TIME	12.42
2 COMBINED AT					
+	W1+W2	2.20	1	FLOW	1317.
				TIME	12.42
ROUTED TO					
+	RT-A	2.20	1	FLOW	1302.
				TIME	12.50
HYDROGRAPH AT					
+	W3R	1.38	1	FLOW	762.
				TIME	12.50

ROUTED TO					
+	RT-A	1.38	1	FLOW TIME	758. 12.58
HYDROGRAPH AT					
+	W4R	1.47	1	FLOW TIME	336. 12.75
3 COMBINED AT					
+	W1234	5.05	1	FLOW TIME	2361. 12.58
ROUTED TO					
+	RT-B	5.05	1	FLOW TIME	2348. 12.67
HYDROGRAPH AT					
+	W5R	1.27	1	FLOW TIME	249. 12.92
2 COMBINED AT					
+	W5+CH	6.32	1	FLOW TIME	2573. 12.67
ROUTED TO					
+	RT-C	6.32	1	FLOW TIME	2536. 12.83
HYDROGRAPH AT					
+	W6R	1.43	1	FLOW TIME	117. 13.50
2 COMBINED AT					
+	W6+CH	7.75	1	FLOW TIME	2617. 12.83
ROUTED TO					
+	RT-D	7.75	1	FLOW TIME	2603. 13.00
HYDROGRAPH AT					
+	W7R	.85	1	FLOW TIME	129. 13.00
2 COMBINED AT					
+	W7+CH	8.60	1	FLOW TIME	2731. 13.00
ROUTED TO					
+	RT-DIF	8.60	1	FLOW TIME	2719. 13.08
HYDROGRAPH AT					
+	W8R	.75	1	FLOW TIME	49. 13.42
2 COMBINED AT					
+	CP DIF	9.35	1	FLOW TIME	2764. 13.08
DIVERSION TO					
+	CH 123	9.35	1	FLOW TIME	2209. 13.08
HYDROGRAPH AT					
+	DV 4	9.35	1	FLOW TIME	555. 13.08
ROUTED TO					
+	RT W4	9.35	1	FLOW TIME	537. 13.25
HYDROGRAPH AT					
+	W17R	.58	1	FLOW TIME	87. 12.25
2 COMBINED AT					
+	CP W4	9.93	1	FLOW TIME	562. 13.25
ROUTED TO					
+	RT F4	9.93	1	FLOW TIME	546. 13.33
HYDROGRAPH AT					
+	W19R	.33	1	FLOW TIME	16. 12.25
HYDROGRAPH AT					
+	W9R	2.39	1	FLOW TIME	335. 12.50
ROUTED TO					
+	RT F4	2.39	1	FLOW TIME	326. 12.67
3 COMBINED AT					
+	CP F4	12.65	1	FLOW TIME	725. 13.33
ROUTED TO					
+	RT V4	12.65	1	FLOW TIME	710. 13.42
HYDROGRAPH AT					
+	W20R	.22	1	FLOW TIME	13. 12.25

2 COMBINED AT					
+ CP V4	12.87	1	FLOW TIME	715.	13.42
ROUTED TO					
+ RT STM	12.87	1	FLOW TIME	714.	13.50
HYDROGRAPH AT					
+ G1G2	8.00	1	FLOW TIME	2018.	14.00
ROUTED TO					
+ OUTJ1	8.00	1	FLOW TIME	2018.	14.08
HYDROGRAPH AT					
+ J1	6.40	1	FLOW TIME	313.	13.67
2 COMBINED AT					
+ OUTJ1	14.40	1	FLOW TIME	2307.	14.00
ROUTED TO					
+ OUTG3	14.40	1	FLOW TIME	2306.	14.17
HYDROGRAPH AT					
+ G3	3.90	1	FLOW TIME	285.	13.42
2 COMBINED AT					
+ OUTG3	18.30	1	FLOW TIME	2531.	14.08
ROUTED TO					
+ OUT30	18.30	1	FLOW TIME	2505.	14.67
HYDROGRAPH AT					
+ 15	4.20	1	FLOW TIME	410.	14.00
ROUTED TO					
+ OUT30	4.20	1	FLOW TIME	401.	15.33
HYDROGRAPH AT					
+ 30	16.70	1	FLOW TIME	2494.	13.92
3 COMBINED AT					
+ OUT30	39.20	1	FLOW TIME	5072.	14.50
ROUTED TO					
+ OUT40	39.20	1	FLOW TIME	5053.	14.75
HYDROGRAPH AT					
+ 35	15.30	1	FLOW TIME	2158.	14.33
HYDROGRAPH AT					
+ 40	2.50	1	FLOW TIME	416.	13.17
3 COMBINED AT					
+ OUT40	57.00	1	FLOW TIME	7318.	14.58
ROUTED TO					
+ OUT341	57.00	1	FLOW TIME	7314.	14.67
** PEAK STAGES IN FEET **					
1	STAGE	4560.87			
	TIME	14.67			
HYDROGRAPH AT					
+ C-1B	.07	1	FLOW TIME	60.	12.08
HYDROGRAPH AT					
+ C-1A	.06	1	FLOW TIME	4.	12.17
ROUTED TO					
+ RT C1	.06	1	FLOW TIME	4.	12.33
ROUTED TO					
+ RT C1	.06	1	FLOW TIME	4.	12.58
2 COMBINED AT					
+ CPC1B	.13	1	FLOW TIME	60.	12.08
2 COMBINED AT					
+ CB CUR	57.13	1	FLOW TIME	7326.	14.67
ROUTED TO					
+ OUTDS	57.13	1	FLOW	7319.	

				TIME	14.83
2 COMBINED AT					
+	CB DS	70.00	1	FLOW TIME	7546. 14.83
ROUTED TO					
+	RT WHT	70.00	1	FLOW TIME	7539. 14.92
HYDROGRAPH AT					
+	DR 123	.00	1	FLOW TIME	2209. 13.08
DIVERSION TO					
+	CH 1	.00	1	FLOW TIME	452. 13.08
HYDROGRAPH AT					
+	DV 263	.00	1	FLOW TIME	1757. 13.08
ROUTED TO					
+	RT 263	.00	1	FLOW TIME	1723. 13.33
HYDROGRAPH AT					
+	W10R	.30	1	FLOW TIME	3. 12.92
2 COMBINED AT					
+	CP 23	.30	1	FLOW TIME	1727. 13.33
DIVERSION TO					
+	CH 2	.30	1	FLOW TIME	863. 13.33
HYDROGRAPH AT					
+	DV 23A	.30	1	FLOW TIME	863. 13.33
ROUTED TO					
+	RT V3	.30	1	FLOW TIME	851. 13.50
HYDROGRAPH AT					
+	W11R	.32	1	FLOW TIME	108. 12.17
2 COMBINED AT					
+	CP V24	.62	1	FLOW TIME	867. 13.50
ROUTED TO					
+	RT F3	.62	1	FLOW TIME	847. 13.75
HYDROGRAPH AT					
+	W16R	.11	1	FLOW TIME	65. 12.08
2 COMBINED AT					
+	CP F3	.73	1	FLOW TIME	856. 13.75
ROUTED TO					
+	RT DSW	.73	1	FLOW TIME	853. 13.83
HYDROGRAPH AT					
+	W18RA	.21	1	FLOW TIME	92. 12.25
2 COMBINED AT					
+	CB DSW	.94	1	FLOW TIME	864. 13.83
HYDROGRAPH AT					
+	S-1	.04	1	FLOW TIME	14. 7.08
ROUTED TO					
+	RT S3	.04	1	FLOW TIME	13. 7.25
HYDROGRAPH AT					
+	S-2	.06	1	FLOW TIME	15. 7.08
ROUTED TO					
+	RT S3	.06	1	FLOW TIME	13. 7.17
HYDROGRAPH AT					
+	S-3A	.04	1	FLOW TIME	11. 7.08
ROUTED TO					
+	RT S3	.04	1	FLOW TIME	10. 7.25
3 COMBINED AT					
+	CPS3A	.14	1	FLOW TIME	35. 7.25
ROUTED TO					

+	RT S5	.14	1	FLOW TIME	34. 7.58
	HYDROGRAPH AT				
+	S-3B	.02	1	FLOW TIME	5. 7.08
	ROUTED TO				
+	RT S5	.02	1	FLOW TIME	5. 7.50
	HYDROGRAPH AT				
+	S-4	.02	1	FLOW TIME	6. 7.08
	ROUTED TO				
+	RT S5	.02	1	FLOW TIME	6. 7.25
	HYDROGRAPH AT				
+	S-5	.03	1	FLOW TIME	21. 6.25
	ROUTED TO				
+	RT S5	.03	1	FLOW TIME	18. 6.33
	4 COMBINED AT				
+	CPS5	.21	1	FLOW TIME	54. 7.58
	ROUTED TO				
+	RT WHT	.21	1	FLOW TIME	54. 7.75
	3 COMBINED AT				
+	CB WHT	71.15	1	FLOW TIME	7986. 14.83
	HYDROGRAPH AT				
+	HD	.11	1	FLOW TIME	113. 6.33
	2 COMBINED AT				
+	CP HD	71.27	1	FLOW TIME	7992. 14.83
	ROUTED TO				
+	DIVSTR	71.27	1	FLOW TIME	7993. 14.83
				** PEAK STAGES IN FEET **	
				1 STAGE	4488.00
				TIME	14.83
	DIVERSION TO				
+	BAS 1	71.27	1	FLOW TIME	3838. 14.83
	HYDROGRAPH AT				
+	STEAM	71.27	1	FLOW TIME	4154. 14.83
	ROUTED TO				
+	OUTDM	71.27	1	FLOW TIME	4153. 15.00
	ROUTED TO				
+	OUTDN	71.27	1	FLOW TIME	4150. 15.17
	HYDROGRAPH AT				
+	A7	.04	1	FLOW TIME	16. 12.42
	2 COMBINED AT				
+	STM+7	71.31	1	FLOW TIME	4158. 15.17
	HYDROGRAPH AT				
+	A6	.02	1	FLOW TIME	16. 12.17
	2 COMBINED AT				
+	STM+6	71.32	1	FLOW TIME	4166. 15.17
	HYDROGRAPH AT				
+	A3	.00	1	FLOW TIME	6. 12.08
	2 COMBINED AT				
+	STM+3	71.33	1	FLOW TIME	4170. 15.17
	HYDROGRAPH AT				
+	A2	.02	1	FLOW TIME	22. 12.08
	2 COMBINED AT				
+	STM+2	71.35	1	FLOW TIME	4177. 15.17
	HYDROGRAPH AT				
+	A17	.03	1	FLOW TIME	19. 12.08

HYDROGRAPH AT +	A18	.04	1	FLOW TIME	20. 12.17
2 COMBINED AT +	CHNL-E	.06	1	FLOW TIME	38. 12.17
2 COMBINED AT +	STM+E	71.41	1	FLOW TIME	4193. 15.17
ROUTED TO +	RT NST	71.41	1	FLOW TIME	4191. 15.58
HYDROGRAPH AT +	A16	.02	1	FLOW TIME	18. 12.08
HYDROGRAPH AT +	A19	.04	1	FLOW TIME	22. 12.17
HYDROGRAPH AT +	A20	.02	1	FLOW TIME	13. 12.25
3 COMBINED AT +	CHNL-F	.08	1	FLOW TIME	51. 12.17
2 COMBINED AT +	STM+AF	71.49	1	FLOW TIME	4213. 15.58
HYDROGRAPH AT +	BVW 6	.01	1	FLOW TIME	3. 12.08
ROUTED TO +	RT W6	.01	1	FLOW TIME	3. 12.75
HYDROGRAPH AT +	BV 16	.01	1	FLOW TIME	4. 12.08
2 COMBINED AT +	Stm+16	.02	1	FLOW TIME	6. 12.75
ROUTED TO +	RT 16	.02	1	FLOW TIME	6. 13.33
HYDROGRAPH AT +	BV 15	.02	1	FLOW TIME	11. 12.08
3 COMBINED AT +	Stm+15	71.53	1	FLOW TIME	4225. 15.58
ROUTED TO +	RT BV3	71.53	1	FLOW TIME	4225. 15.58
HYDROGRAPH AT +	APTS-9	.03	1	FLOW TIME	24. 12.17
HYDROGRAPH AT +	A8	.07	1	FLOW TIME	50. 12.17
2 COMBINED AT +	CHNL-B	.10	1	FLOW TIME	74. 12.17
HYDROGRAPH AT +	D12&13	.06	1	FLOW TIME	34. 12.17
HYDROGRAPH AT +	A9	.05	1	FLOW TIME	30. 12.17
2 COMBINED AT +	CHNL-C	.11	1	FLOW TIME	64. 12.17
2 COMBINED AT +	B&C	.21	1	FLOW TIME	138. 12.17
HYDROGRAPH AT +	A14	.05	1	FLOW TIME	32. 12.17
HYDROGRAPH AT +	A13	.05	1	FLOW TIME	26. 12.17
HYDROGRAPH AT +	A15	.02	1	FLOW TIME	13. 12.17

4 COMBINED AT					
+	CHNL-D	.33	1	FLOW TIME	209. 12.17
HYDROGRAPH AT					
+	A11	.01	1	FLOW TIME	12. 12.17
HYDROGRAPH AT					
+	A12	.02	1	FLOW TIME	12. 12.33
2 COMBINED AT					
+	11+12	.03	1	FLOW TIME	23. 12.17
2 COMBINED AT					
+	CHNL D	.36	1	FLOW TIME	232. 12.17
HYDROGRAPH AT					
+	X12+13	.08	1	FLOW TIME	27. 12.58
HYDROGRAPH AT					
+	A10	.01	1	FLOW TIME	12. 12.08
2 COMBINED AT					
+		.09	1	FLOW TIME	37. 12.58
HYDROGRAPH AT					
+	A21	.01	1	FLOW TIME	17. 12.08
3 COMBINED AT					
+	WTLNDS	.47	1	FLOW TIME	272. 12.17
HYDROGRAPH AT					
+	RC BAS	.00	1	FLOW TIME	3838. 14.83
ROUTED TO					
+	BAS 1	.00	1	FLOW TIME	3412. 15.33
				** PEAK STAGES IN FEET **	
			1	STAGE	4481.69
				TIME	15.33
DIVERSION TO					
+	36DIVQ	.00	1	FLOW TIME	61. 15.33
HYDROGRAPH AT					
+	BAS1DS	.00	1	FLOW TIME	3351. 15.33
ROUTED TO					
+	POND2	.00	1	FLOW TIME	3319. 15.58
HYDROGRAPH AT					
+	T-1	.04	1	FLOW TIME	34. 12.08
ROUTED TO					
+	RT T2	.04	1	FLOW TIME	33. 12.08
HYDROGRAPH AT					
+	T-2	.06	1	FLOW TIME	61. 12.08
2 COMBINED AT					
+	CPT2	.10	1	FLOW TIME	95. 12.08
ROUTED TO					
+	RT T3	.10	1	FLOW TIME	89. 12.17
HYDROGRAPH AT					
+	T-3	.06	1	FLOW TIME	63. 12.08
2 COMBINED AT					
+	CPT3	.16	1	FLOW TIME	152. 12.08
2 COMBINED AT					
+	CPD1A	.16	1	FLOW TIME	3341. 15.58
ROUTED TO					
+	RT WT	.16	1	FLOW TIME	3316. 15.83
HYDROGRAPH AT					
+	WSF1	.77	1	FLOW TIME	335. 12.17
HYDROGRAPH AT					
+	WSE1	2.10	1	FLOW	568.

				TIME	12.42
2 COMBINED AT					
+	F1E1	2.88	1	FLOW	766.
				TIME	12.25
HYDROGRAPH AT					
+	C-2	.03	1	FLOW	10.
				TIME	12.08
ROUTED TO					
+	RT C3	.03	1	FLOW	10.
				TIME	12.25
HYDROGRAPH AT					
+	C-1C	.07	1	FLOW	46.
				TIME	12.08
ROUTED TO					
+	RT C3	.07	1	FLOW	45.
				TIME	12.17
HYDROGRAPH AT					
+	C-3	.03	1	FLOW	10.
				TIME	12.08
4 COMBINED AT					
+	CPC3	3.01	1	FLOW	828.
				TIME	12.25
ROUTED TO					
+	RT C4	3.01	1	FLOW	619.
				TIME	12.25
HYDROGRAPH AT					
+	C-4	.04	1	FLOW	34.
				TIME	12.08
2 COMBINED AT					
+	CPC4	3.05	1	FLOW	837.
				TIME	12.25
ROUTED TO					
+	RT C7	3.05	1	FLOW	825.
				TIME	12.33
ROUTED TO					
+	RT C7	3.05	1	FLOW	811.
				TIME	12.42
HYDROGRAPH AT					
+	C-5	.07	1	FLOW	59.
				TIME	12.08
ROUTED TO					
+	RT C7	.07	1	FLOW	58.
				TIME	12.08
ROUTED TO					
+	RT C7	.07	1	FLOW	57.
				TIME	12.25
HYDROGRAPH AT					
+	C-7	.03	1	FLOW	28.
				TIME	12.08
HYDROGRAPH AT					
+	C-6	.13	1	FLOW	34.
				TIME	12.08
ROUTED TO					
+	RT C7	.13	1	FLOW	34.
				TIME	12.25
ROUTED TO					
+	RT C7	.13	1	FLOW	34.
				TIME	12.25
ROUTED TO					
+	RT C7	.13	1	FLOW	34.
				TIME	12.42
4 COMBINED AT					
+	CPC7	3.27	1	FLOW	892.
				TIME	12.33
ROUTED TO					
+	RT WT	3.27	1	FLOW	829.
				TIME	12.58
HYDROGRAPH AT					
+	W-1	.06	1	FLOW	62.
				TIME	12.08
ROUTED TO					
+	RT W1	.06	1	FLOW	56.
				TIME	12.17
3 COMBINED AT					
+	CPNET	3.50	1	FLOW	3393.
				TIME	15.83
ROUTED TO					
+	RT W1	3.50	1	FLOW	3366.
				TIME	16.08
HYDROGRAPH AT					

+	E2A	2.10	1	FLOW TIME	568. 12.42
	HYDROGRAPH AT				
+	SE-2	.06	1	FLOW TIME	14. 12.08
	ROUTED TO				
+	RT S3	.06	1	FLOW TIME	14. 12.17
	HYDROGRAPH AT				
+	SE-3	.05	1	FLOW TIME	16. 12.08
	HYDROGRAPH AT				
+	SE-1	.11	1	FLOW TIME	32. 12.08
	ROUTED TO				
+	RT S3	.11	1	FLOW TIME	32. 12.17
	3 COMBINED AT				
+	CPSE3	.22	1	FLOW TIME	59. 12.17
	ROUTED TO				
+	RT S5	.22	1	FLOW TIME	60. 12.25
	HYDROGRAPH AT				
+	SE-4	.02	1	FLOW TIME	5. 12.08
	HYDROGRAPH AT				
+	SE-5	.02	1	FLOW TIME	1. 12.00
	3 COMBINED AT				
+	CPSE5	.26	1	FLOW TIME	66. 12.25
	ROUTED TO				
+	RT S7	.26	1	FLOW TIME	67. 12.33
	HYDROGRAPH AT				
+	SE-6	.00	1	FLOW TIME	1. 12.08
	ROUTED TO				
+	RT S7	.00	1	FLOW TIME	1. 12.42
	HYDROGRAPH AT				
+	SE-7	.10	1	FLOW TIME	104. 12.00
	3 COMBINED AT				
+	CPSE7	.36	1	FLOW TIME	123. 12.08
	ROUTED TO				
+	RT WI	.36	1	FLOW TIME	121. 12.08
	ROUTED TO				
+	RT WI	.36	1	FLOW TIME	123. 12.25
	HYDROGRAPH AT				
+	SE-8	.06	1	FLOW TIME	59. 12.08
	ROUTED TO				
+	RTWI	.06	1	FLOW TIME	58. 12.08
	ROUTED TO				
+	RT WI	.06	1	FLOW TIME	57. 12.25
	HYDROGRAPH AT				
+	W-2	.03	1	FLOW TIME	9. 12.08
	HYDROGRAPH AT				
+	W-3	.04	1	FLOW TIME	40. 12.08
	2 COMBINED AT				
+	CPW2	.07	1	FLOW TIME	49. 12.08
	ROUTED TO				
+	RTG WI	.07	1	FLOW TIME	45. 12.08
	3 COMBINED AT				
+	PWETIN	.49	1	FLOW TIME	215. 12.25
	2 COMBINED AT				
+	CPWETA	2.59	1	FLOW TIME	746. 12.33

ROUTED TO						
+	RT W1	2.59	1	FLOW	712.	
				TIME	12.50	
2 COMBINED AT						
+	CPWET1	6.09	1	FLOW	3430.	
				TIME	16.08	
ROUTED TO						
+	RTWET1	6.09	1	FLOW	3399.	
				TIME	16.33	
HYDROGRAPH AT						
+	WET	.12	1	FLOW	42.	
				TIME	12.25	
2 COMBINED AT						
+	CPWETB	6.21	1	FLOW	3406.	
				TIME	16.33	
ROUTED TO						
+	RTWETB	6.21	1	FLOW	3375.	
				TIME	16.50	
HYDROGRAPH AT						
+	E-2	.07	1	FLOW	45.	
				TIME	12.08	
ROUTED TO						
+	RT E3	.07	1	FLOW	42.	
				TIME	12.17	
HYDROGRAPH AT						
+	E-1	.05	1	FLOW	2.	
				TIME	12.17	
ROUTED TO						
+	RT E3	.05	1	FLOW	2.	
				TIME	12.25	
ROUTED TO						
+	RTE3	.05	1	FLOW	2.	
				TIME	12.42	
2 COMBINED AT						
+	CPE3	.12	1	FLOW	42.	
				TIME	12.17	
HYDROGRAPH AT						
+	WSB2	.12	1	FLOW	68.	
				TIME	12.00	
HYDROGRAPH AT						
+	WSB1	.36	1	FLOW	174.	
				TIME	12.08	
2 COMBINED AT						
+	CPB12	.48	1	FLOW	213.	
				TIME	12.08	
ROUTED TO						
+	RT E3	.48	1	FLOW	211.	
				TIME	12.08	
ROUTED TO						
+	RT E3	.48	1	FLOW	197.	
				TIME	12.17	
ROUTED TO						
+	RT E4	.48	1	FLOW	188.	
				TIME	12.17	
HYDROGRAPH AT						
+	E-4	.10	1	FLOW	71.	
				TIME	12.08	
ROUTED TO						
+	RT E4	.10	1	FLOW	66.	
				TIME	12.08	
3 COMBINED AT						
+	CPE4	.70	1	FLOW	294.	
				TIME	12.17	
HYDROGRAPH AT						
+	W-8	.06	1	FLOW	63.	
				TIME	12.08	
3 COMBINED AT						
+	CPWETO	6.97	1	FLOW	3410.	
				TIME	16.50	
ROUTED TO						
+	RS DT2	6.97	1	FLOW	2805.	
				TIME	17.33	
				** PEAK STAGES IN FEET **		
				1	STAGE	4461.21
					TIME	17.33
HYDROGRAPH AT						
+	W-9	.04	1	FLOW	42.	
				TIME	12.08	
2 COMBINED AT						
+	CW-9	7.01	1	FLOW	2812.	
				TIME	17.33	

ROUTED TO					
+	POND4	7.01	1	FLOW TIME	2652. 17.83
				** PEAK STAGES IN FEET **	
			1	STAGE TIME	4456.36 17.83
2 COMBINED AT					
+	WET-IN	7.48	1	FLOW TIME	2724. 17.83
HYDROGRAPH AT					
+	D1	1.72	1	FLOW TIME	530. 12.33
ROUTED TO					
+	RT N1	1.72	1	FLOW TIME	524. 12.33
ROUTED TO					
+	RT N1	1.72	1	FLOW TIME	520. 12.42
ROUTED TO					
+	RT N1	1.72	1	FLOW TIME	512. 12.42
HYDROGRAPH AT					
+	WSC	3.31	1	FLOW TIME	820. 12.50
ROUTED TO					
+	RT N1	3.31	1	FLOW TIME	810. 12.58
ROUTED TO					
+	RT N1	3.31	1	FLOW TIME	809. 12.58
HYDROGRAPH AT					
+	NE-1	.04	1	FLOW TIME	18. 12.08
ROUTED TO					
+	RT N1	.04	1	FLOW TIME	18. 12.17
3 COMBINED AT					
+	CPNE1	5.07	1	FLOW TIME	1298. 12.50
ROUTED TO					
+	RT W3	5.07	1	FLOW TIME	1280. 12.50
ROUTED TO					
+	RT W3	5.07	1	FLOW TIME	756. 13.50
HYDROGRAPH AT					
+	D2	.15	1	FLOW TIME	102. 12.00
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	88. 12.00
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	85. 12.08
ROUTED TO					
+	RT N4	.15	1	FLOW TIME	80. 12.17
HYDROGRAPH AT					
+	NE2345	.23	1	FLOW TIME	97. 12.08
2 COMBINED AT					
+	CPNE4	.38	1	FLOW TIME	168. 12.08
ROUTED TO					
+	RT W3	.38	1	FLOW TIME	88. 13.08
2 COMBINED AT					
+	CPWET3	5.46	1	FLOW TIME	811. 13.42
ROUTED TO					
+	RT DN	5.46	1	FLOW TIME	778. 13.92
2 COMBINED AT					
+	DMNTE	12.94	1	FLOW TIME	2762. 17.83
HYDROGRAPH AT					
+	BV 14	.01	1	FLOW TIME	5. 12.08
ROUTED TO					
+	RT 14	.01	1	FLOW	6.

				TIME	12.58
HYDROGRAPH AT					
+	BV 13	.00	1	FLOW	4.
				TIME	12.08
HYDROGRAPH AT					
+	D4	.80	1	FLOW	70.
				TIME	12.67
ROUTED TO					
+	RT D4	.80	1	FLOW	57.
				TIME	13.25
5 COMBINED AT					
+	StmBV3	85.27	1	FLOW	6407.
				TIME	17.33
ROUTED TO					
+	RT 13	85.27	1	FLOW	6407.
				TIME	17.42
HYDROGRAPH AT					
+	BV 12	.03	1	FLOW	22.
				TIME	12.08
2 COMBINED AT					
+	StBV33	85.30	1	FLOW	6413.
				TIME	17.42
ROUTED TO					
+	RT 12	85.30	1	FLOW	6411.
				TIME	17.58
HYDROGRAPH AT					
+	BVW 7	.06	1	FLOW	28.
				TIME	12.17
ROUTED TO					
+	RT W7	.06	1	FLOW	26.
				TIME	12.17
HYDROGRAPH AT					
+	BV 8	.02	1	FLOW	14.
				TIME	12.08
HYDROGRAPH AT					
+	BV 7	.02	1	FLOW	14.
				TIME	12.08
3 COMBINED AT					
+	7+8	.10	1	FLOW	50.
				TIME	12.08
ROUTED TO					
+	RT	.10	1	FLOW	48.
				TIME	12.17
HYDROGRAPH AT					
+	BV 6	.01	1	FLOW	8.
				TIME	12.08
HYDROGRAPH AT					
+	BV 9	.02	1	FLOW	11.
				TIME	12.08
3 COMBINED AT					
+	6+9	.13	1	FLOW	66.
				TIME	12.17
ROUTED TO					
+	RT	.13	1	FLOW	66.
				TIME	12.17
HYDROGRAPH AT					
+	BV 5	.00	1	FLOW	3.
				TIME	12.08
HYDROGRAPH AT					
+	BV 10	.01	1	FLOW	9.
				TIME	12.08
3 COMBINED AT					
+	5+10	.15	1	FLOW	77.
				TIME	12.17
ROUTED TO					
+	RT	.15	1	FLOW	76.
				TIME	12.17
HYDROGRAPH AT					
+	BV 11	.01	1	FLOW	8.
				TIME	12.08
2 COMBINED AT					
+	EST-WS	.16	1	FLOW	84.
				TIME	12.17
2 COMBINED AT					
+	StmBV2	85.46	1	FLOW	6452.
				TIME	17.58
ROUTED TO					
+	RTto4	85.46	1	FLOW	6451.
				TIME	17.58
HYDROGRAPH AT					

+	BV 4	.01	1	FLOW TIME	11. 12.08
+	2 COMBINED AT				
+	Stm+ 4	85.48	1	FLOW TIME	6457. 17.58
+	ROUTED TO				
+	RTto3	85.48	1	FLOW TIME	6457. 17.58
+	HYDROGRAPH AT				
+	BV 3	.01	1	FLOW TIME	11. 12.08
+	2 COMBINED AT				
+	Stm+ 3	85.49	1	FLOW TIME	6463. 17.58
+	ROUTED TO				
+	RTto2	85.49	1	FLOW TIME	6463. 17.58
+	HYDROGRAPH AT				
+	BV 2	.01	1	FLOW TIME	4. 12.08
+	2 COMBINED AT				
+	Stm+ 2	85.50	1	FLOW TIME	6466. 17.58
+	ROUTED TO				
+	RTStBV	85.50	1	FLOW TIME	6465. 17.58
+	HYDROGRAPH AT				
+	BVW 8	.04	1	FLOW TIME	27. 12.08
+	HYDROGRAPH AT				
+	BV 1	.03	1	FLOW TIME	29. 12.08
+	2 COMBINED AT				
+	HCL+8	.07	1	FLOW TIME	57. 12.08
+	2 COMBINED AT				
+	StmBV1	85.57	1	FLOW TIME	6477. 17.58
+	ROUTED TO				
+	RT03	85.57	1	FLOW TIME	6414. 20.00
+	HYDROGRAPH AT				
+	D3	.70	1	FLOW TIME	114. 12.67
+	ROUTED TO				
+	RT03	.70	1	FLOW TIME	79. 14.08
+	2 COMBINED AT				
+	PT03	86.27	1	FLOW TIME	6421. 20.00
+	HYDROGRAPH AT				
+	A22	.00	1	FLOW TIME	2. 12.33
+	HYDROGRAPH AT				
+	A5	.05	1	FLOW TIME	26. 12.17
+	2 COMBINED AT				
+	CARAT1	.05	1	FLOW TIME	28. 12.17
+	HYDROGRAPH AT				
+	A4	.02	1	FLOW TIME	18. 12.08
+	HYDROGRAPH AT				
+	A23	.00	1	FLOW TIME	2. 12.33
+	HYDROGRAPH AT				
+	A1	.01	1	FLOW TIME	12. 12.17
+	4 COMBINED AT				
+	CHNL-A	.09	1	FLOW TIME	57. 12.17
+	HYDROGRAPH AT				
+	BVN-5	.05	1	FLOW TIME	44. 12.08
+	2 COMBINED AT				
+	ACHBV5	.14	1	FLOW TIME	98. 12.08
+	ROUTED TO				
+	RT5-3	.14	1	FLOW TIME	98. 12.33

6477.
17.58

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HYDROGRAPH AT +	BVW-3	.05	1	FLOW TIME	14. 12.08
2 COMBINED AT +	CP3&5	.19	1	FLOW TIME	108. 12.33
HYDROGRAPH AT +	BVW-1	.03	1	FLOW TIME	9. 12.08
2 COMBINED AT +	WSTOUT	.21	1	FLOW TIME	117. 12.33
ROUTED TO +	RT03	.21	1	FLOW TIME	70. 14.92
2 COMBINED AT +	PT03	86.48	1	FLOW TIME	5460. 20.00
HYDROGRAPH AT +	W18RB	.13	1	FLOW TIME	141. 12.08
HYDROGRAPH AT +	V18-19	.05	1	FLOW TIME	51. 12.08
HYDROGRAPH AT +	V20	.05	1	FLOW TIME	46. 12.08
HYDROGRAPH AT +	WET	.02	1	FLOW TIME	7. 12.17
4 COMBINED AT +	CB WET	.25	1	FLOW TIME	244. 12.08
HYDROGRAPH AT +	PH-IV	.19	1	FLOW TIME	158. 12.17
HYDROGRAPH AT +	E14	.03	1	FLOW TIME	24. 12.08
3 COMBINED AT +	C14	.47	1	FLOW TIME	412. 12.17
ROUTED TO +	E14-E1	.47	1	FLOW TIME	411. 12.17
HYDROGRAPH AT +	E1	.01	1	FLOW TIME	7. 12.00
2 COMBINED AT +	C1	.47	1	FLOW TIME	418. 12.17
ROUTED TO +	E1-E2	.47	1	FLOW TIME	413. 12.17
HYDROGRAPH AT +	E2	.00	1	FLOW TIME	4. 12.00
2 COMBINED AT +	C2	.47	1	FLOW TIME	417. 12.17
ROUTED TO +	E2-E3	.47	1	FLOW TIME	409. 12.17
HYDROGRAPH AT +	E3	.00	1	FLOW TIME	3. 12.00
2 COMBINED AT +	C3	.48	1	FLOW TIME	412. 12.17
ROUTED TO +	E3-E4	.48	1	FLOW TIME	402. 12.17
HYDROGRAPH AT +	E4	.00	1	FLOW TIME	4. 12.00
2 COMBINED AT +	C4	.48	1	FLOW TIME	406. 12.17
HYDROGRAPH AT +	D10	.12	1	FLOW TIME	106. 12.17

HYDROGRAPH AT +	D12	.02	1	FLOW TIME	18. 12.08
HYDROGRAPH AT +	PARK	.01	1	FLOW TIME	5. 12.08
4 COMBINED AT +	C10PRK	.63	1	FLOW TIME	530. 12.17
ROUTED TO +	PK-CAR	.63	1	FLOW TIME	515. 12.25
HYDROGRAPH AT +	PhVa	.01	1	FLOW TIME	12. 12.08
HYDROGRAPH AT +	V4	.03	1	FLOW TIME	21. 12.08
3 COMBINED AT +	CB 1	.66	1	FLOW TIME	535. 12.25
ROUTED TO +	RT1-2	.66	1	FLOW TIME	530. 12.25
HYDROGRAPH AT +	PhVb	.03	1	FLOW TIME	27. 12.08
2 COMBINED AT +	CB2	.69	1	FLOW TIME	549. 12.25
ROUTED TO +	RT2-3	.69	1	FLOW TIME	537. 12.33
HYDROGRAPH AT +	V12	.01	1	FLOW TIME	12. 12.08
HYDROGRAPH AT +	V11	.01	1	FLOW TIME	7. 12.00
HYDROGRAPH AT +	V3	.03	1	FLOW TIME	20. 12.08
4 COMBINED AT +	CB3	.74	1	FLOW TIME	563. 12.33
ROUTED TO +	RT3-4	.74	1	FLOW TIME	555. 12.33
HYDROGRAPH AT +	PhVc	.02	1	FLOW TIME	23. 12.08
HYDROGRAPH AT +	V2	.04	1	FLOW TIME	30. 12.08
3 COMBINED AT +	CB4	.80	1	FLOW TIME	575. 12.33
ROUTED TO +	RT4-5	.80	1	FLOW TIME	569. 12.33
HYDROGRAPH AT +	PARKVI	.00	1	FLOW TIME	2. 12.08
2 COMBINED AT +	CB5	.81	1	FLOW TIME	571. 12.33
ROUTED TO +	RT5-6	.81	1	FLOW TIME	558. 12.42
HYDROGRAPH AT +	K6SCHL	.01	1	FLOW TIME	10. 12.08
2 COMBINED AT +	CB6	.82	1	FLOW TIME	568. 12.42
ROUTED TO +	RT6-7	.82	1	FLOW TIME	558. 12.50
HYDROGRAPH AT +	V1	.04	1	FLOW	27.

				TIME	12.08
HYDROGRAPH AT					
+	V29	.06	1	FLOW TIME	67. 12.08
3 COMBINED AT					
+	CB7	.92	1	FLOW TIME	578. 12.50
HYDROGRAPH AT					
+	DR 1	.00	1	FLOW TIME	452. 13.08
ROUTED TO					
+	RT Z1	.00	1	FLOW TIME	439. 13.42
HYDROGRAPH AT					
+	W13R	1.30	1	FLOW TIME	35. 12.42
2 COMBINED AT					
+	CP Z1	1.30	1	FLOW TIME	449. 13.42
DIVERSION TO					
+	CH 1A	1.30	1	FLOW TIME	200. 13.00
HYDROGRAPH AT					
+	DV 1B	1.30	1	FLOW TIME	249. 13.42
ROUTED TO					
+	RT V12	1.30	1	FLOW TIME	242. 13.58
HYDROGRAPH AT					
+	W12R	.60	1	FLOW TIME	18. 12.42
2 COMBINED AT					
+	CP V12	1.90	1	FLOW TIME	251. 13.58
HYDROGRAPH AT					
+	DR CH2	.00	1	FLOW TIME	863. 13.33
ROUTED TO					
+	RT V12	.00	1	FLOW TIME	844. 13.58
2 COMBINED AT					
+	CP V12	1.90	1	FLOW TIME	1095. 13.58
ROUTED TO					
+	RT F12	1.90	1	FLOW TIME	1061. 13.75
HYDROGRAPH AT					
+	W15R	.21	1	FLOW TIME	106. 12.08
2 COMBINED AT					
+	CP F12	2.11	1	FLOW TIME	1070. 13.75
HYDROGRAPH AT					
+	DR 1A	.00	1	FLOW TIME	200. 13.00
ROUTED TO					
+	RT F1A	.00	1	FLOW TIME	200. 14.00
HYDROGRAPH AT					
+	W14R	.18	1	FLOW TIME	69. 12.17
2 COMBINED AT					
+	CP F1A	.18	1	FLOW TIME	209. 13.75
2 COMBINED AT					
+	CB 1&2	2.29	1	FLOW TIME	1279. 13.75
ROUTED TO					
+	RT WT2	2.29	1	FLOW TIME	1271. 13.92
ROUTED TO					
+	RT WT2	2.29	1	FLOW TIME	1219. 14.42
ROUTED TO					
+	RT WT2	2.29	1	FLOW TIME	1215. 14.50
HYDROGRAPH AT					
+	WT 6P1	.07	1	FLOW TIME	32. 12.25
HYDROGRAPH AT					

+	W WT2P	.59	1	FLOW TIME	122. 12.58
+	3 COMBINED AT CB WT2	2.95	1	FLOW TIME	1233. 14.50
+	HYDROGRAPH AT WS WT1	1.93	1	FLOW TIME	73. 12.83
+	ROUTED TO RT WT3	1.93	1	FLOW TIME	72. 13.17
+	HYDROGRAPH AT THOMAS	11.54	1	FLOW TIME	2544. 13.25
+	DIVERSION TO HOLCOM	11.54	1	FLOW TIME	1380. 13.25
+	HYDROGRAPH AT DV HOL	11.54	1	FLOW TIME	1164. 13.25
+	ROUTED TO RT WT3	11.54	1	FLOW TIME	1151. 13.50
+	DIVERSION TO THOM	11.54	1	FLOW TIME	52. 13.50
+	HYDROGRAPH AT DV THO	11.54	1	FLOW TIME	1099. 13.50
+	ROUTED TO RT WT3	11.54	1	FLOW TIME	1097. 13.58
+	HYDROGRAPH AT WT3P	.49	1	FLOW TIME	185. 12.25
+	3 COMBINED AT CB WT3	13.96	1	FLOW TIME	1163. 13.58
+	2 COMBINED AT CB OFF	16.91	1	FLOW TIME	2055. 14.42
+	ROUTED TO RT WHC	16.91	1	FLOW TIME	2050. 14.50
+	HYDROGRAPH AT D2	.36	1	FLOW TIME	31. 12.42
+	2 COMBINED AT CB WHC	17.27	1	FLOW TIME	2058. 14.50
+	ROUTED TO RT DET	17.27	1	FLOW TIME	2055. 14.58
+	ROUTED TO RT DET	17.27	1	FLOW TIME	1743. 15.08
				** PEAK STAGES IN FEET **	
			1	STAGE TIME	4427.22 15.08
+	ROUTED TO RT WT	17.27	1	FLOW TIME	1741. 15.17
+	HYDROGRAPH AT THOMAS	.00	1	FLOW TIME	52. 13.50
+	ROUTED TO RT WT	.00	1	FLOW TIME	32. 15.08
+	HYDROGRAPH AT WT4P	1.73	1	FLOW TIME	220. 13.42
+	2 COMBINED AT	1.73	1	FLOW TIME	220. 13.42
+	HYDROGRAPH AT WT7P	.16	1	FLOW TIME	19. 13.33
+	ROUTED TO RT WT	.16	1	FLOW TIME	18. 14.00

HYDROGRAPH AT
 + WS WT5 .49 1 FLOW 266.
 TIME 12.17
 ROUTED TO
 + RT WT .49 1 FLOW 202.
 TIME 12.58
 3 COMBINED AT
 + CB WT 2.38 1 FLOW 327.
 TIME 12.67
 2 COMBINED AT
 + CP WT 19.65 1 FLOW 1852.
 TIME 15.08
 3 COMBINED AT
 + PT03 107.05 1 FLOW 7183.
 TIME 19.83
 ROUTED TO
 + RT04 107.05 1 FLOW 7096.
 TIME 21.58
 HYDROGRAPH AT
 + D1 .44 1 FLOW 74.
 TIME 12.50
 HYDROGRAPH AT
 + D5 .75 1 FLOW 19.
 TIME 14.58
 3 COMBINED AT
 + PT04 108.24 1 FLOW 7106.
 TIME 21.58
 1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME	
						PEAK	TIME TO PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1	RATIO=	.94							
RT STM	MANE	1.51	714.59	808.24	.23	5.00	713.88	810.00	.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1609E+03 EXCESS= .0000E+00 OUTFLOW= .1602E+03 BASIN STORAGE= .8542E+00 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
OUTJ1	MANE	5.00	2017.57	845.00	1.64	5.00	2017.57	845.00	1.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7027E+03 EXCESS= .0000E+00 OUTFLOW= .6995E+03 BASIN STORAGE= .4234E+01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
OUTG3	MANE	5.00	2305.58	850.00	1.06	5.00	2305.58	850.00	1.06
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8204E+03 EXCESS= .0000E+00 OUTFLOW= .8146E+03 BASIN STORAGE= .7346E+01 PERCENT ERROR= -.2									
FOR PLAN = 1	RATIO=	.00							
RT C1	MANE	1.25	4.32	736.25	.77	5.00	4.25	740.00	.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2549E+01 EXCESS= .0000E+00 OUTFLOW= .2532E+01 BASIN STORAGE= .1746E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RT C1	MANE	1.75	4.35	747.25	.75	5.00	4.22	755.00	.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2533E+01 EXCESS= .0000E+00 OUTFLOW= .2492E+01 BASIN STORAGE= .4446E-01 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO=	.00							
RT DSW	MANE	5.00	853.15	830.00	4.91	5.00	853.15	830.00	4.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1933E+03 EXCESS= .0000E+00 OUTFLOW= .1915E+03 BASIN STORAGE= .2393E+01 PERCENT ERROR= -.3									
FOR PLAN = 1	RATIO=	.00							
RT S3	MANE	1.50	10.23	433.50	3.62	5.00	10.19	435.00	3.62
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7578E+01 EXCESS= .0000E+00 OUTFLOW= .7537E+01 BASIN STORAGE= .4286E-01 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RT W6	MANE	1.75	3.22	764.75	2.98	5.00	3.14	765.00	2.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1675E+01 EXCESS= .0000E+00 OUTFLOW= .1592E+01 BASIN STORAGE= .1015E+00 PERCENT ERROR= -1.1									
FOR PLAN = 1	RATIO=	.00							
RT 16	MANE	5.00	6.47	800.00	4.21	5.00	6.47	800.00	4.21
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3743E+01 EXCESS= .0000E+00 OUTFLOW= .3601E+01 BASIN STORAGE= .1704E+00 PERCENT ERROR= -.8									

RT S5	MANE	5.00	59.58	735.00	1.75	5.00	59.58	735.00	1.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2057E+02 EXCESS= .0000E+00 OUTFLOW= .2044E+02 BASIN STORAGE= .1706E+00 PERCENT ERROR= -.2									
FOR PLAN = 1		RATIO= .00							
RT S7	MANE	5.00	66.58	740.00	1.79	5.00	66.58	740.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2471E+02 EXCESS= .0000E+00 OUTFLOW= .2454E+02 BASIN STORAGE= .2175E+00 PERCENT ERROR= -.2									
FOR PLAN = 1		RATIO= .00							
RT S7	MANE	1.00	.55	736.00	1.39	5.00	.50	745.00	1.39
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2995E+00 EXCESS= .0000E+00 OUTFLOW= .2958E+00 BASIN STORAGE= .4227E-02 PERCENT ERROR= -.2									
FOR PLAN = 1		RATIO= .00							
RT WI	MANE	3.02	121.38	725.34	1.88	5.00	120.52	725.00	1.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3627E+02 EXCESS= .0000E+00 OUTFLOW= .3613E+02 BASIN STORAGE= .1719E+00 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT WI	MANE	5.00	122.68	735.00	1.86	5.00	122.68	735.00	1.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3621E+02 EXCESS= .0000E+00 OUTFLOW= .3576E+02 BASIN STORAGE= .5598E+00 PERCENT ERROR= -.3									
FOR PLAN = 1		RATIO= .00							
RTWI	MANE	.76	58.84	725.86	2.71	5.00	58.13	725.00	2.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9414E+01 EXCESS= .0000E+00 OUTFLOW= .9405E+01 BASIN STORAGE= .1230E-01 PERCENT ERROR= .0									
FOR PLAN = 1		RATIO= .00							
RT WI	MANE	5.00	57.05	735.00	2.67	5.00	57.05	735.00	2.67
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9419E+01 EXCESS= .0000E+00 OUTFLOW= .9284E+01 BASIN STORAGE= .2083E+00 PERCENT ERROR= -.8									
FOR PLAN = 1		RATIO= .00							
RT E3	MANE	3.98	43.14	727.90	2.20	5.00	42.00	730.00	2.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8242E+01 EXCESS= .0000E+00 OUTFLOW= .8205E+01 BASIN STORAGE= .4259E-01 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT E3	MANE	1.00	2.26	735.00	.50	5.00	2.26	735.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1343E+01 EXCESS= .0000E+00 OUTFLOW= .1335E+01 BASIN STORAGE= .8296E-02 PERCENT ERROR= .0									
FOR PLAN = 1		RATIO= .00							
RTE3	MANE	1.25	2.26	745.00	.50	5.00	2.26	745.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1336E+01 EXCESS= .0000E+00 OUTFLOW= .1323E+01 BASIN STORAGE= .1421E-01 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT E3	MANE	2.19	214.40	723.98	.72	5.00	211.41	725.00	.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1851E+02 EXCESS= .0000E+00 OUTFLOW= .1846E+02 BASIN STORAGE= .6918E-01 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT E3	MANE	3.50	205.63	728.00	.72	5.00	196.52	730.00	.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1845E+02 EXCESS= .0000E+00 OUTFLOW= .1837E+02 BASIN STORAGE= .1198E+00 PERCENT ERROR= -.2									
FOR PLAN = 1		RATIO= .00							
RT E4	MANE	3.53	192.31	731.27	.71	5.00	187.57	730.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1836E+02 EXCESS= .0000E+00 OUTFLOW= .1827E+02 BASIN STORAGE= .1105E+00 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT E4	MANE	2.15	68.68	727.70	1.59	5.00	66.45	725.00	1.59
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8479E+01 EXCESS= .0000E+00 OUTFLOW= .8463E+01 BASIN STORAGE= .3004E-01 PERCENT ERROR= -.2									
FOR PLAN = 1		RATIO= .00							
RT N1	MANE	1.75	527.46	741.36	.40	5.00	524.16	740.00	.40
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3716E+02 EXCESS= .0000E+00 OUTFLOW= .3714E+02 BASIN STORAGE= .5565E-01 PERCENT ERROR= -.1									
FOR PLAN = 1		RATIO= .00							
RT N1	MANE	4.13	524.45	744.13	.40	5.00	520.20	745.00	.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3715E+02 EXCESS= .0000E+00 OUTFLOW= .3711E+02 BASIN STORAGE= .1322E+00 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT N1 MANE 2.78 514.77 747.09 .40 5.00 511.73 745.00 .40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3711E+02 EXCESS= .0000E+00 OUTFLOW= .3706E+02 BASIN STORAGE= .1116E+00 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT N1 MANE 3.56 815.58 752.02 .41 5.00 810.13 755.00 .41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7198E+02 EXCESS= .0000E+00 OUTFLOW= .7193E+02 BASIN STORAGE= .1395E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N1 MANE 2.36 809.53 754.46 .41 5.00 808.79 755.00 .41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7195E+02 EXCESS= .0000E+00 OUTFLOW= .7189E+02 BASIN STORAGE= .1172E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N1 MANE 1.20 17.99 727.21 2.95 5.00 17.57 730.00 2.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6939E+01 EXCESS= .0000E+00 OUTFLOW= .6929E+01 BASIN STORAGE= .1264E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RT W3 MANE 1.66 1291.37 751.31 .43 5.00 1279.89 750.00 .43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1159E+03 EXCESS= .0000E+00 OUTFLOW= .1158E+03 BASIN STORAGE= .1849E+00 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N4 MANE 3.20 95.23 722.71 1.01 5.00 88.38 720.00 1.01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8099E+01 EXCESS= .0000E+00 OUTFLOW= .8067E+01 BASIN STORAGE= .4219E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N4 MANE 2.39 87.38 722.64 1.00 5.00 85.32 725.00 1.01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8053E+01 EXCESS= .0000E+00 OUTFLOW= .8029E+01 BASIN STORAGE= .3054E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT N4 MANE 4.00 84.88 728.00 1.00 5.00 80.39 730.00 1.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8045E+01 EXCESS= .0000E+00 OUTFLOW= .7986E+01 BASIN STORAGE= .8840E-01 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RT 14 MANE 5.00 6.00 755.00 7.43 5.00 6.00 755.00 7.43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2890E+01 EXCESS= .0000E+00 OUTFLOW= .2779E+01 BASIN STORAGE= .1348E+00 PERCENT ERROR= -.8

FOR PLAN = 1 RATIO= .00
RT 13 MANE 1.10 6406.63 1044.13 .98 5.00 6406.56 1045.00 .98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4443E+04 EXCESS= .0000E+00 OUTFLOW= .4438E+04 BASIN STORAGE= .5986E+01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RT 12 MANE 5.00 6411.11 1055.00 .96 5.00 6411.11 1055.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4453E+04 EXCESS= .0000E+00 OUTFLOW= .4397E+04 BASIN STORAGE= .6710E+02 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT W7 MANE 2.12 26.74 730.83 2.06 5.00 26.36 730.00 2.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6847E+01 EXCESS= .0000E+00 OUTFLOW= .6831E+01 BASIN STORAGE= .2881E-01 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT MANE 2.00 48.84 727.10 3.58 5.00 47.84 730.00 3.58

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1933E+02 EXCESS= .0000E+00 OUTFLOW= .1929E+02 BASIN STORAGE= .6615E-01 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RT MANE .94 65.63 729.55 4.43 5.00 65.61 730.00 4.43

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3030E+02 EXCESS= .0000E+00 OUTFLOW= .3026E+02 BASIN STORAGE= .4590E-01 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RT MANE 2.38 76.68 731.86 4.72 5.00 76.08 730.00 4.73

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3737E+02 EXCESS= .0000E+00 OUTFLOW= .3727E+02 BASIN STORAGE= .1415E+00 PERCENT ERROR= -.1

FOR PLAN = 1	RATIO= .00									
RTto4	MANE	.46	6451.52	1054.74	.97	5.00	6451.47	1055.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4431E+04 EXCESS= .0000E+00 OUTFLOW= .4429E+04 BASIN STORAGE= .2591E+01 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO= .00									
RTto3	MANE	.42	6457.31	1054.94	.97	5.00	6457.30	1055.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4435E+04 EXCESS= .0000E+00 OUTFLOW= .4433E+04 BASIN STORAGE= .2330E+01 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO= .00									
RTto2	MANE	.42	6463.12	1055.02	.97	5.00	6463.12	1055.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4440E+04 EXCESS= .0000E+00 OUTFLOW= .4438E+04 BASIN STORAGE= .2333E+01 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO= .00									
RTStBV	MANE	.68	6465.35	1055.08	.97	5.00	6465.33	1055.00	.97	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4440E+04 EXCESS= .0000E+00 OUTFLOW= .4437E+04 BASIN STORAGE= .3723E+01 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO= .00									
RT5-3	MANE	5.00	98.31	740.00	4.04	5.00	98.31	740.00	4.04	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2975E+02 EXCESS= .0000E+00 OUTFLOW= .2917E+02 BASIN STORAGE= .6256E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
E14-E1	MANE	1.62	412.48	728.62	2.22	5.00	411.06	730.00	2.22	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5538E+02 EXCESS= .0000E+00 OUTFLOW= .5527E+02 BASIN STORAGE= .1670E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
E1-E2	MANE	1.21	413.41	731.11	2.36	5.00	413.31	730.00	2.36	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5942E+02 EXCESS= .0000E+00 OUTFLOW= .5936E+02 BASIN STORAGE= .1343E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
E2-E3	MANE	1.21	411.54	730.41	2.43	5.00	409.39	730.00	2.43	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6164E+02 EXCESS= .0000E+00 OUTFLOW= .6158E+02 BASIN STORAGE= .1392E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
E3-E4	MANE	1.46	408.98	731.46	2.49	5.00	402.02	730.00	2.49	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6347E+02 EXCESS= .0000E+00 OUTFLOW= .6334E+02 BASIN STORAGE= .1720E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
PK-CAR	MANE	2.65	520.86	732.14	2.57	5.00	515.01	735.00	2.58	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8632E+02 EXCESS= .0000E+00 OUTFLOW= .8602E+02 BASIN STORAGE= .4259E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
RT1-2	MANE	5.00	530.03	735.00	2.77	5.00	530.03	735.00	2.77	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9902E+02 EXCESS= .0000E+00 OUTFLOW= .9834E+02 BASIN STORAGE= .9926E+00 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO= .00									
RT2-3	MANE	2.34	539.29	738.46	2.84	5.00	536.73	740.00	2.84	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1053E+03 EXCESS= .0000E+00 OUTFLOW= .1050E+03 BASIN STORAGE= .4521E+00 PERCENT ERROR= -.2										
FOR PLAN = 1	RATIO= .00									
RT3-4	MANE	1.60	556.29	740.48	3.08	5.00	554.78	740.00	3.08	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1220E+03 EXCESS= .0000E+00 OUTFLOW= .1218E+03 BASIN STORAGE= .3505E+00 PERCENT ERROR= -.1										
FOR PLAN = 1	RATIO= .00									
RT4-5	MANE	.87	569.85	740.54	3.16	5.00	568.79	740.00	3.16	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1354E+03 EXCESS= .0000E+00 OUTFLOW= .1353E+03 BASIN STORAGE= .2078E+00 PERCENT ERROR= .0										
FOR PLAN = 1	RATIO= .00									
RT5-6	MANE	2.04	562.72	741.73	3.17	5.00	557.94	745.00	3.17	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1367E+03 EXCESS= .0000E+00 OUTFLOW= .1364E+03 BASIN STORAGE= .4902E+00 PERCENT ERROR= -.1										

FOR PLAN = 1 RATIO= .00
RT6-7 MANE 5.00 557.74 750.00 3.23 5.00 557.74 750.00 3.23

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1427E+03 EXCESS= .0000E+00 OUTFLOW= .1414E+03 BASIN STORAGE= .1791E+01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RT WT2 MANE 5.00 1271.33 835.00 2.36 5.00 1271.33 835.00 2.36

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2918E+03 EXCESS= .0000E+00 OUTFLOW= .2881E+03 BASIN STORAGE= .5190E+01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RT WT2 MANE 5.00 1215.49 870.00 2.31 5.00 1215.49 870.00 2.31

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2843E+03 EXCESS= .0000E+00 OUTFLOW= .2824E+03 BASIN STORAGE= .3325E+01 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RT WHC MANE 5.00 2049.74 870.00 .86 5.00 2049.74 870.00 .86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7837E+03 EXCESS= .0000E+00 OUTFLOW= .7786E+03 BASIN STORAGE= .6366E+01 PERCENT ERROR= -.2

FOR PLAN = 1 RATIO= .00
RT DET MANE 5.00 2054.69 875.00 .85 5.00 2054.69 875.00 .85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7858E+03 EXCESS= .0000E+00 OUTFLOW= .7804E+03 BASIN STORAGE= .7286E+01 PERCENT ERROR= -.2

1

HEC-1 INPUT

PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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*

*** NORMAL END OF HEC-1 ***


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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 04JAN08 TIME 11:08:39
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX KXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID *****
2 ID TRUNCATED MODEL FOR DAMONTE RANCH PHASE V and BELLA VESTA RANCH PHASE 1
3 ID JANUARY 2008
4 ID *****
5 ID FILE NAME: BVCHK.DAT IS A PORTION OF DRph1+BVL.DAT THE PROPOSED
6 ID CONDITION MODEL FOR BELLA VISTA PHASE 1
7 ID THIS MODEL TO BE USED ONLY FOR CHECKING EXISTING CONDITIONS MODEL FOR
8 ID FLOWS IN STEAMBOAT CHANNEL AT THE COMMON BOUNDARY LINE BETWEEN DAMONTE
9 ID PHASE 5 AND BELLA VISTA PHASE 1.

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3 COMBINED AT
+ DMNTE 84.43 1 FLOW 6384.
TIME 17.42

```

DMNTE is the combined runoff from the Damonte Phase V Model. Subbasins for Channel A the Westside Channel have been eliminated from the Model as well as all downstream subbasins. The model was combined at a point in Steamboat Channel just below the Damonte Wetlands and the routing cards were not corrected.

Complete copies of the Model are included on the CD submitted with the LOMR application.

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 04JAN08 TIME 11:04:40
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X XXXXXXX XXXXX      X
X   X X      X   X      XX
X   X X      X           X
XXXXXXX XXXX X           XXXX X
X   X X      X           X
X   X X      X   X      X
X   X XXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID *****
2 ID TRUNCATED MODEL FOR DAMONTE RANCH PHASE V and BELLA VESTA RANCH PHASE 1
3 ID JANUARY 2008
4 ID *****
5 ID FILE NAME: DRCHK.dat IS A PORTION OF DRph1.DAT THE EXISTING
6 ID CONDITION MODEL FOR BELLA VISTA PHASE 1
7 ID THIS MODEL TO BE USED ONLY FOR CHECKING EXISTING CONDITIONS MODEL FOR
8 ID FLOWS IN STEAMBOAT CHANNEL AT THE COMMON BOUNDARY LINE BETWEEN DAMONTE
9 ID PHASE 5 AND BELLA VISTA PHASE 1.
10 ID *****

```

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3 COMBINED AT
+ DRSUM      84.45      1 FLOW      6382.
  TIME      17.42

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DRSUM is the combined runoff from the Damonte Phase V Model. Subbasins for Channel A the Westside Channel have been eliminated from the Model as well as all downstream subbasins. The model was combined at a point in Steamboat Channel just below the Damonte Wetlands and the routing cards were not corrected.

Complete copies of the Model are included on the CD submitted with the LOMR application.

APPENDIX D

HEC-RAS MODELS

Steamboat

Damonte Wetlands

East-West

HEC-RAS Plan: LOMR River Steamboat Reach: Bella Vista Profile: PF 1

Reach	River Sta	Profile	Q.Total (cfs)	Min Chl El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Bella Vista	90.9	PF 1	4193.00	4444.03	4451.33	4449.12	4451.86	0.003751	5.85	716.91	136.41	0.45
Bella Vista	90	PF 1	4193.00	4444.78	4450.38		4451.33	0.008219	7.83	536.69	153.62	0.74
Bella Vista	89.5	PF 1	4193.00	4443.89	4450.21		4450.91	0.005993	6.67	628.29	156.42	0.59
Bella Vista	89	PF 1	4193.00	4443.75	4450.15		4450.67	0.002509	5.80	723.08	157.48	0.48
Bella Vista	88.83	PF 1	4193.00	4443.65	4450.11		4450.63	0.002520	5.78	726.02	155.95	0.47
Bella Vista	88.68	PF 1	4193.00	4443.49	4449.99		4450.57	0.004827	6.12	685.43	151.41	0.51
Bella Vista	88	PF 1	4193.00	4443.30	4449.71		4450.31	0.003047	6.22	674.57	145.04	0.51
Bella Vista	87.85	PF 1	4193.00	4443.05	4449.40		4450.09	0.006108	6.66	629.27	145.09	0.56
Bella Vista	87.55	PF 1	4193.00	4442.92	4449.08		4449.91	0.007504	7.29	575.20	135.01	0.62
Bella Vista	87.3	PF 1	4193.00	4442.78	4448.56	4447.81	4449.66	0.010837	8.40	499.23	124.81	0.74
Bella Vista	87.05	PF 1	4193.00	4442.63	4447.75	4447.75	4449.49	0.002014	10.59	395.94	114.46	1.00
Bella Vista	86.97	PF 1	4193.00	4441.70	4445.67	4446.71	4449.28	0.006950	15.25	274.91	117.72	1.76
Bella Vista	86.89	PF 1	4193.00	4440.76	4444.35	4445.69	4449.09	0.011397	17.48	239.88	121.51	2.19
Bella Vista	86.81	PF 1	4193.00	4439.83	4443.16	4444.67	4448.89	0.016297	19.21	218.28	125.39	2.57
Bella Vista	86.73	PF 1	4193.00	4438.90	4442.02	4443.65	4448.65	0.021714	20.65	203.02	129.34	2.90
Bella Vista	86.45	Bridge										
Bella Vista	85.94	PF 1	4193.00	4437.56	4441.09	4442.40	4445.74	0.012815	17.32	242.15	136.46	2.29
Bella Vista	85.88	PF 1	4193.00	4437.34	4440.94	4442.26	4445.66	0.013007	17.44	240.47	136.13	2.31
Bella Vista	85.82	PF 1	4193.00	4437.10	4440.78	4442.11	4445.57	0.013234	17.57	238.68	135.76	2.33
Bella Vista	85.76	PF 1	4193.00	4436.87	4440.63	4441.97	4445.48	0.013456	17.69	237.02	135.40	2.36
Bella Vista	85.7	PF 1	4193.00	4436.64	4440.47	4441.87	4445.40	0.013691	17.82	235.33	135.04	2.38
Bella Vista	85.6*	PF 1	4193.00	4436.63	4440.51	4441.79	4444.92	0.152159	16.86	248.70	139.95	2.23
Bella Vista	85.5*	PF 1	4193.00	4436.63	4443.28	4441.73	4443.89	0.006407	6.26	689.40	152.62	0.53
Bella Vista	85.4*	PF 1	4193.00	4436.62	4443.24	4441.64	4443.81	0.006107	6.09	688.81	158.86	0.52
Bella Vista	85.3*	PF 1	4193.00	4436.61	4443.20	4441.58	4443.74	0.005814	5.91	709.49	165.50	0.50
Bella Vista	85.2*	PF 1	4193.00	4436.60	4443.17	4441.49	4443.68	0.005498	5.72	732.91	172.66	0.49
Bella Vista	85.1*	PF 1	4193.00	4436.60	4443.14	4441.43	4443.61	0.005201	5.53	757.95	180.56	0.48
Bella Vista	85	PF 1	4193.00	4436.59	4443.11	4441.34	4443.55	0.004870	5.32	787.58	189.58	0.46
Bella Vista	84.5	Lat Struct										
Bella Vista	84	PF 1	4031.64	4436.31	4442.98	4440.74	4443.24	0.001542	4.12	984.31	246.30	0.36
Bella Vista	83	PF 1	4031.64	4436.11	4442.86	4440.31	4443.10	0.001170	3.93	1026.61	223.49	0.32
Bella Vista	82	PF 1	4031.64	4435.92	4442.72	4440.36	4442.97	0.001325	4.08	989.22	224.75	0.34
Bella Vista	81	PF 1	4031.64	4435.92	4442.52	4440.54	4442.82	0.001685	4.40	917.31	225.95	0.38
Bella Vista	80	PF 1	4031.64	4435.69	4442.35	4440.34	4442.65	0.001679	4.42	912.50	222.76	0.38
Bella Vista	79	PF 1	4031.64	4435.16	4442.10	4440.46	4442.46	0.002162	4.80	840.58	223.23	0.44
Bella Vista	78	PF 1	4031.64	4435.10	4441.93	4440.06	4442.25	0.001818	4.56	894.60	220.63	0.40
Bella Vista	77	PF 1	4031.64	4435.05	4441.67	4440.06	4442.04	0.002328	4.90	822.59	219.86	0.45
Bella Vista	76	PF 1	4031.64	4434.88	4441.24	4440.10	4441.74	0.003607	5.69	708.09	210.50	0.55
Bella Vista	75.25	PF 1	4031.64	4434.54	4441.04	4439.67	4441.47	0.002979	5.26	767.14	216.71	0.49

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	Q Total (cfs)	Min Ch E (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.C. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #/Chl
Bella Vista	75	PF 1	4031.64	4434.43	4440.96		4441.38	0.004462	5.14	784.02	218.85	0.48
Bella Vista	74.75	PF 1	4031.64	4434.09	4440.88		4441.26	0.003984	4.94	815.62	221.99	0.45
Bella Vista	74	PF 1	4031.64	4433.08	4440.77		4441.06	0.001554	4.26	945.90	231.37	0.37
Bella Vista	73	PF 1	4031.64	4432.70	4440.68		4440.92	0.001018	3.96	1018.18	227.69	0.33
Bella Vista	72	PF 1	4031.64	4432.92	4440.58		4440.82	0.000957	3.89	1035.42	224.05	0.32
Bella Vista	71.25	PF 1	4031.64	4433.06	4440.51		4440.74	0.000999	3.92	1028.01	223.46	0.32
Bella Vista	71	PF 1	4031.64	4433.10	4440.48		4440.72	0.001117	3.93	1025.58	223.28	0.32
Bella Vista	70.6	PF 1	4031.64	4432.99	4440.43		4440.67	0.001134	3.92	1029.65	227.23	0.32
Bella Vista	70	PF 1	4051.64	4432.83	4440.37		4440.60	0.001128	3.89	1040.35	232.03	0.32
Bella Vista	69.75	PF 1	4051.64	4432.73	4440.33		4440.58	0.001145	3.93	1030.25	230.56	0.33
Bella Vista	69	PF 1	4051.64	4432.44	4440.22		4440.48	0.001277	4.09	991.27	225.85	0.34
Bella Vista	68	PF 1	4051.64	4432.50	4440.02		4440.33	0.001656	4.46	909.34	221.11	0.39
Bella Vista	67	PF 1	4051.64	4432.30	4439.92		4440.17	0.001230	4.06	998.83	222.57	0.34
Bella Vista	66.75	PF 1	4051.64	4432.23	4439.89		4440.14	0.001375	4.04	1002.81	222.71	0.34
Bella Vista	66	PF 1	4051.64	4432.01	4439.80		4440.04	0.001180	4.00	1012.71	223.42	0.33
Bella Vista	65	PF 1	4051.64	4432.09	4439.62		4439.91	0.001486	4.31	939.07	220.22	0.37
Bella Vista	64	PF 1	4051.64	4432.00	4439.49		4439.76	0.001375	4.22	960.60	219.85	0.36
Bella Vista	63	PF 1	4051.64	4431.64	4439.38		4439.63	0.001169	4.01	1010.94	221.99	0.33
Bella Vista	62	PF 1	4051.64	4431.47	4439.26		4439.51	0.001208	3.99	1014.87	225.81	0.33
Bella Vista	61	PF 1	4051.64	4431.32	4439.17		4439.38	0.001071	3.70	1094.81	244.37	0.31
Bella Vista	60	PF 1	4051.64	4431.12	4439.10		4439.28	0.000845	3.35	1208.60	247.21	0.27
Bella Vista	59	PF 1	4051.64	4431.00	4439.02		4439.19	0.000838	3.32	1219.63	251.25	0.27
Bella Vista	58	PF 1	4114.64	4430.60	4438.97		4439.11	0.000610	3.02	1361.79	255.26	0.23
Bella Vista	57	PF 1	4400.64	4430.43	4438.89		4439.05	0.000652	3.17	1388.52	251.89	0.24
Bella Vista	56	PF 1	5231.64	4430.27	4438.71		4438.96	0.001072	3.97	1319.27	248.31	0.30
Bella Vista	55	PF 1	5771.64	4430.38	4438.56		4438.84	0.001142	4.25	1358.76	242.62	0.32
Bella Vista	54	PF 1	6099.64	4429.90	4438.37		4438.71	0.001483	4.68	1303.60	241.42	0.35
Bella Vista	53	PF 1	6227.64	4429.76	4438.18		4438.55	0.001471	4.92	1266.11	234.19	0.37
Bella Vista	52	PF 1	6245.64	4429.60	4438.05		4438.41	0.001382	4.77	1309.02	236.25	0.36
Bella Vista	51	PF 1	6245.64	4429.32	4437.91		4438.27	0.001293	4.80	1300.38	228.11	0.35
Bella Vista	50	PF 1	6245.64	4429.29	4437.76	4435.02	4438.13	0.001446	4.89	1276.66	234.45	0.37
Bella Vista	49.7		Lat Struct									
Bella Vista	49	PF 1	6064.75	4429.02	4437.64	4434.80	4437.99	0.001330	4.78	1269.61	230.28	0.36
Bella Vista	48	PF 1	6064.75	4429.09	4437.44	4434.88	4437.84	0.001612	5.05	1200.29	231.37	0.39
Bella Vista	47	PF 1	6064.75	4428.86	4437.23	4434.94	4437.66	0.001849	5.29	1147.41	229.25	0.42
Bella Vista	46	PF 1	6064.75	4428.65	4436.98	4434.86	4437.46	0.002149	5.55	1093.63	224.74	0.44
Bella Vista	45	PF 1	6064.75	4428.45	4436.82		4437.25	0.001825	5.21	1164.73	229.88	0.41
Bella Vista	44	PF 1	6064.75	4428.34	4436.58		4437.04	0.002116	5.47	1109.16	229.55	0.44
Bella Vista	43	PF 1	6064.75	4428.48	4436.37		4436.84	0.001992	5.47	1109.47	226.11	0.43

HEC-RAS Plan: LOMR River Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	Q Total (cfs)	Min Chl E (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Bella Vista	42	PF-1	6064.75	4428.55	4436.07		4436.61	0.002568	5.86	1035.34	228.71	0.49
Bella Vista	41	PF-1	6064.75	4428.16	4435.71		4436.33	0.002897	6.30	962.95	232.03	0.54
Bella Vista	40	PF-1	6064.75	4427.76	4435.54		4436.04	0.002143	5.71	1061.25	231.36	0.47
Bella Vista	39.75	PF-1	6064.75	4427.66	4435.49		4435.98	0.002707	5.60	1082.65	232.43	0.46
Bella Vista	39	PF-1	6064.75	4427.35	4435.37		4435.80	0.001715	5.29	1147.12	234.68	0.42
Bella Vista	38	PF-1	6064.75	4427.05	4435.22		4435.63	0.001561	5.14	1179.75	233.96	0.40
Bella Vista	37	PF-1	6064.75	4426.92	4435.04		4435.47	0.001679	5.28	1147.64	233.63	0.42
Bella Vista	36	PF-1	6064.75	4426.78	4434.91		4435.30	0.001426	5.02	1207.12	233.70	0.39
Bella Vista	35	PF-1	6064.75	4426.50	4434.74		4435.15	0.001535	5.16	1175.03	231.04	0.40
Bella Vista	34	PF-1	6064.75	4426.17	4434.54		4434.99	0.001678	5.38	1126.81	222.13	0.42
Bella Vista	33.75	PF-1	6064.75	4426.06	4434.49		4434.94	0.002423	5.39	1124.80	223.59	0.42
Bella Vista	33	PF-1	6109.75	4425.81	4434.32		4434.78	0.001780	5.45	1121.96	228.00	0.43
Bella Vista	32	PF-1	6109.75	4425.75	4434.18		4434.60	0.001599	5.25	1164.05	230.42	0.41
Bella Vista	31	PF-1	6109.75	4425.81	4434.08		4434.44	0.001265	4.86	1257.33	230.74	0.37
Bella Vista	30	PF-1	6109.75	4425.88	4433.91		4434.31	0.001447	5.07	1204.59	228.83	0.39
Bella Vista	29	PF-1	6109.75	4425.70	4433.75		4434.16	0.001470	5.13	1190.39	225.21	0.39
Bella Vista	28	PF-1	6109.75	4425.40	4433.60		4434.01	0.001492	5.12	1194.09	227.51	0.39
Bella Vista	27	PF-1	6109.75	4425.09	4433.39		4433.84	0.001787	5.40	1132.16	228.94	0.43
Bella Vista	26	PF-1	6109.75	4424.93	4433.23		4433.66	0.001672	5.30	1152.64	229.67	0.42
Bella Vista	25	PF-1	6109.75	4425.02	4433.07		4433.50	0.001621	5.23	1168.81	233.52	0.41
Bella Vista	24	PF-1	6109.75	4425.06	4432.93		4433.33	0.001471	5.09	1201.40	232.48	0.39
Bella Vista	23	PF-1	6109.75	4424.74	4432.82		4433.19	0.001243	4.87	1256.89	256.43	0.37
Bella Vista	22	PF-1	6109.75	4424.43	4432.67		4433.06	0.001300	4.98	1225.93	230.07	0.38
Bella Vista	21	PF-1	6109.75	4424.17	4432.55		4432.93	0.001295	4.95	1234.87	231.06	0.38
Bella Vista	20	PF-1	6109.75	4423.92	4432.24		4432.76	0.001913	5.77	1059.00	227.62	0.47
Bella Vista	19.8	PF-1	6109.75	4423.86	4432.22		4432.71	0.001764	5.62	1087.39	228.12	0.45
Bella Vista	19.55	PF-1	6109.75	4423.75	4432.18		4432.65	0.003055	5.51	1108.32	227.89	0.44
Bella Vista	19	PF-1	6109.75	4423.53	4432.14		4432.52	0.001299	4.92	1247.96	271.87	0.37
Bella Vista	18.25	PF-1	6109.75	4423.18	4432.10		4432.42	0.000970	4.49	1360.47	233.75	0.33
Bella Vista	18	PF-1	6134.75	4423.08	4432.07	4428.87	4432.39	0.001089	4.56	1352.31	262.65	0.33
Bella Vista	17	PF-1	6134.75	4422.80	4432.04	4428.39	4432.28	0.000732	3.96	1653.77	859.04	0.29
Bella Vista	16	PF-1	6134.75	4422.79	4431.98	4428.39	4432.20	0.000679	3.87	1890.24	1053.58	0.29
Bella Vista	15	PF-1	6134.75	4422.78	4431.93	4428.33	4432.13	0.000588	3.80	2163.06	1284.60	0.27
Bella Vista	14	PF-1	6134.75	4422.77	4431.86	4428.42	4432.07	0.000678	3.98	2321.96	1408.68	0.29
Bella Vista	13	PF-1	6134.75	4422.77	4431.84	4428.77	4431.99	0.000574	3.42	2792.12	1485.44	0.29
Bella Vista	12	PF-1	6134.75	4422.76	4431.74	4428.77	4431.92	0.000637	4.29	2862.36	1474.65	0.29
Bella Vista	11	PF-1	6134.75	4422.76	4431.53	4428.77	4431.82	0.001291	5.78	2476.18	1528.71	0.42
Bella Vista	10	PF-1	6134.75	4422.75	4431.42	4428.77	4431.66	0.001713	6.17	2467.24	1576.98	0.47
Bella Vista	9	PF-1	6134.75	4422.74	4431.27	4430.66	4431.46	0.001113	5.38	2855.20	1609.15	0.39

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	Q Total (cfs)	Min Chl El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Bella Vista	8	PF 1	6134.75	4422.74	4431.16	4430.42	4431.32	0.000998	5.11	2981.47	1595.94	0.37
Bella Vista	7	PF 1	6134.75	4422.73	4430.95	4430.23	4431.13	0.001137	5.37	2771.82	1443.85	0.39
Bella Vista	6	PF 1	6134.75	4422.72	4430.66	4430.14	4430.88	0.001546	5.86	2524.03	1412.74	0.45
Bella Vista	5	PF 1	6134.75	4422.71	4430.09	4430.06	4430.51	0.002761	7.57	2168.11	1771.68	0.59
Bella Vista	4	PF 1	6134.75	4422.71	4429.89	4429.72	4430.23	0.002320	7.00	2377.22	1746.16	0.54
Bella Vista	3	PF 1	6134.75	4422.80	4429.59	4429.50	4429.92	0.004278	7.69	2086.40	1687.42	0.69
Bella Vista	2	PF 1	6134.75	4422.23	4429.41	4427.84	4429.55	0.002399	4.74	2624.84	1718.97	0.50
Bella Vista	1	PF 1	6134.75	4421.90	4429.33	4428.13	4429.38	0.000985	2.75	3586.62	1795.14	0.31
Bella Vista	.225	PF 1	6134.75	4422.58	4428.78	4427.82	4428.85	0.003106	2.05	2990.74	2168.96	0.31

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frctn Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Bella Vista	90.9	PF 1	4451.86	4451.33	0.53	0.48	0.04		4193.00		136.41
Bella Vista	90	PF 1	4451.33	4450.38	0.95	0.35	0.08		4188.91	4.09	153.62
Bella Vista	89.5	PF 1	4450.91	4450.21	0.69	0.18	0.05		4193.00		156.42
Bella Vista	89	PF 1	4450.67	4450.15	0.52	0.04	0.00		4193.00		157.48
Bella Vista	88.83	PF 1	4450.63	4450.11	0.52	0.05	0.01		4193.00		155.95
Bella Vista	88.68	PF 1	4450.57	4449.99	0.58	0.26	0.00		4193.00		151.41
Bella Vista	88	PF 1	4450.31	4449.71	0.60	0.21	0.01		4193.00		145.04
Bella Vista	87.85	PF 1	4450.09	4449.40	0.69	0.17	0.01		4193.00		145.09
Bella Vista	87.55	PF 1	4449.91	4449.08	0.83	0.22	0.03		4193.00		135.01
Bella Vista	87.3	PF 1	4449.66	4448.56	1.10	0.10	0.06		4193.00		124.81
Bella Vista	87.05	PF 1	4449.49	4447.75	1.74	0.02	0.01		4193.00		114.46
Bella Vista	86.97	PF 1	4449.28	4445.67	3.61	0.03	0.19		4193.00		117.72
Bella Vista	86.89	PF 1	4449.09	4444.35	4.74	0.07	0.11		4193.00		121.51
Bella Vista	86.81	PF 1	4448.89	4443.16	5.73	0.11	0.10		4193.00		125.39
Bella Vista	86.73	PF 1	4448.65	4442.02	6.62	0.15	0.09		4193.00		129.34
Bella Vista	86.45		Bridge								
Bella Vista	85.94	PF 1	4445.74	4441.09	4.66				4193.00		136.46
Bella Vista	85.88	PF 1	4445.66	4440.94	4.72	0.08	0.01		4193.00		136.13
Bella Vista	85.82	PF 1	4445.57	4440.78	4.79	0.08	0.01		4193.00		135.76
Bella Vista	85.76	PF 1	4445.48	4440.63	4.86	0.08	0.01		4193.00		135.40
Bella Vista	85.7	PF 1	4445.40	4440.47	4.93	0.08	0.01		4193.00		135.04
Bella Vista	85.6*	PF 1	4444.92	4440.51	4.41	0.32	0.15		4193.00		139.95
Bella Vista	85.5*	PF 1	4443.89	4443.28	0.61	0.06	0.01		4193.00		152.62
Bella Vista	85.4*	PF 1	4443.81	4443.24	0.58	0.06	0.01		4193.00		158.86
Bella Vista	85.3*	PF 1	4443.74	4443.20	0.54	0.06	0.01		4193.00		165.50
Bella Vista	85.2*	PF 1	4443.68	4443.17	0.51	0.05	0.01		4193.00		172.66
Bella Vista	85.1*	PF 1	4443.61	4443.14	0.48	0.05	0.01		4193.00		180.56
Bella Vista	85	PF 1	4443.55	4443.11	0.44	0.26	0.05		4193.00		189.58
Bella Vista	84.5		Lat Struct								
Bella Vista	84	PF 1	4443.24	4442.98	0.26	0.13	0.01		4018.95	12.70	246.30
Bella Vista	83	PF 1	4443.10	4442.86	0.24	0.12	0.00		4031.64		223.49
Bella Vista	82	PF 1	4442.97	4442.72	0.26	0.15	0.00		4031.64		224.75
Bella Vista	81	PF 1	4442.82	4442.52	0.30	0.17	0.00		4031.64		225.95
Bella Vista	80	PF 1	4442.65	4442.35	0.30	0.19	0.01		4031.64		222.76
Bella Vista	79	PF 1	4442.46	4442.10	0.36	0.20	0.01		4031.64		223.23
Bella Vista	78	PF 1	4442.25	4441.93	0.32	0.20	0.01		4031.64		220.63

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frict. Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Bella Vista	77	PF 1	4442.04	4441.67	0.37	0.29	0.01		4031.64		219.86
Bella Vista	76	PF 1	4441.74	4441.24	0.50	0.25	0.02		4031.64		210.50
Bella Vista	75.25	PF 1	4441.47	4441.04	0.43	0.09	0.01		4031.64		216.71
Bella Vista	75	PF 1	4441.38	4440.96	0.41	0.11	0.01		4031.64		218.85
Bella Vista	74.75	PF 1	4441.26	4440.88	0.38	0.18	0.03		4031.64		221.99
Bella Vista	74	PF 1	4441.06	4440.77	0.28	0.12	0.01		4031.64		231.37
Bella Vista	73	PF 1	4440.92	4440.68	0.24	0.10	0.00		4031.64		227.69
Bella Vista	72	PF 1	4440.82	4440.58	0.24	0.07	0.00		4031.64		224.05
Bella Vista	71.25	PF 1	4440.74	4440.51	0.24	0.03	0.00		4031.64		223.46
Bella Vista	71	PF 1	4440.72	4440.48	0.24	0.05	0.00		4031.64		223.28
Bella Vista	70.6	PF 1	4440.67	4440.43	0.24	0.07	0.00		4031.64		227.23
Bella Vista	70	PF 1	4440.60	4440.37	0.24	0.03	0.00		4051.64		232.03
Bella Vista	69.75	PF 1	4440.58	4440.33	0.24	0.09	0.00		4051.64		230.56
Bella Vista	69	PF 1	4440.48	4440.22	0.26	0.14	0.00		4051.64		225.85
Bella Vista	68	PF 1	4440.33	4440.02	0.31	0.14	0.02		4051.64		221.11
Bella Vista	67	PF 1	4440.17	4439.92	0.26	0.03	0.00		4051.64		222.57
Bella Vista	66.75	PF 1	4440.14	4439.89	0.25	0.10	0.00		4051.64		222.71
Bella Vista	66	PF 1	4440.04	4439.80	0.25	0.13	0.00		4051.64		223.42
Bella Vista	65	PF 1	4439.91	4439.62	0.29	0.14	0.00		4051.64		220.22
Bella Vista	64	PF 1	4439.76	4439.49	0.28	0.13	0.01		4051.64		219.85
Bella Vista	63	PF 1	4439.63	4439.38	0.25	0.12	0.00		4051.64		221.99
Bella Vista	62	PF 1	4439.51	4439.26	0.25	0.11	0.01		4051.64		225.81
Bella Vista	61	PF 1	4439.38	4439.17	0.21	0.09	0.01		4051.64		244.37
Bella Vista	60	PF 1	4439.28	4439.10	0.17	0.08	0.00		4051.64		247.21
Bella Vista	59	PF 1	4439.19	4439.02	0.17	0.07	0.01		4051.64		251.25
Bella Vista	58	PF 1	4439.11	4438.97	0.14	0.06	0.00		4114.64		255.26
Bella Vista	57	PF 1	4439.05	4438.89	0.16	0.08	0.01		4400.64		251.89
Bella Vista	56	PF 1	4438.96	4438.71	0.24	0.11	0.00		5231.64		248.31
Bella Vista	55	PF 1	4438.84	4438.56	0.28	0.13	0.01		5771.64		242.62
Bella Vista	54	PF 1	4438.71	4438.37	0.34	0.15	0.00		6099.64		241.42
Bella Vista	53	PF 1	4438.55	4438.18	0.38	0.14	0.01		6227.64		234.19
Bella Vista	52	PF 1	4438.41	4438.05	0.35	0.13	0.00		6245.64		236.25
Bella Vista	51	PF 1	4438.27	4437.91	0.36	0.14	0.00		6245.64		228.11
Bella Vista	50	PF 1	4438.13	4437.76	0.37	0.14	0.01		6245.64		234.45
Bella Vista	49.7	Lat Struct									
Bella Vista	49	PF 1	4437.99	4437.64	0.35	0.15	0.00		6064.75		230.28

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frctn Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Bella Vista	48	PF 1	4437.84	4437.44	0.40	0.17	0.00		6064.75		231.37
Bella Vista	47	PF 1	4437.66	4437.23	0.43	0.20	0.00		6064.75		229.25
Bella Vista	46	PF 1	4437.46	4436.98	0.48	0.20	0.02		6064.75		224.74
Bella Vista	45	PF 1	4437.25	4436.82	0.42	0.20	0.00		6064.75		229.88
Bella Vista	44	PF 1	4437.04	4436.58	0.46	0.21	0.00		6064.75		229.55
Bella Vista	43	PF 1	4436.84	4436.37	0.46	0.23	0.01		6064.75		226.11
Bella Vista	42	PF 1	4436.61	4436.07	0.53	0.27	0.01		6064.75		228.71
Bella Vista	41	PF 1	4436.33	4435.71	0.62	0.25	0.03		6064.75		232.03
Bella Vista	40	PF 1	4436.04	4435.54	0.51	0.06	0.01		6064.75		231.36
Bella Vista	39.75	PF 1	4435.98	4435.49	0.49	0.16	0.02		6064.75		232.43
Bella Vista	39	PF 1	4435.80	4435.37	0.43	0.16	0.01		6064.75		234.68
Bella Vista	38	PF 1	4435.63	4435.22	0.41	0.16	0.00		6064.75		233.96
Bella Vista	37	PF 1	4435.47	4435.04	0.43	0.15	0.01		6064.75		233.63
Bella Vista	36	PF 1	4435.30	4434.91	0.39	0.15	0.00		6064.75		233.70
Bella Vista	35	PF 1	4435.15	4434.74	0.41	0.16	0.00		6064.75		231.04
Bella Vista	34	PF 1	4434.99	4434.54	0.45	0.05	0.00		6064.75		222.13
Bella Vista	33.75	PF 1	4434.94	4434.49	0.45	0.15	0.00		6064.75		223.59
Bella Vista	33	PF 1	4434.78	4434.32	0.46	0.17	0.01		6109.75		228.00
Bella Vista	32	PF 1	4434.60	4434.18	0.43	0.14	0.02		6109.75		230.42
Bella Vista	31	PF 1	4434.44	4434.08	0.37	0.14	0.00		6109.75		230.74
Bella Vista	30	PF 1	4434.31	4433.91	0.40	0.15	0.00		6109.75		228.83
Bella Vista	29	PF 1	4434.16	4433.75	0.41	0.15	0.00		6109.75		225.21
Bella Vista	28	PF 1	4434.01	4433.60	0.41	0.16	0.00		6109.75		227.51
Bella Vista	27	PF 1	4433.84	4433.39	0.45	0.17	0.00		6109.75		228.94
Bella Vista	26	PF 1	4433.66	4433.23	0.44	0.16	0.00		6109.75		229.67
Bella Vista	25	PF 1	4433.50	4433.07	0.42	0.15	0.01		6109.75		233.52
Bella Vista	24	PF 1	4433.33	4432.93	0.40	0.14	0.01		6109.75		232.48
Bella Vista	23	PF 1	4433.19	4432.82	0.37	0.13	0.00		6109.31	0.44	256.43
Bella Vista	22	PF 1	4433.06	4432.67	0.39	0.13	0.00		6109.75		230.07
Bella Vista	21	PF 1	4432.93	4432.55	0.38	0.16	0.01		6109.75		231.06
Bella Vista	20	PF 1	4432.76	4432.24	0.52	0.04	0.01		6109.75		227.62
Bella Vista	19.8	PF 1	4432.71	4432.22	0.49	0.06	0.01		6109.75		228.12
Bella Vista	19.55	PF 1	4432.65	4432.18	0.47	0.10	0.03		6109.75		227.89
Bella Vista	19	PF 1	4432.52	4432.14	0.38	0.08	0.02		6106.89	2.86	271.87
Bella Vista	18.25	PF 1	4432.42	4432.10	0.31	0.03	0.00		6109.75		233.75
Bella Vista	18	PF 1	4432.39	4432.07	0.32	0.09	0.02		6131.51	3.24	262.65

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1 (Continued)

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frict Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Bella Vista	17	PF 1	4432.28	4432.04	0.24	0.07	0.01	95.28	6004.46	35.01	859.04
Bella Vista	16	PF 1	4432.20	4431.98	0.22	0.06	0.01	393.75	5669.47	71.53	1053.58
Bella Vista	15	PF 1	4432.13	4431.93	0.20	0.06	0.00	651.57	5407.93	75.25	1284.60
Bella Vista	14	PF 1	4432.07	4431.86	0.21	0.06	0.02	827.67	5181.88	125.19	1408.68
Bella Vista	13	PF 1	4431.99	4431.84	0.15	0.06	0.00	1141.01	4947.88	45.86	1485.44
Bella Vista	12	PF 1	4431.92	4431.74	0.19	0.09	0.01	1817.19	3807.80	509.76	1474.65
Bella Vista	11	PF 1	4431.82	4431.53	0.29	0.15	0.01	2045.14	3186.87	902.75	1528.71
Bella Vista	10	PF 1	4431.66	4431.42	0.24	0.18	0.02	2963.09	2094.49	1077.18	1576.98
Bella Vista	9	PF 1	4431.46	4431.27	0.19	0.13	0.01	2840.00	2185.94	1108.80	1609.15
Bella Vista	8	PF 1	4431.32	4431.16	0.16	0.19	0.00	2832.31	2052.46	1249.98	1595.94
Bella Vista	7	PF 1	4431.13	4430.95	0.18	0.24	0.00	2993.01	2024.17	1117.57	1443.85
Bella Vista	6	PF 1	4430.88	4430.66	0.23	0.35	0.02	2975.77	2197.51	961.46	1412.74
Bella Vista	5	PF 1	4430.51	4430.09	0.42	0.25	0.02	2430.92	2658.02	1045.81	1771.68
Bella Vista	4	PF 1	4430.23	4429.89	0.34	0.31	0.00	2744.31	2534.87	855.57	1746.16
Bella Vista	3	PF 1	4429.92	4429.59	0.33	0.31	0.06	3782.09	1823.83	528.83	1687.42
Bella Vista	2	PF 1	4429.55	4429.41	0.13	0.15	0.03	4597.05	1537.70		1718.97
Bella Vista	1	PF 1	4429.38	4429.33	0.05	0.53	0.00	5361.23	749.88	23.64	1795.14
Bella Vista	.225	PF 1	4428.85	4428.78	0.07				6134.75		2168.96

Plan: LOMR Steamboat Bella Vista RS: 86.45 Profile: PF 1

E.G. US. (ft)	4448.65	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	4442.02	E.G. Elev (ft)	4448.14	4445.79
Q Total (cfs)	4193.00	W.S. Elev (ft)	4442.23	4441.35
Q Bridge (cfs)	4193.00	Crit. W.S. (ft)	4443.81	4442.64
Q Weir (cfs)		Max Chl Dpth (ft)	3.33	3.79
Weir Sta Lift (ft)		Vel Total (ft/s)	19.51	16.91
Weir Sta Rgt (ft)		Flow Area (sq ft)	214.92	248.00
Weir Submerg		Froude # Chl	1.88	1.53
Weir Max Depth (ft)		Specif Force (cu ft)	2853.71	2747.39
Min El Weir Flow (ft)	4451.49	Hydr Depth (ft)	1.79	2.07
Min El Prs (ft)	4446.86	W.P. Total (ft)	155.38	161.45
Delta EG (ft)	2.90	Conv. Total (cfs)	28317.6	35043.4
Delta WS (ft)	0.93	Top Width (ft)	120.01	119.58
BR Open Area (sq ft)	770.23	Frctn Loss (ft)		
BR Open Vel (ft/s)	19.51	C & E Loss (ft)		
Coef of Q		Shear Total (lb/sq ft)	1.89	1.37
Br Sel Method	Momentum	Power Total (lb/ft s)	36.94	23.21

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Crit.W.S. (ft)	Frctn Loss (ft)	C & E Loss (ft)	Top Width (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Vel Chnl (ft/s)
Bella Vista	86.81	PF 1	4448.89	4443.16	4444.67	0.11	0.10	125.39		4193.00		19.21
Bella Vista	86.73	PF 1	4448.65	4442.02	4443.65	0.15	0.09	129.34		4193.00		20.65
Bella Vista	86.45 BR U	PF 1	4448.14	4442.23	4443.81			120.01		4193.00		19.51
Bella Vista	86.45 BR D	PF 1	4445.79	4441.35	4442.64			119.58		4193.00		16.91
Bella Vista	85.94	PF 1	4445.74	4441.09	4442.40			136.46		4193.00		17.32
Bella Vista	85.88	PF 1	4445.66	4440.94	4442.26	0.08	0.01	136.13		4193.00		17.44

HEC-RAS Plan: LOMR River: Steamboat Reach: Bella Vista Profile: PF 1

Reach	River Sta	Profile	Q US (cfs)	Q Leaving Tail (cfs)	Q DS (cfs)	Q Weir (cfs)	Q Gales (cfs)	Wr Top Wdth (ft)	Weir Max Depth (ft)	Weir Avg Depth (ft)	Min El Weir Flow (ft)	E.G. US (ft)	W.S. US (ft)	E.G. DS (ft)	W.S. DS (ft)
Bella Vista	84.5	PF 1	4193.00	161.95	4031.64	161.95		77.19	0.93	0.77	4442.14	4443.52	4443.10	4443.28	4443.00
Bella Vista	49.7	PF 1	6245.64	181.29	6064.75	181.29		48.41	1.73	1.08	4436.00	4438.13	4437.76	4438.05	4437.69

Plan: LOMR Steamboat Bella Vista RS: 84.5 Lat Struct Profile: PF 1

E.G. US. (ft)	4443.52	Weir Sta US (ft)	0.00
W.S. US. (ft)	4443.10	Weir Sta DS (ft)	118.00
E.G. DS (ft)	4443.28	Weir Max Depth (ft)	0.93
W.S. DS (ft)	4443.00	Weir Avg Depth (ft)	0.77
Q US (cfs)	4193.00	Weir Submerg	0.00
Q Leaving Total (cfs)	161.95	Min El Weir Flow (ft)	4442.14
Q DS (cfs)	4031.64	Wr Top Width (ft)	77.19
Perc Q Leaving	3.85	Q Gate Group (cfs)	
Q Weir (cfs)	161.95	Gate Open Ht (ft)	
Q Gates (cfs)		Gate #Open	
Q Culv (cfs)		Gate Area (sq ft)	
Q Lat RC (cfs)		Gate Submerg	
Weir Flow Area (sq ft)	59.36	Gate Invert (ft)	
		Gate Weir Coef (ft)	

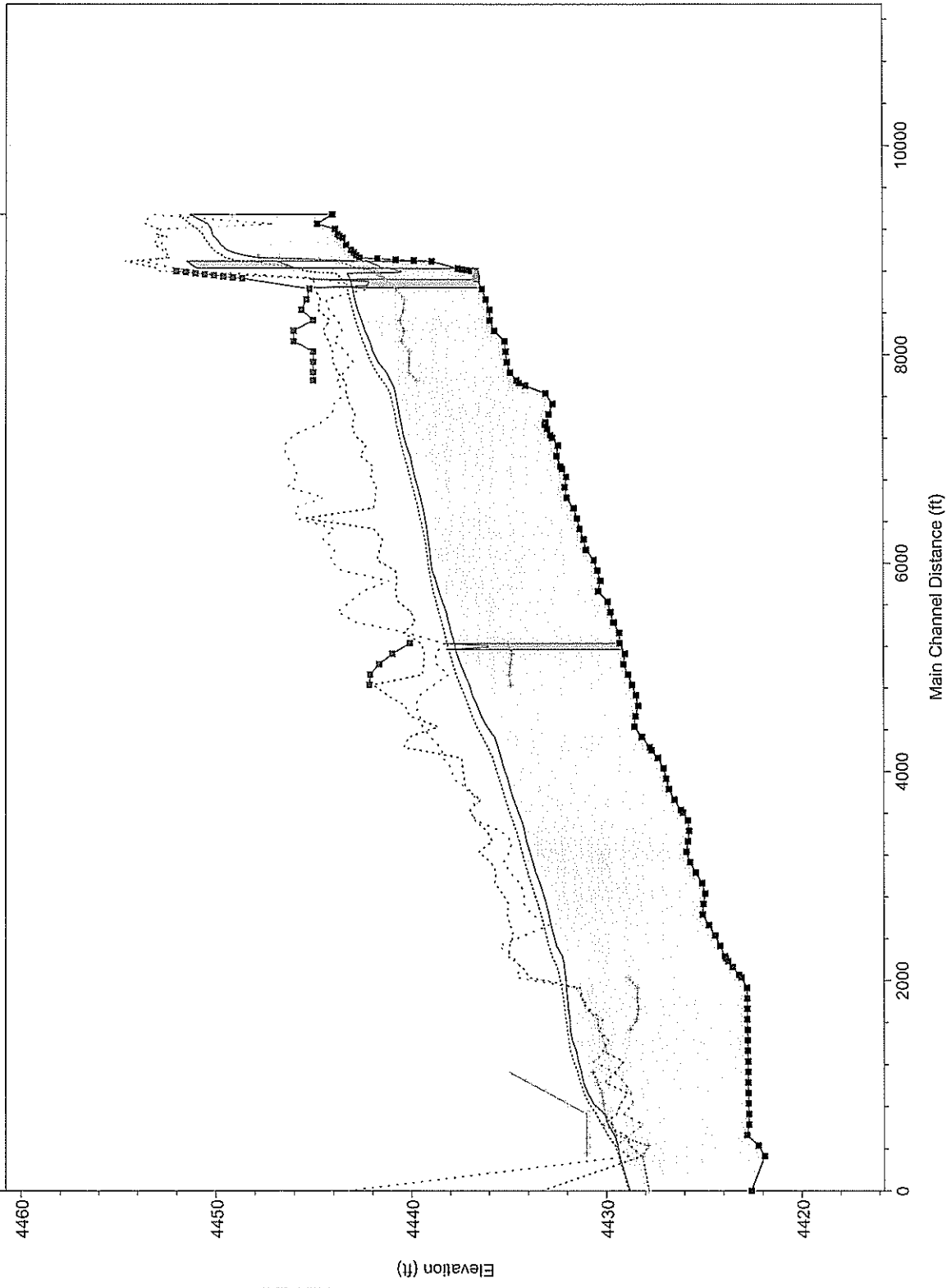
Plan: LOMR Steamboat Bella Vista RS: 49.7 Lat Struct Profile: PF 1

E.G. US. (ft)	4438.13	Weir Sta US (ft)	0.00
W.S. US. (ft)	4437.76	Weir Sta DS (ft)	59.00
E.G. DS (ft)	4438.05	Weir Max Depth (ft)	1.73
W.S. DS (ft)	4437.69	Weir Avg Depth (ft)	1.08
Q US (cfs)	6245.64	Weir Submerg	0.00
Q Leaving Total (cfs)	181.29	Min El Weir Flow (ft)	4436.00
Q DS (cfs)	6064.75	Wr Top Width (ft)	48.41
Perc Q Leaving	2.90	Q Gate Group (cfs)	
Q Weir (cfs)	181.29	Gate Open Ht (ft)	
Q Gates (cfs)		Gate #Open	
Q Culv (cfs)		Gate Area (sq ft)	
Q Lat RC (cfs)		Gate Submerg	
Weir Flow Area (sq ft)	52.32	Gate Invert (ft)	
		Gate Weir Coef (ft)	

From as-built topo Plan: LOMR Submittal 1/8/2008

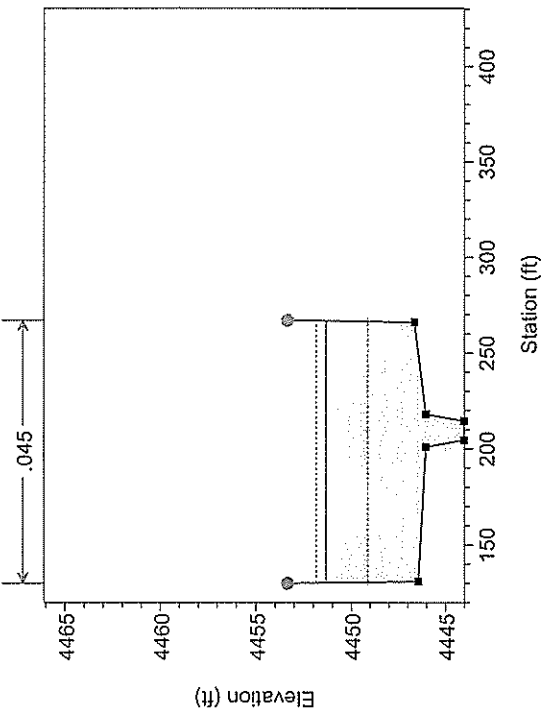
Steamboat Bella Vista

Legend	
.....	EG PF 1
-----	WS PF 1
.....	Crit PF 1
-----	Ground
.....	LOB
.....	ROB
-----	Left Levee
-----	Right Levee

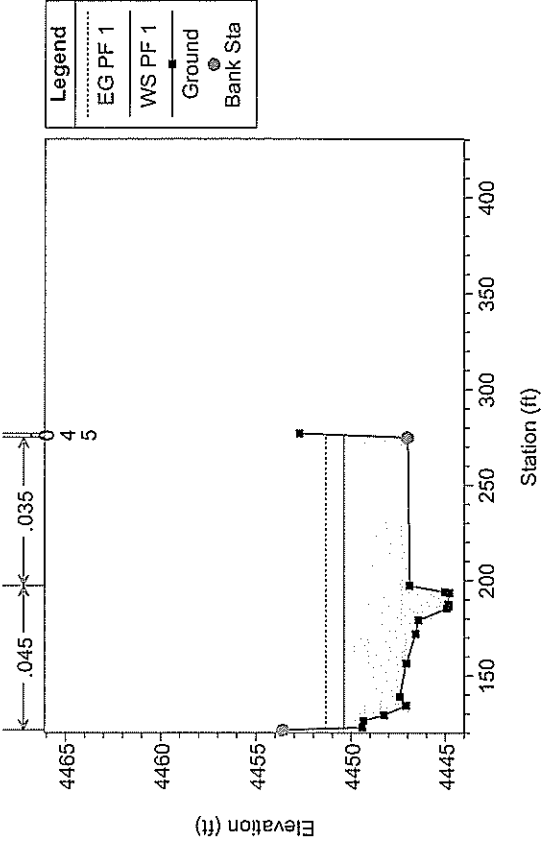


1 in Horiz. = 1500 ft 1 in Vert. = 8 ft

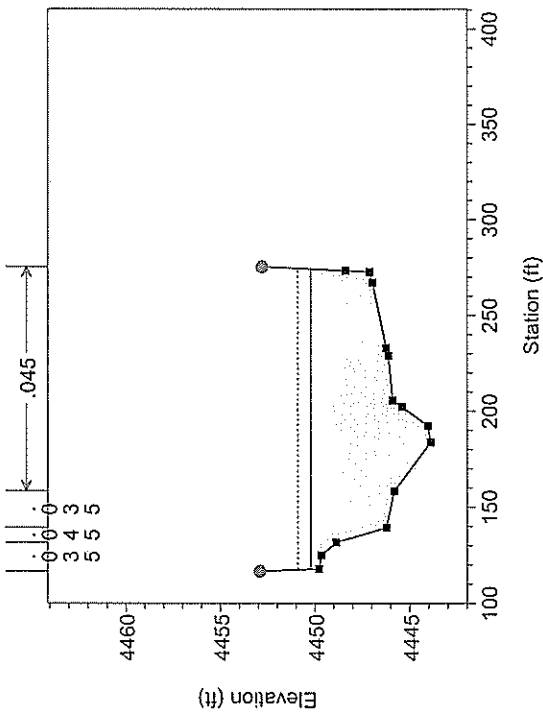
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 90.9



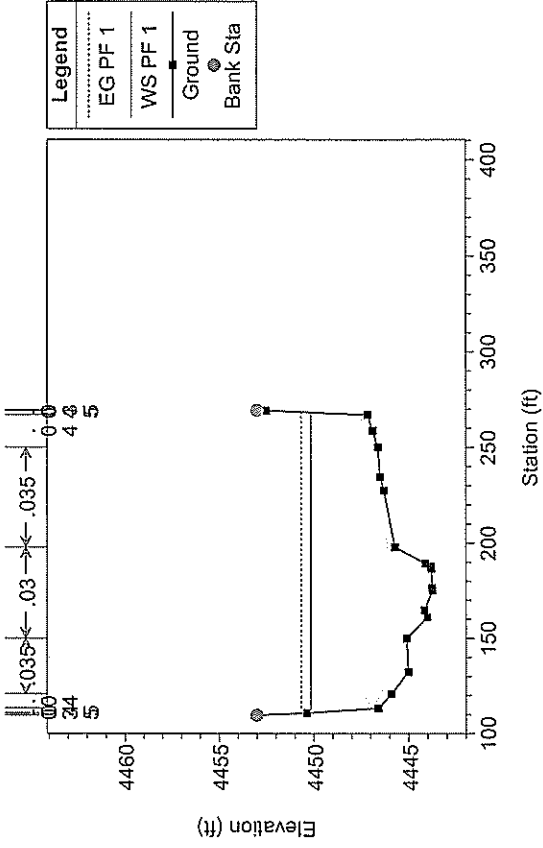
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 90



From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 89.5

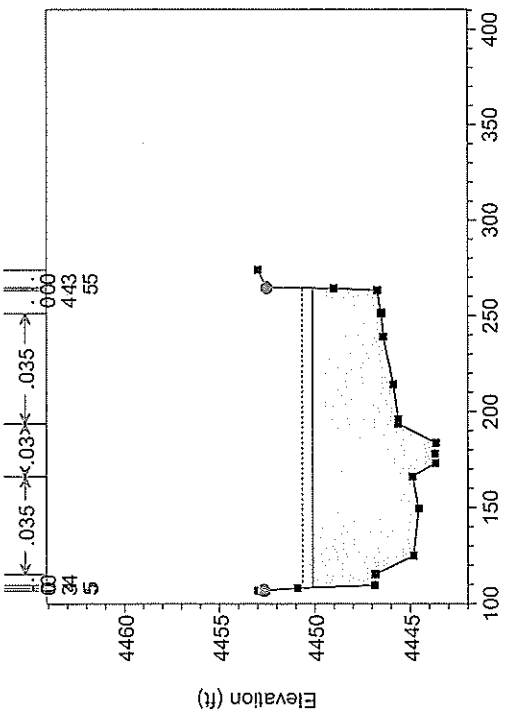


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 89

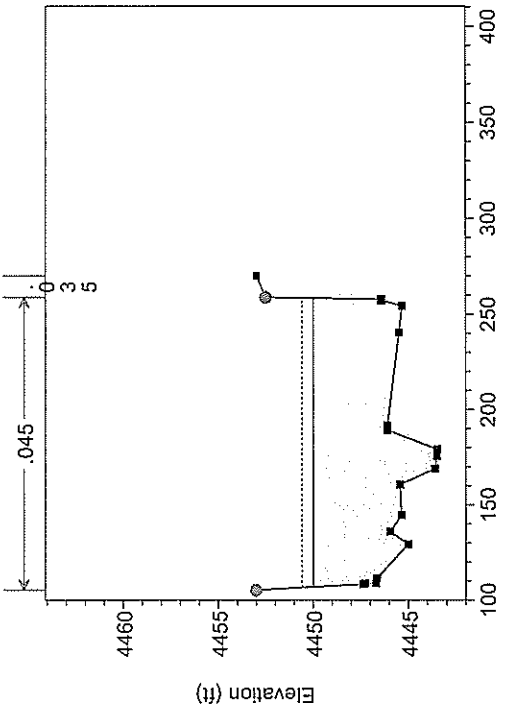


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

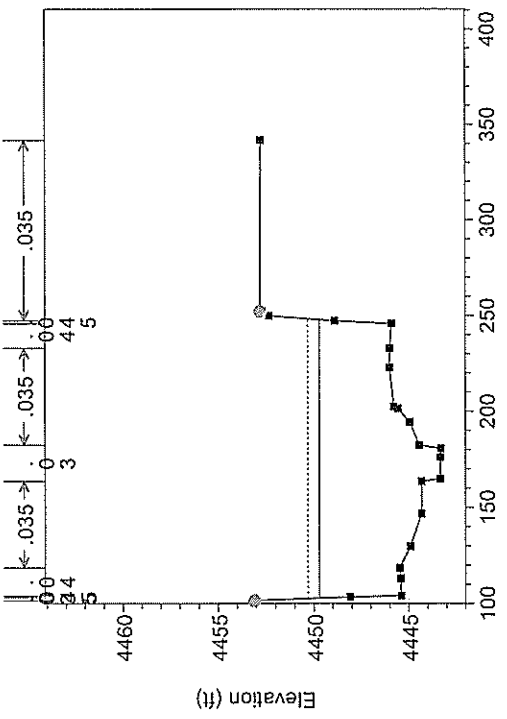
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 88.83



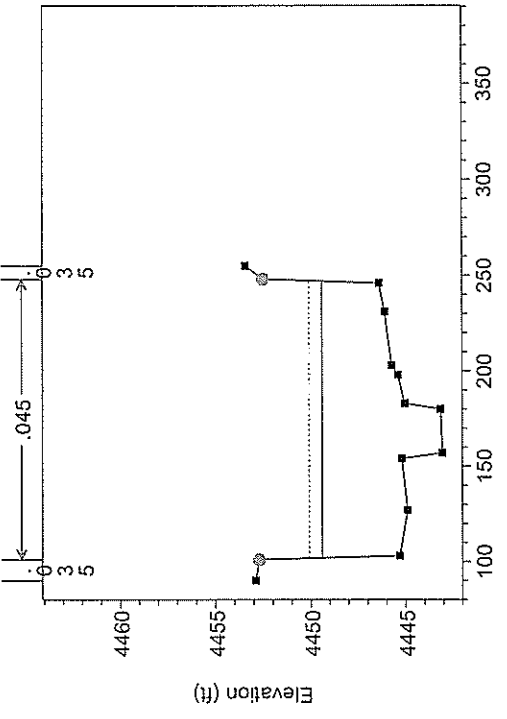
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 88.68



From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 88

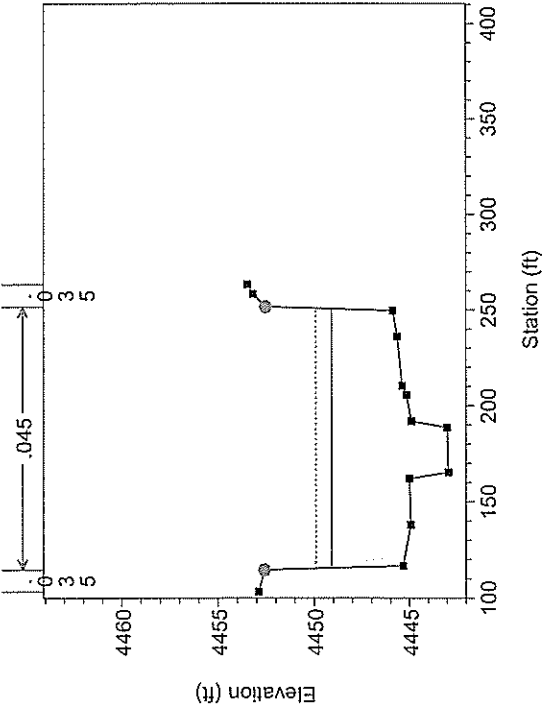


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 87.85

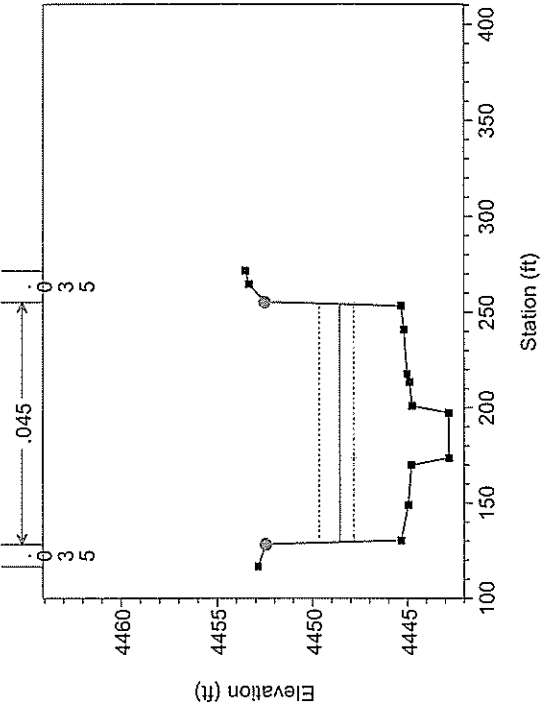


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

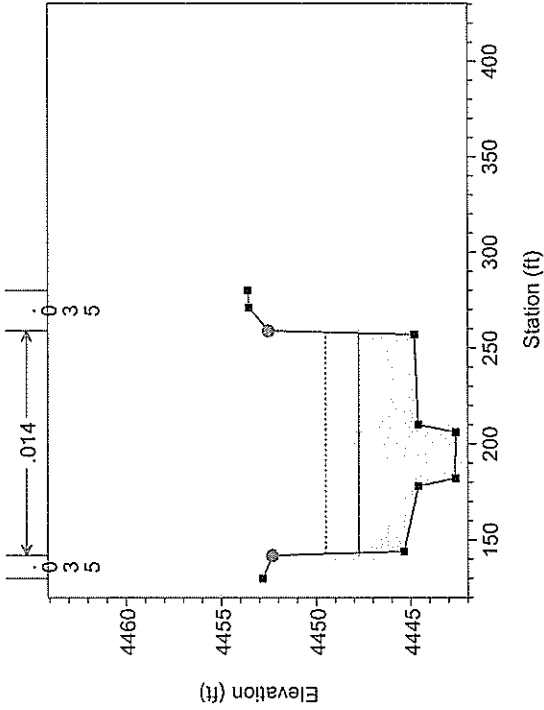
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 87.55



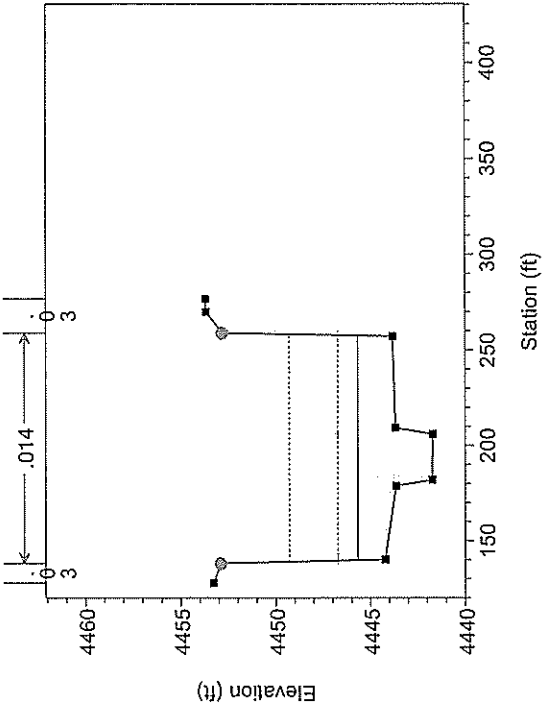
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 87.3



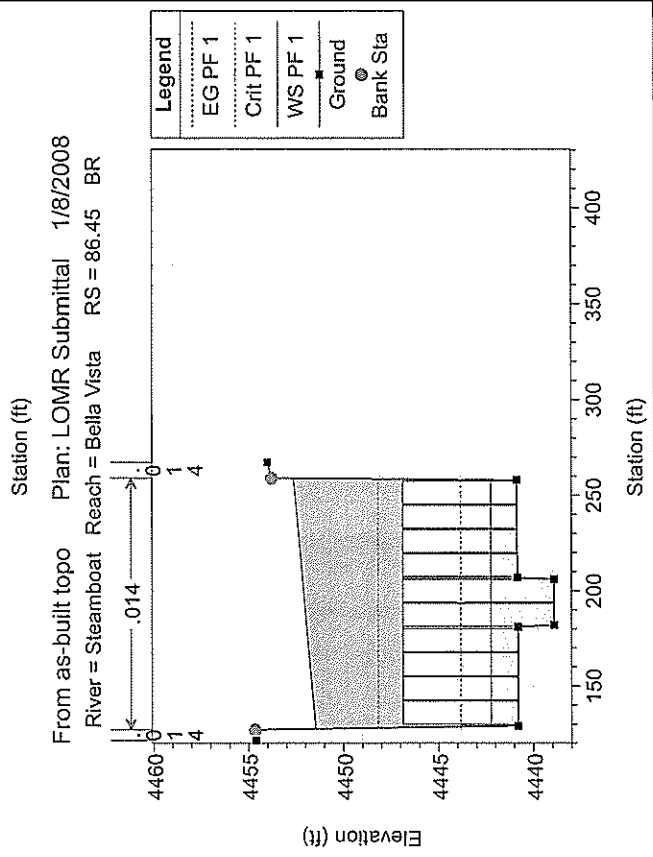
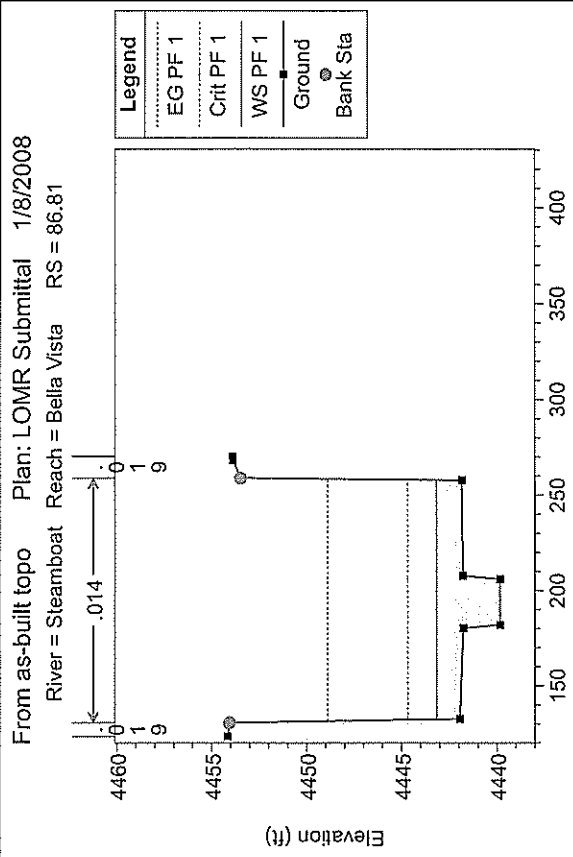
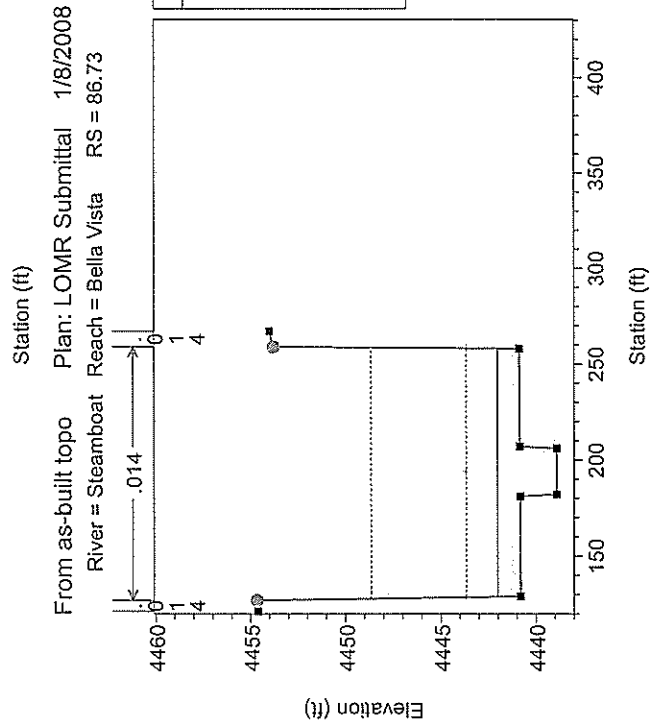
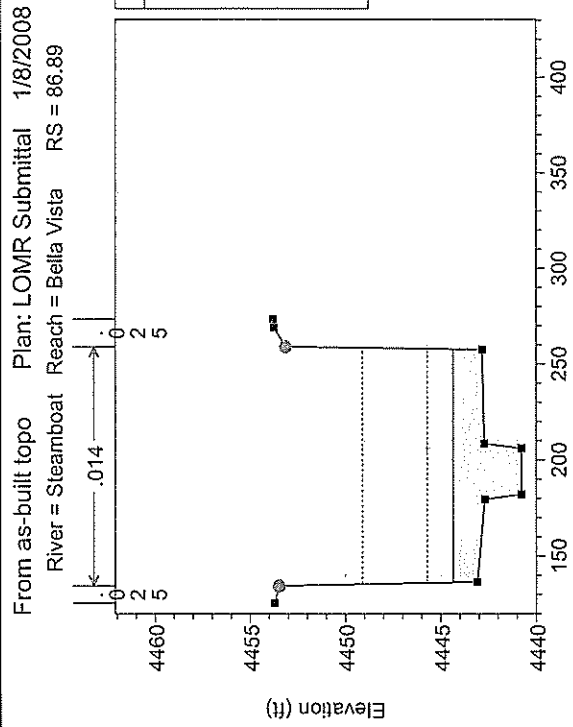
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 87.05



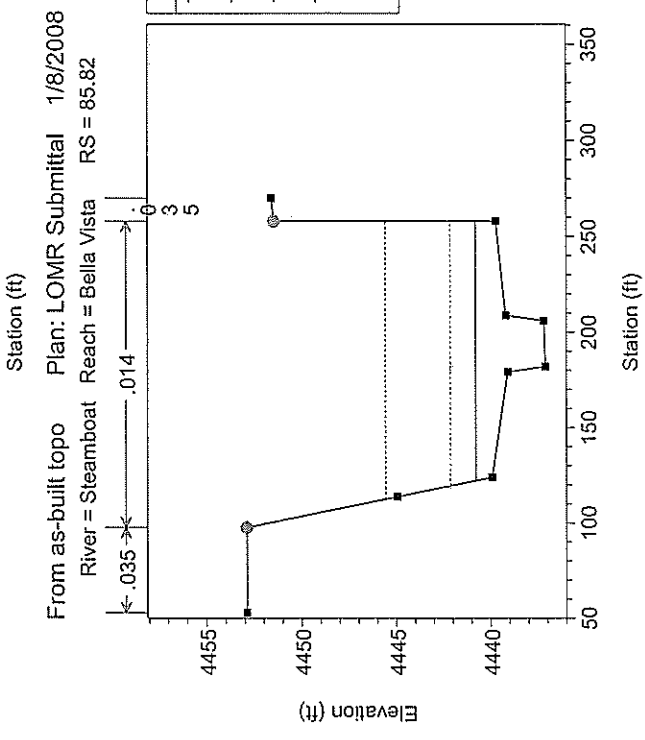
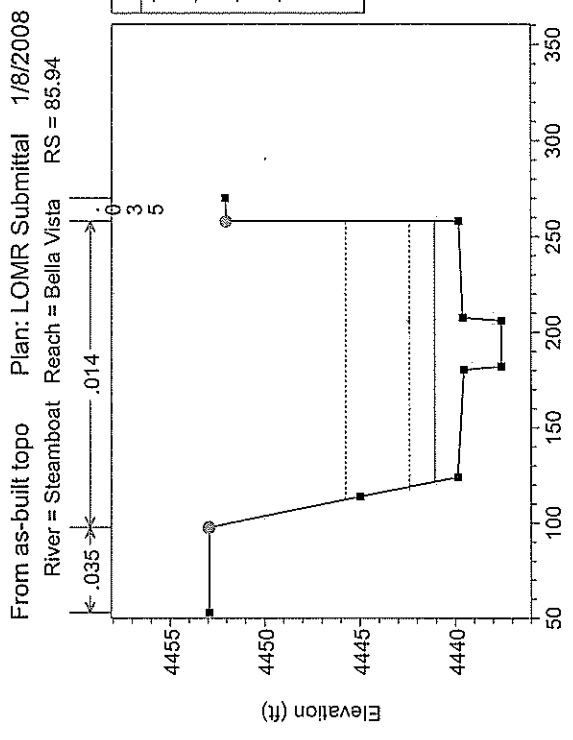
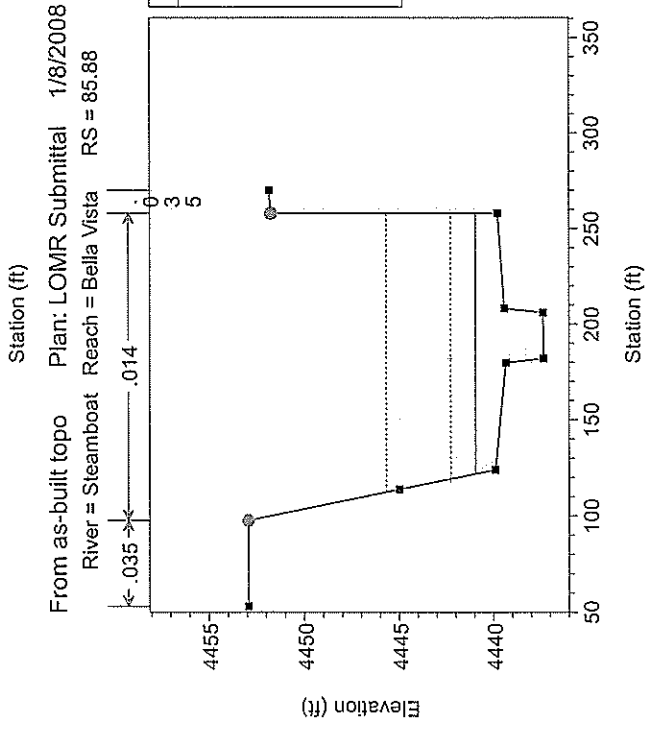
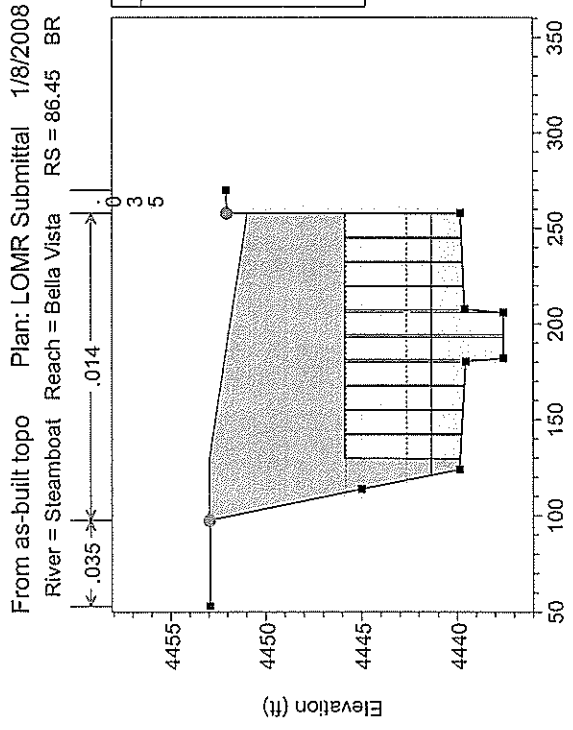
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 86.97



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

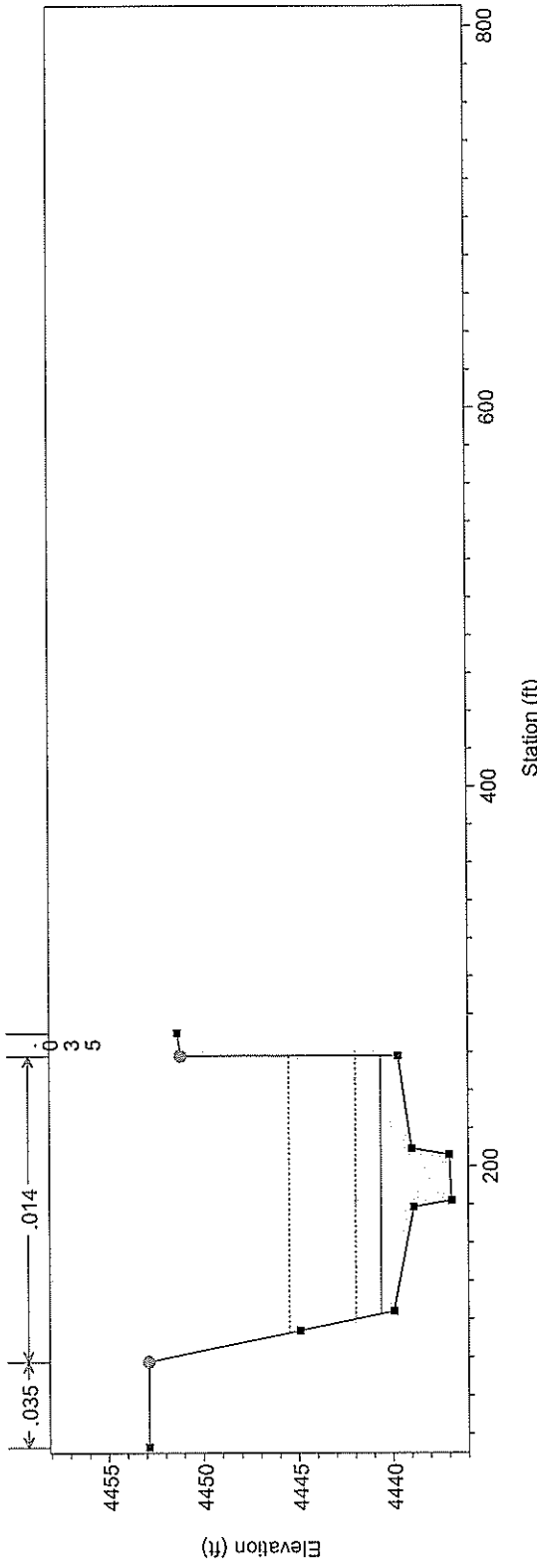


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

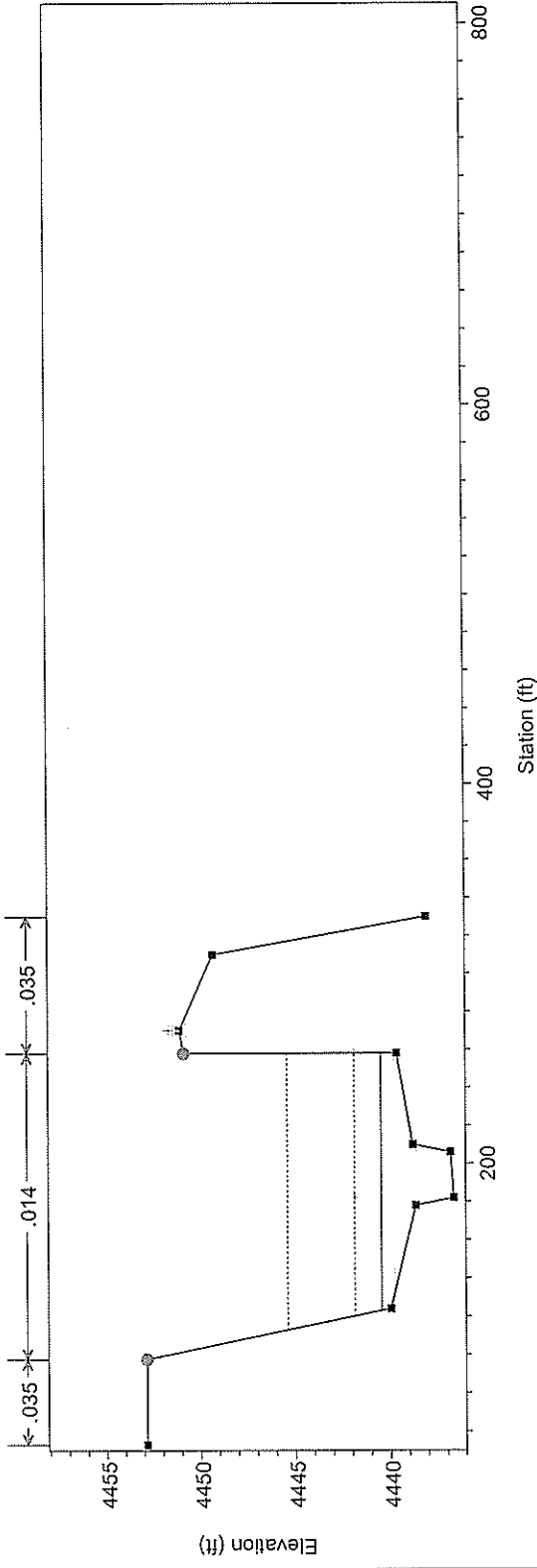


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 85.76



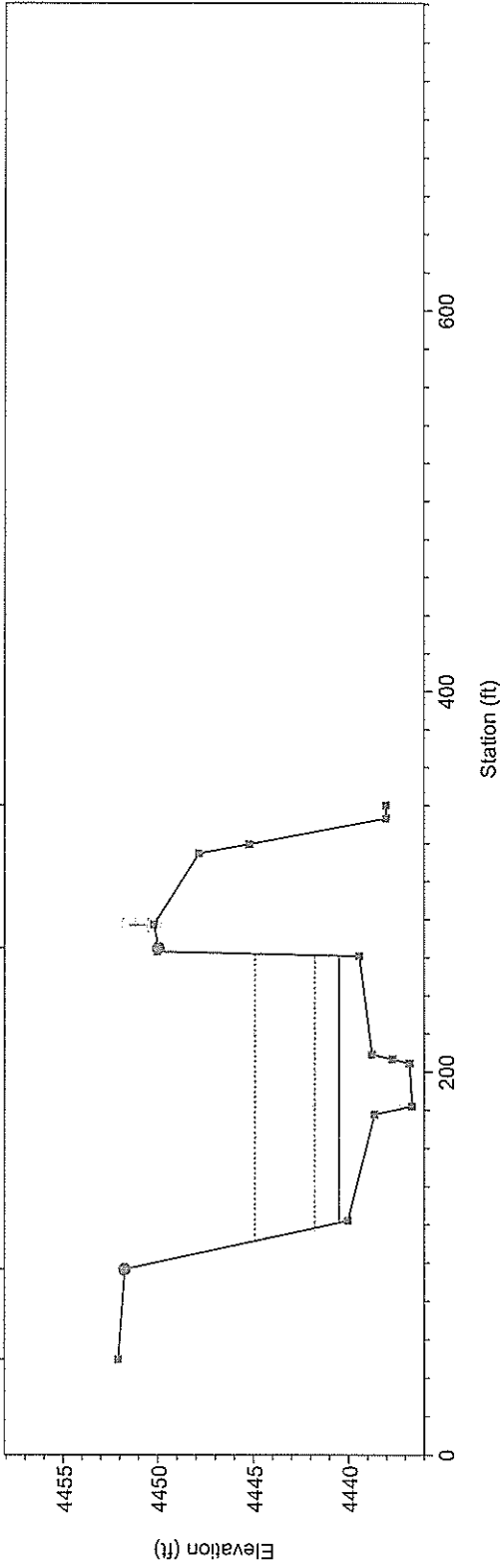
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 85.7



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

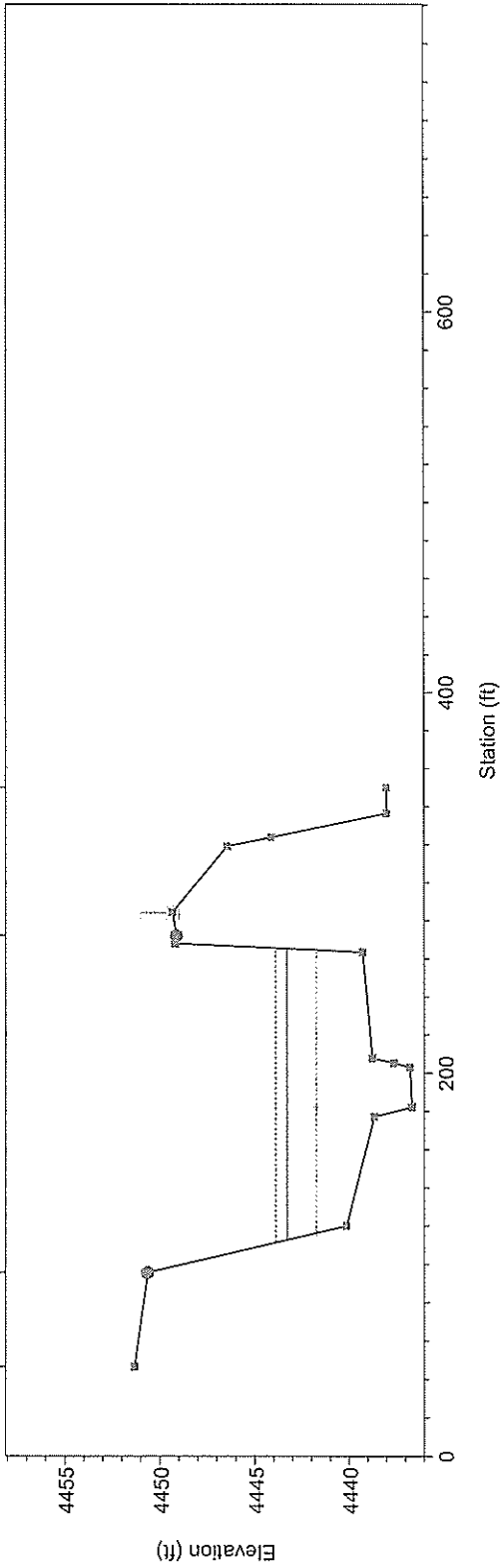
Plan: LOMR Submittal 1/8/2008
 Reach = Bella Vista RS = 85.6*

From as-built topo
 River = Steamboat



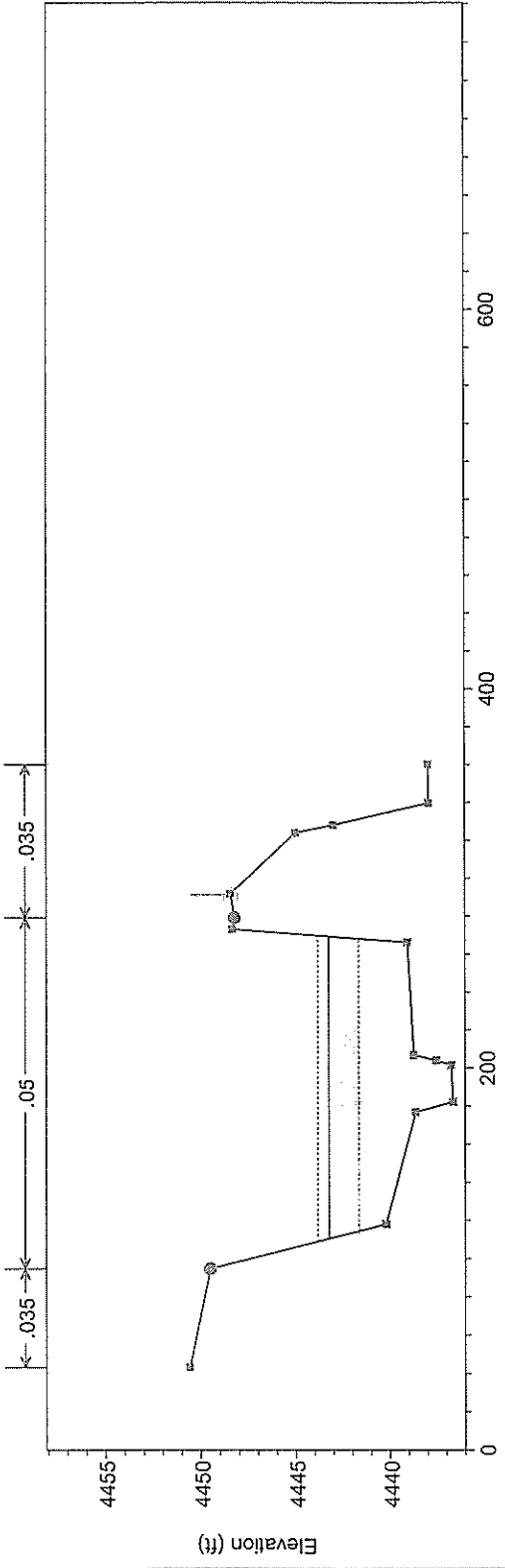
Plan: LOMR Submittal 1/8/2008
 Reach = Bella Vista RS = 85.5*

From as-built topo
 River = Steamboat

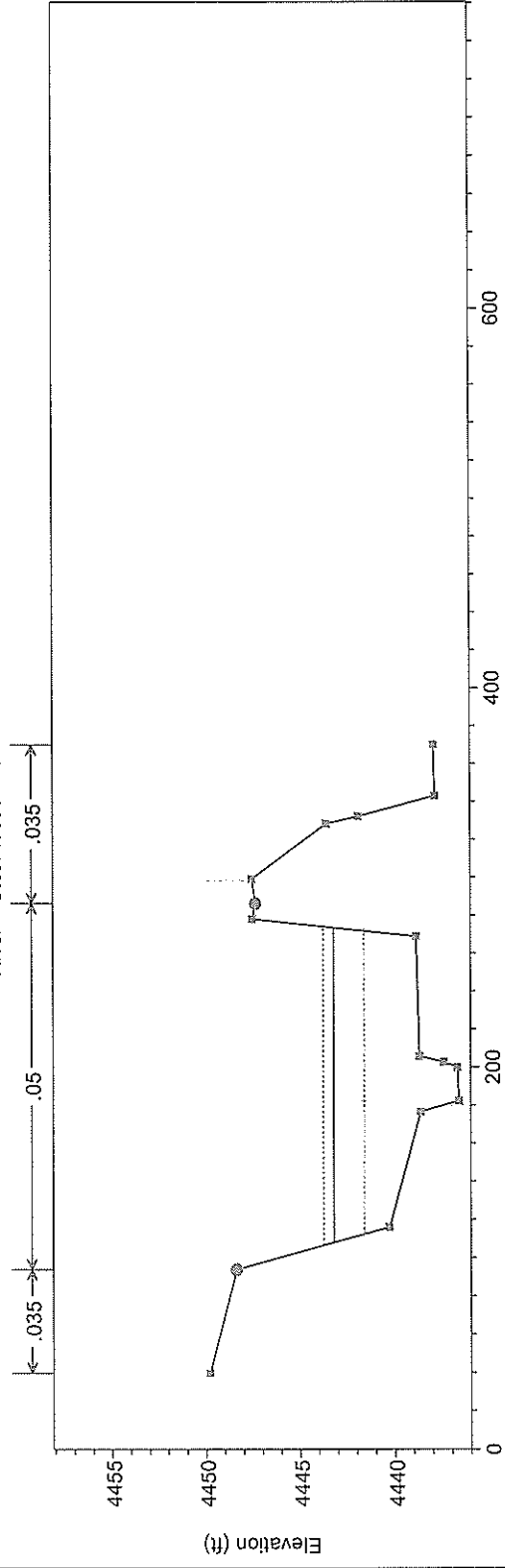


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 85.4*



From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 85.3*

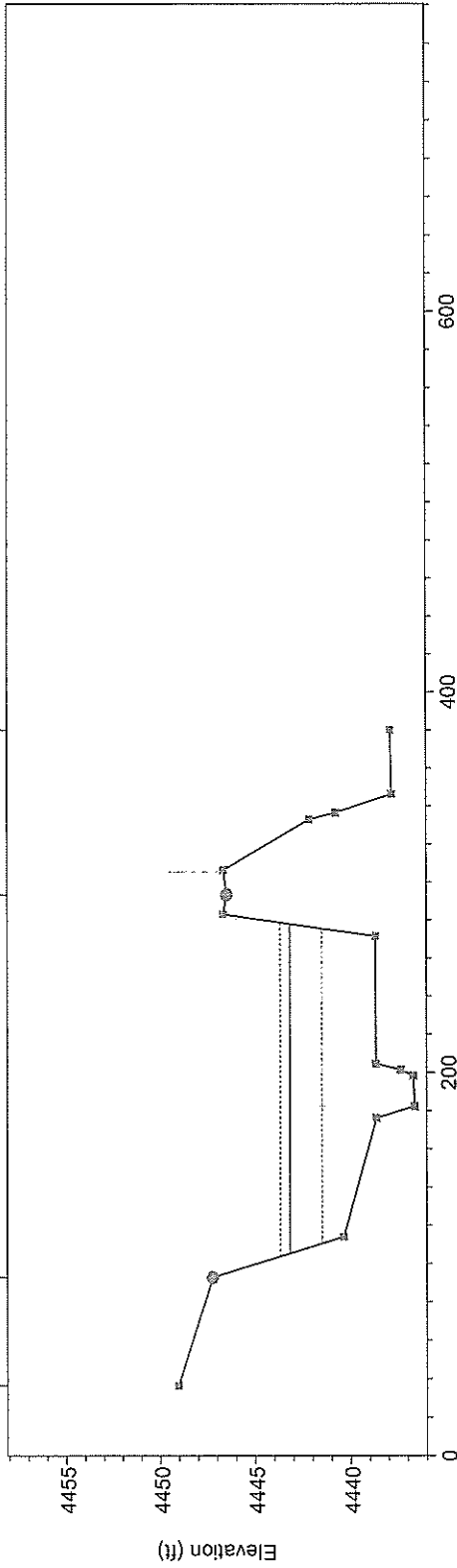


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 85.2*

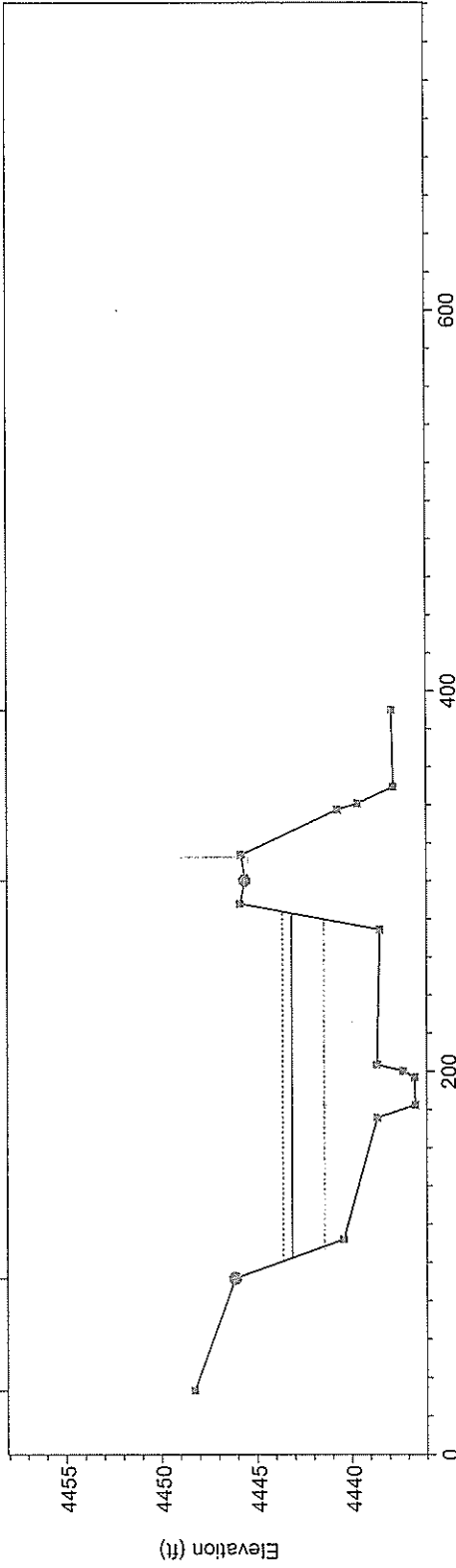
← .035 → ← .05 → ← .035 →



From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 85.1*

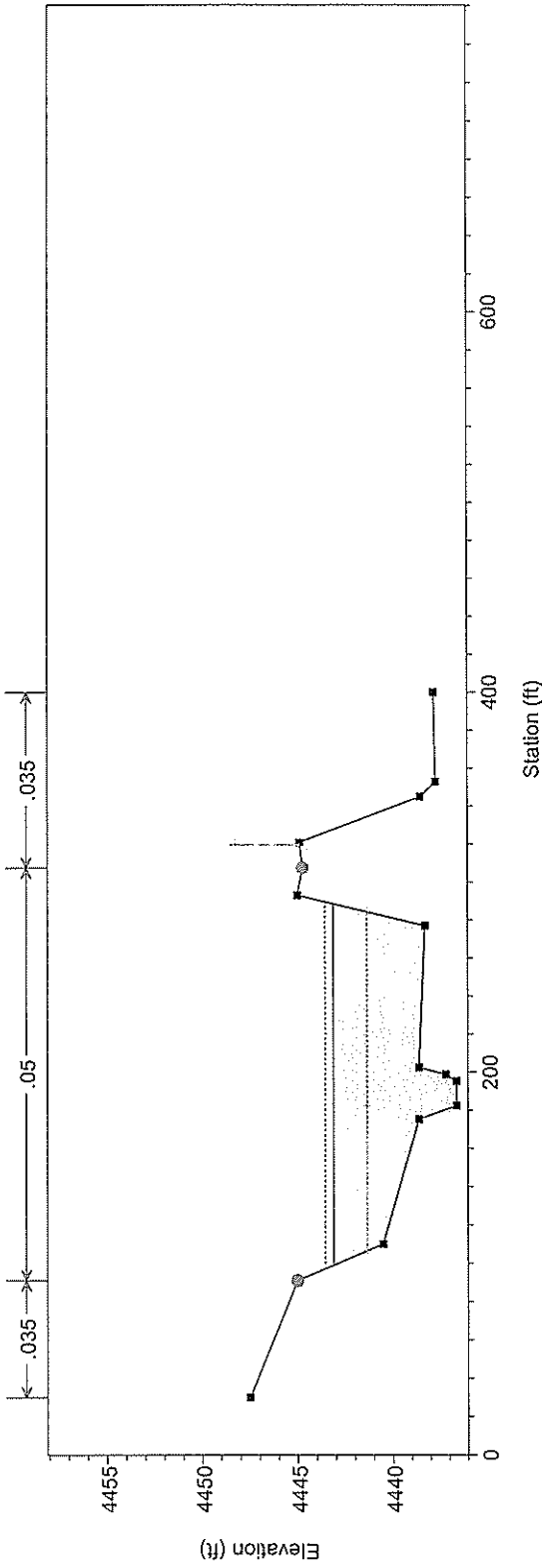
← .035 → ← .05 → ← .035 →



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 85

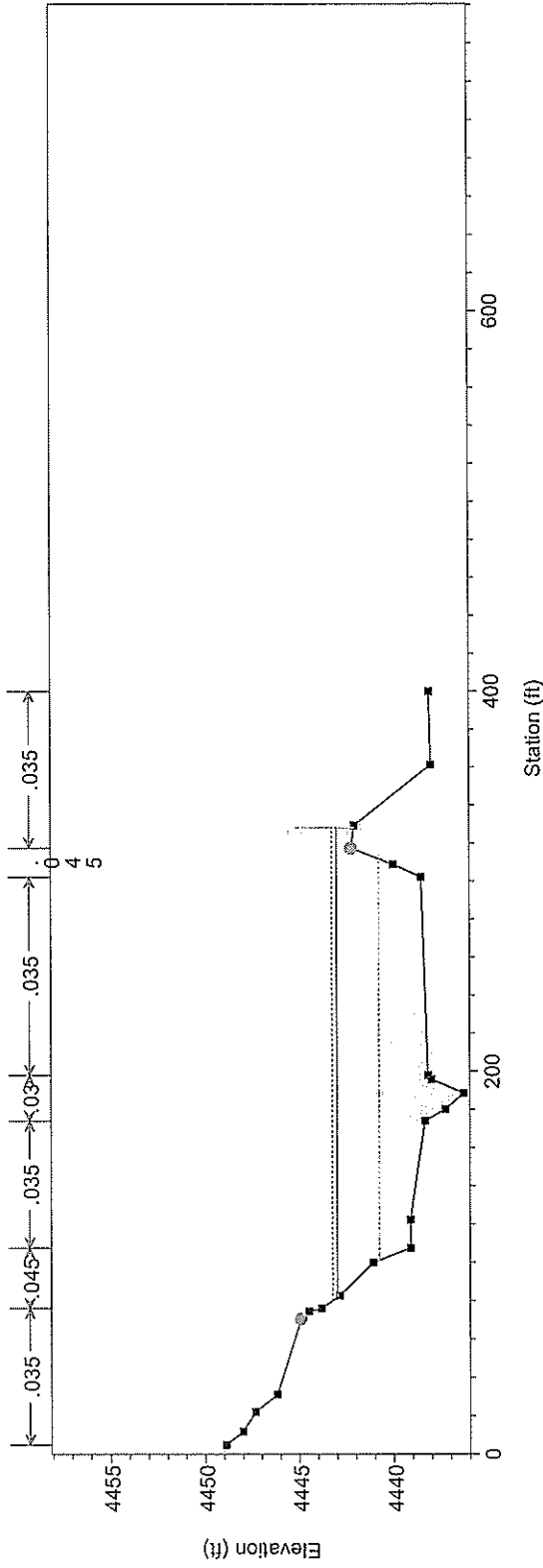


Legend

EG PF 1
WS PF 1
Crit PF 1
Ground
Levee
Bank Sta

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 84



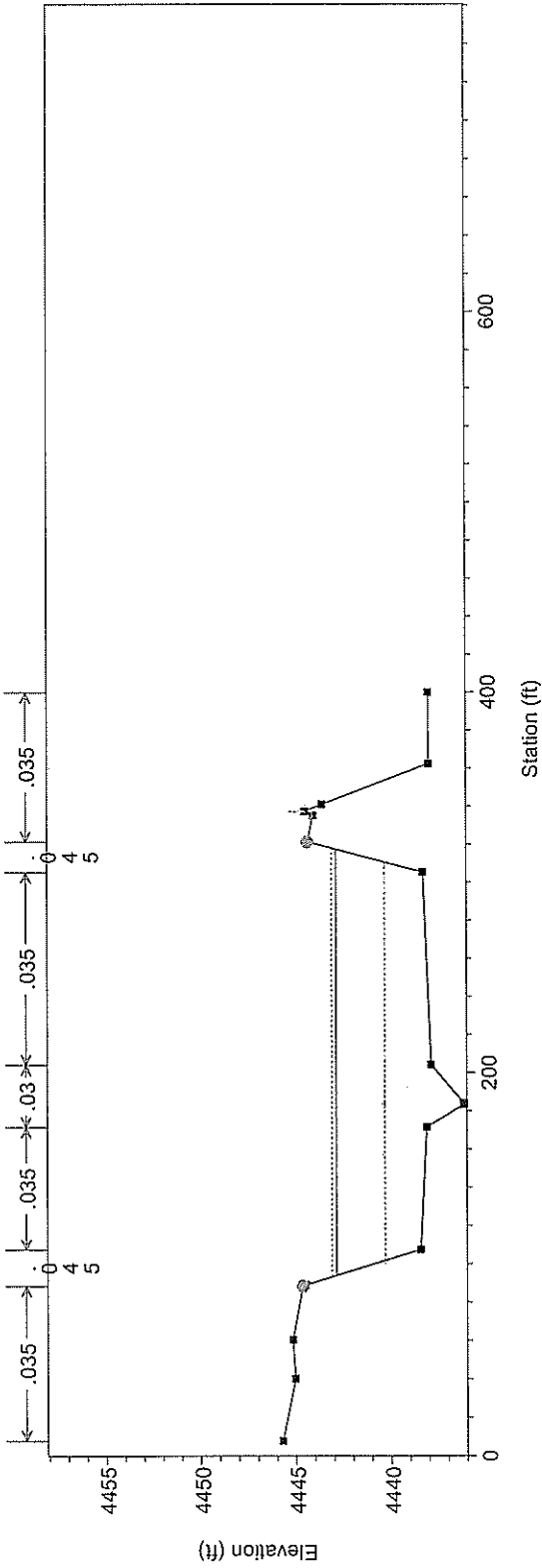
Legend

EG PF 1
WS PF 1
Crit PF 1
Ground
Levee
Bank Sta

1 in Horiz. = 100 ft 1 in Vert. = 10 ft

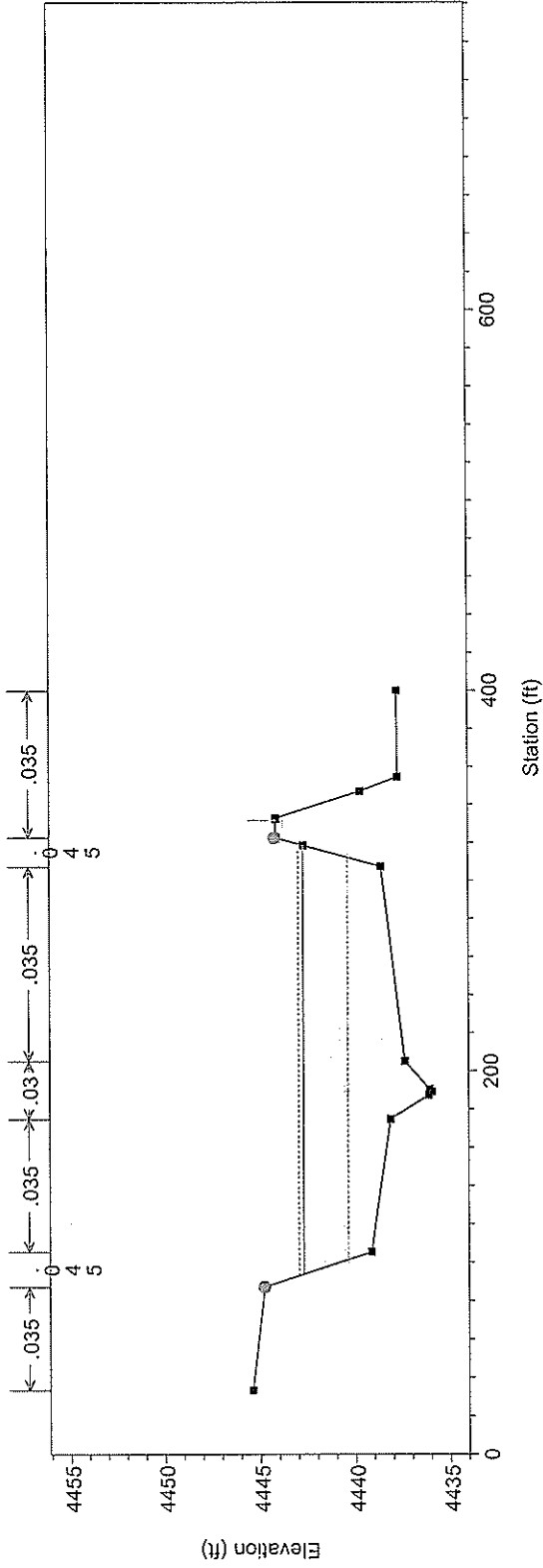
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 83



From as-built topo Plan: LOMR Submittal 1/8/2008

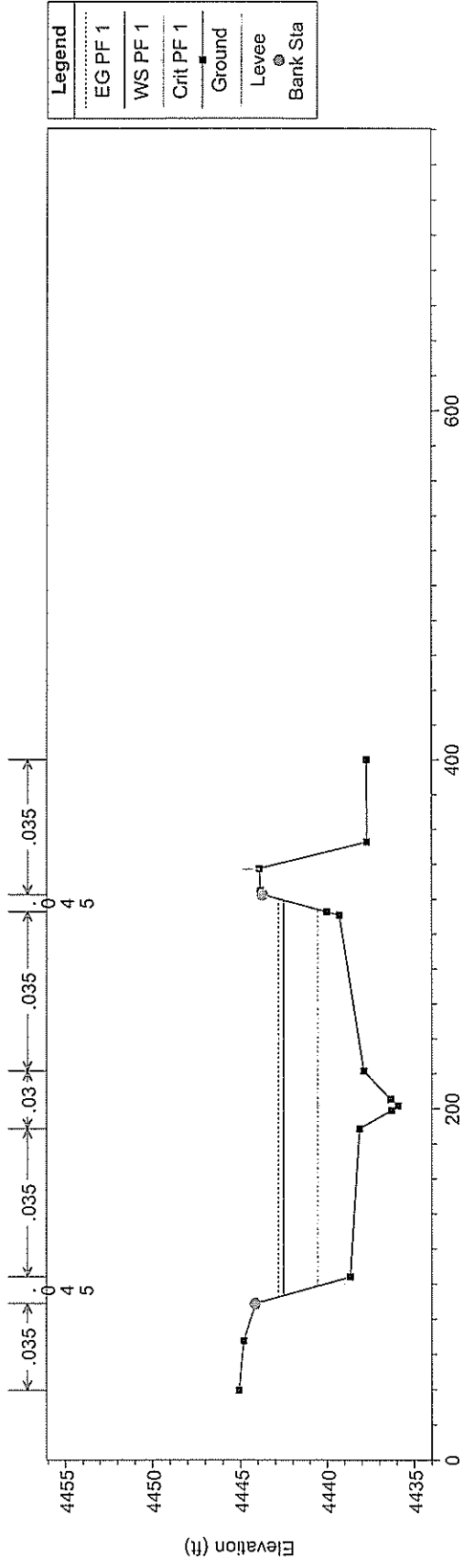
River = Steamboat Reach = Bella Vista RS = 82



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

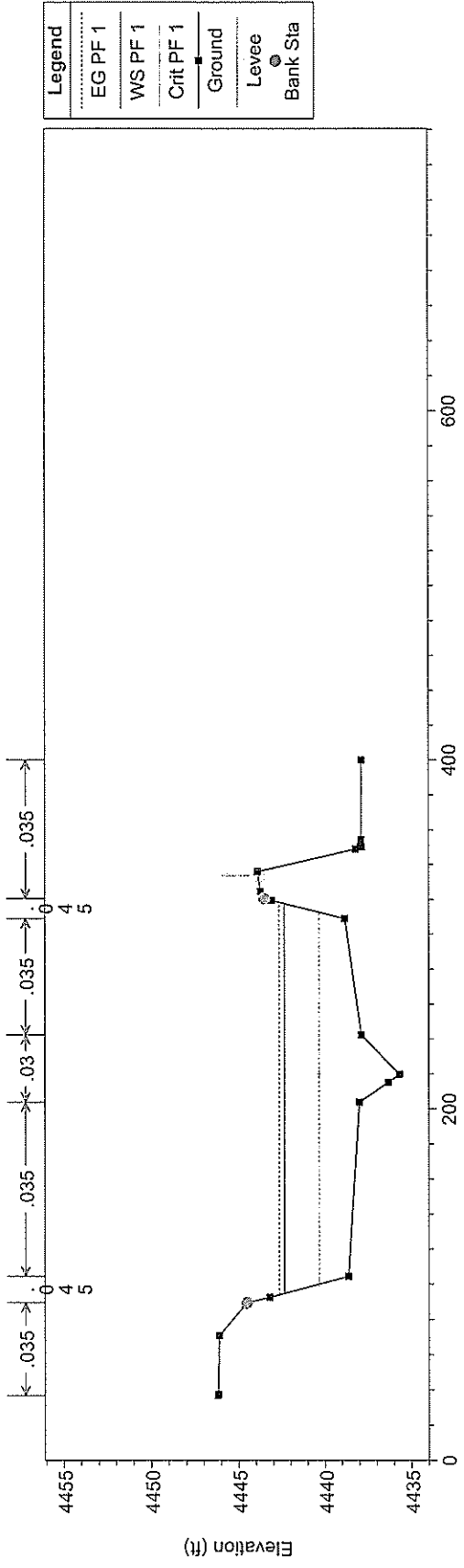
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 81



From as-built topo Plan: LOMR Submittal 1/8/2008

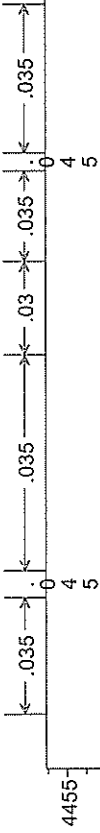
River = Steamboat Reach = Bella Vista RS = 80



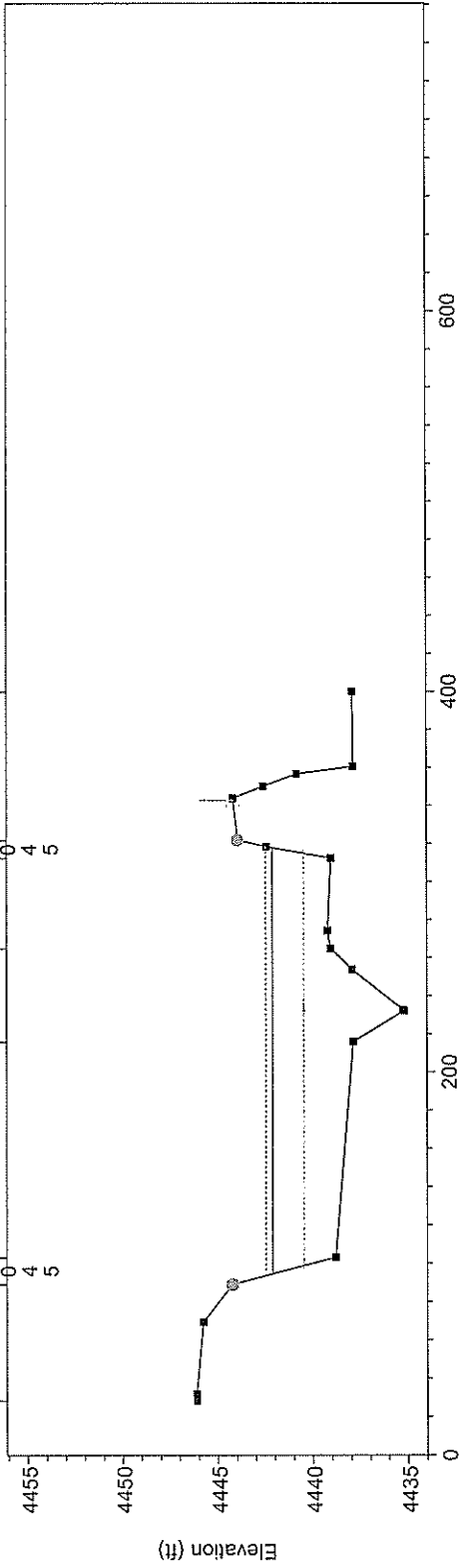
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 79

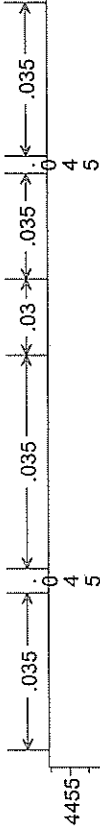


Legend	
---	EG PF 1
---	WS PF 1
---	Crit PF 1
—	Ground
—	Levee
●	Bank Sta

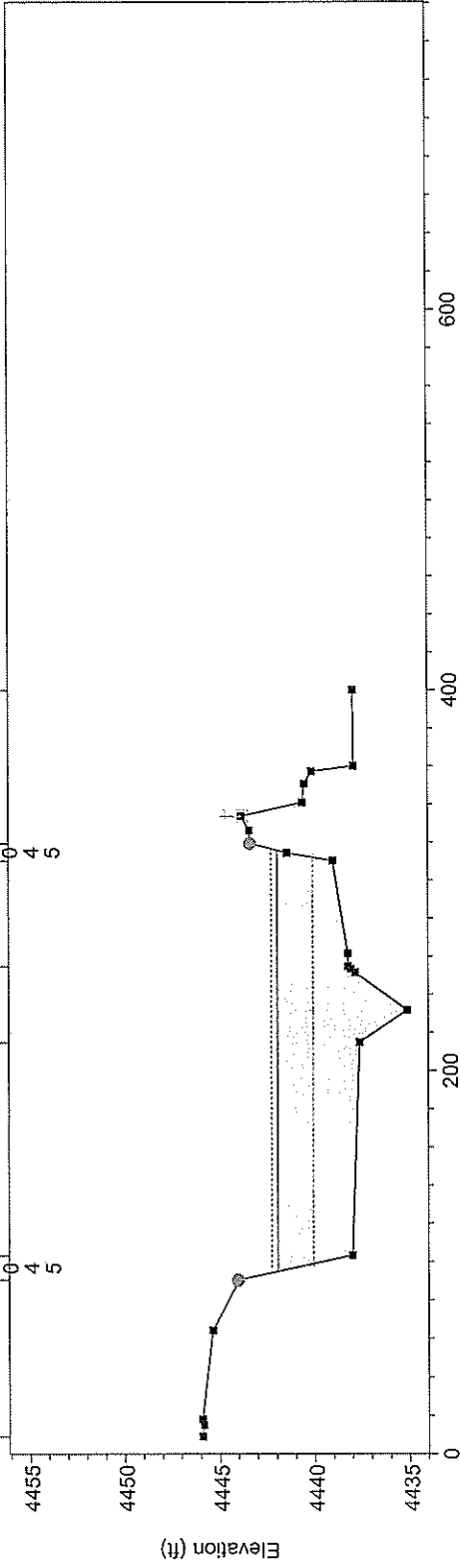


From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 78



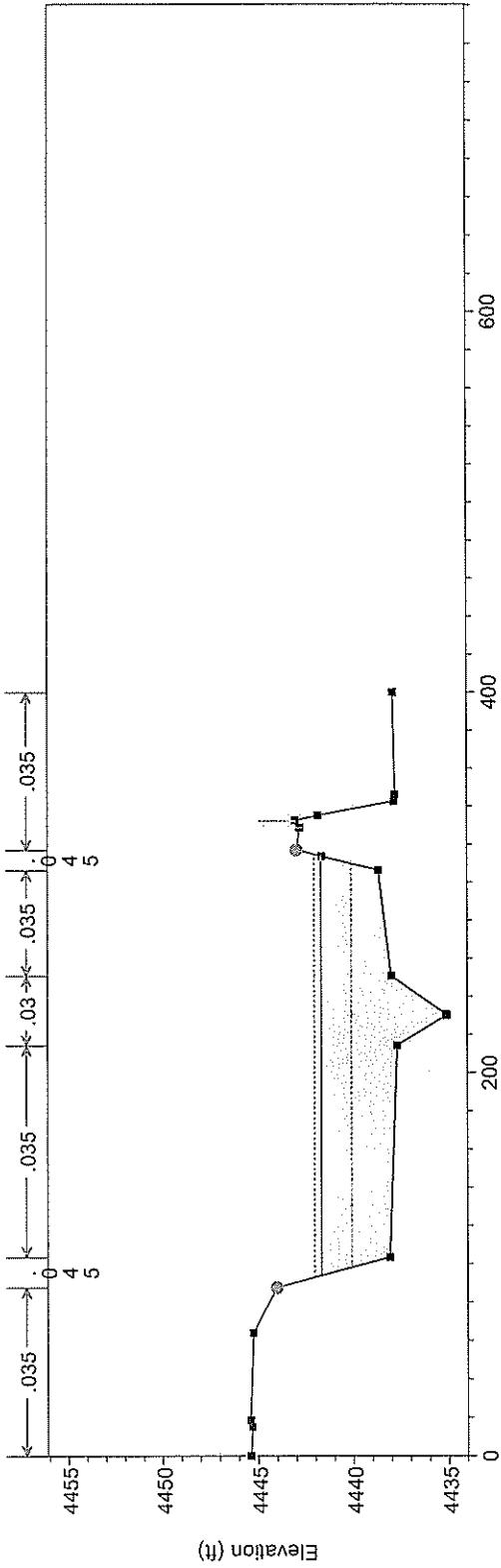
Legend	
---	EG PF 1
---	WS PF 1
---	Crit PF 1
—	Ground
—	Levee
●	Bank Sta



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

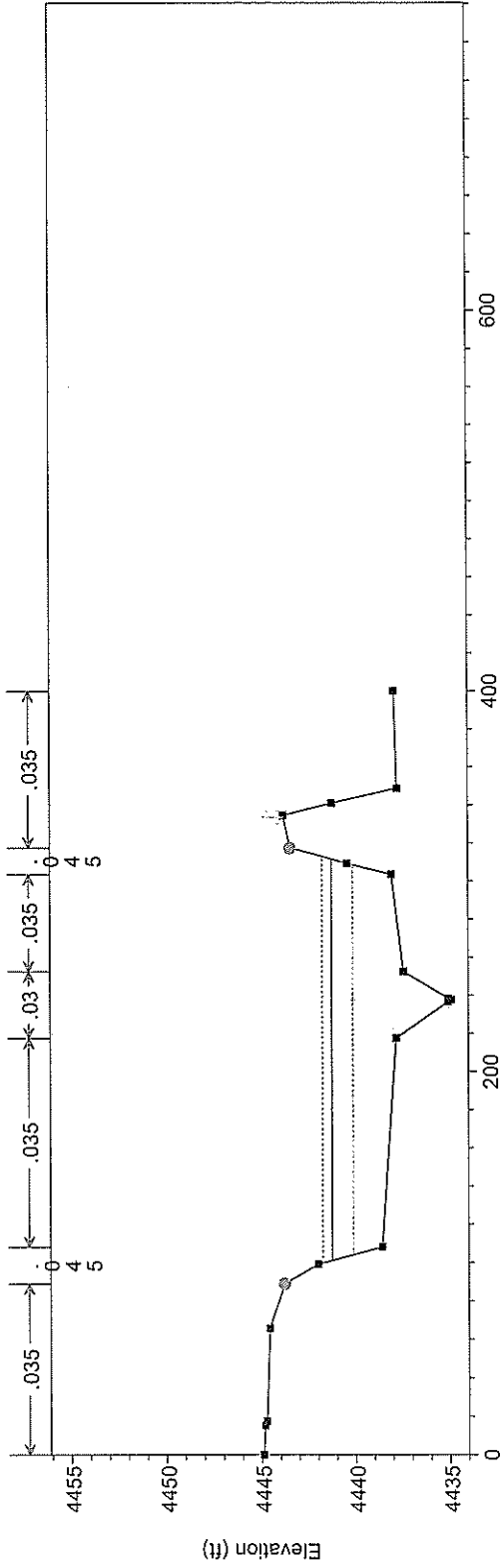
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 77



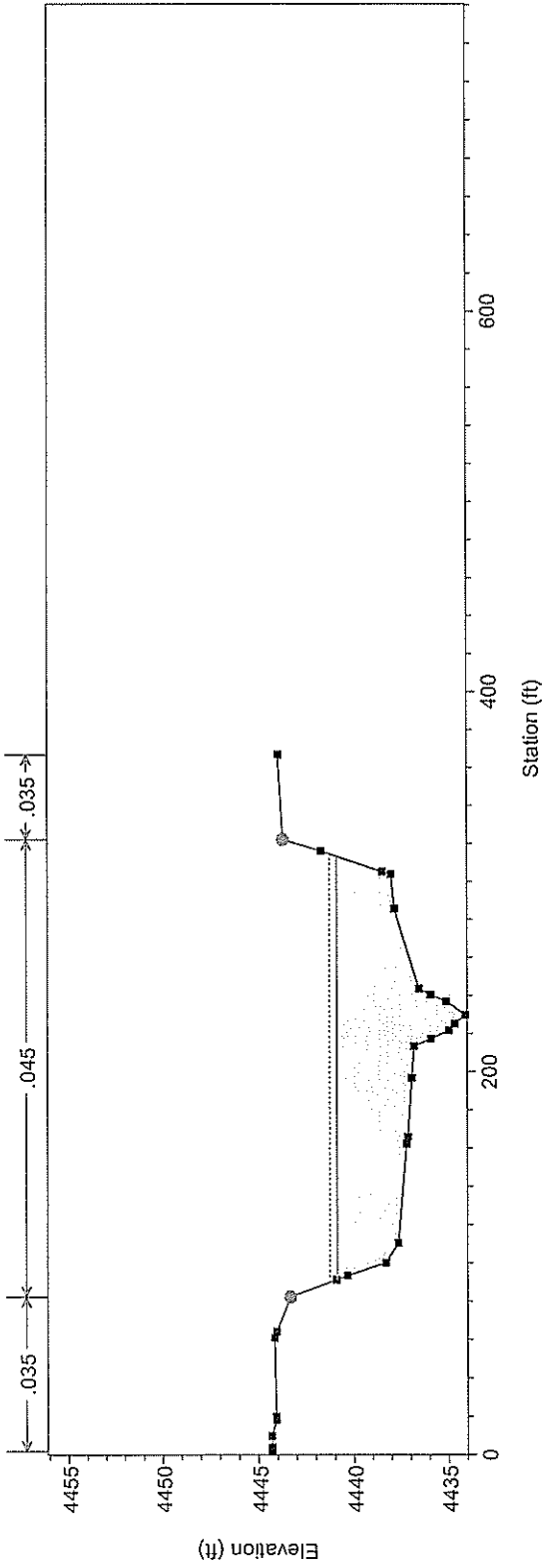
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 76

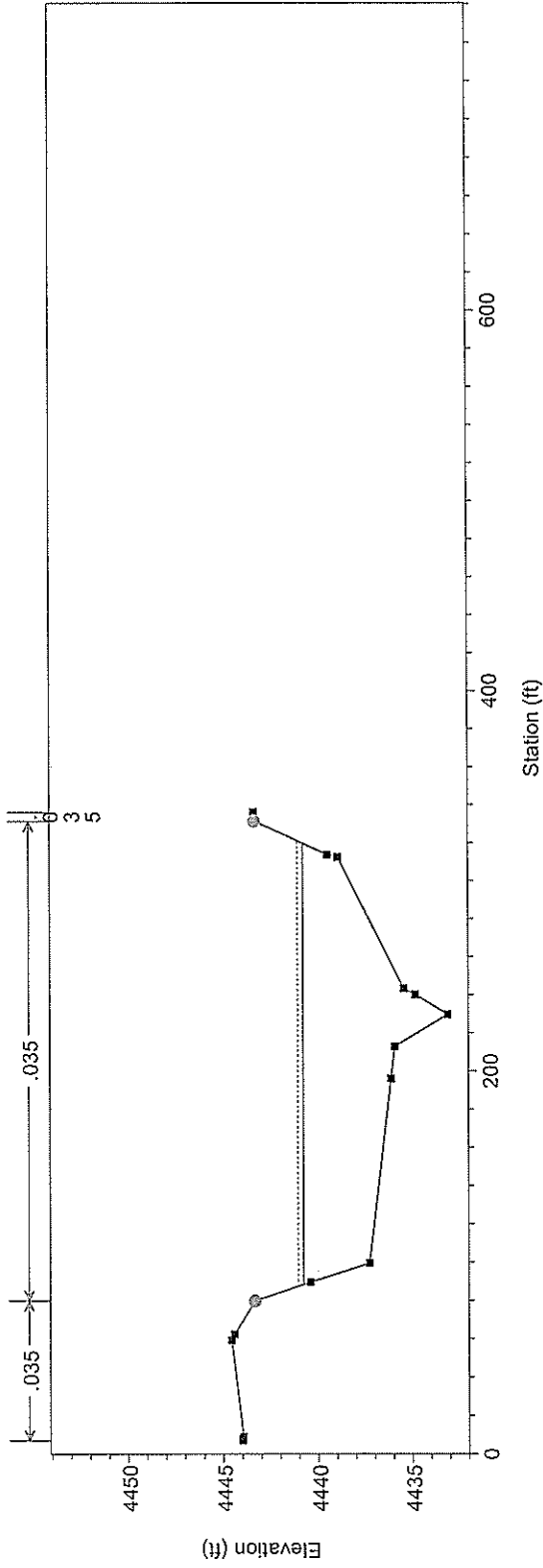


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 74.75

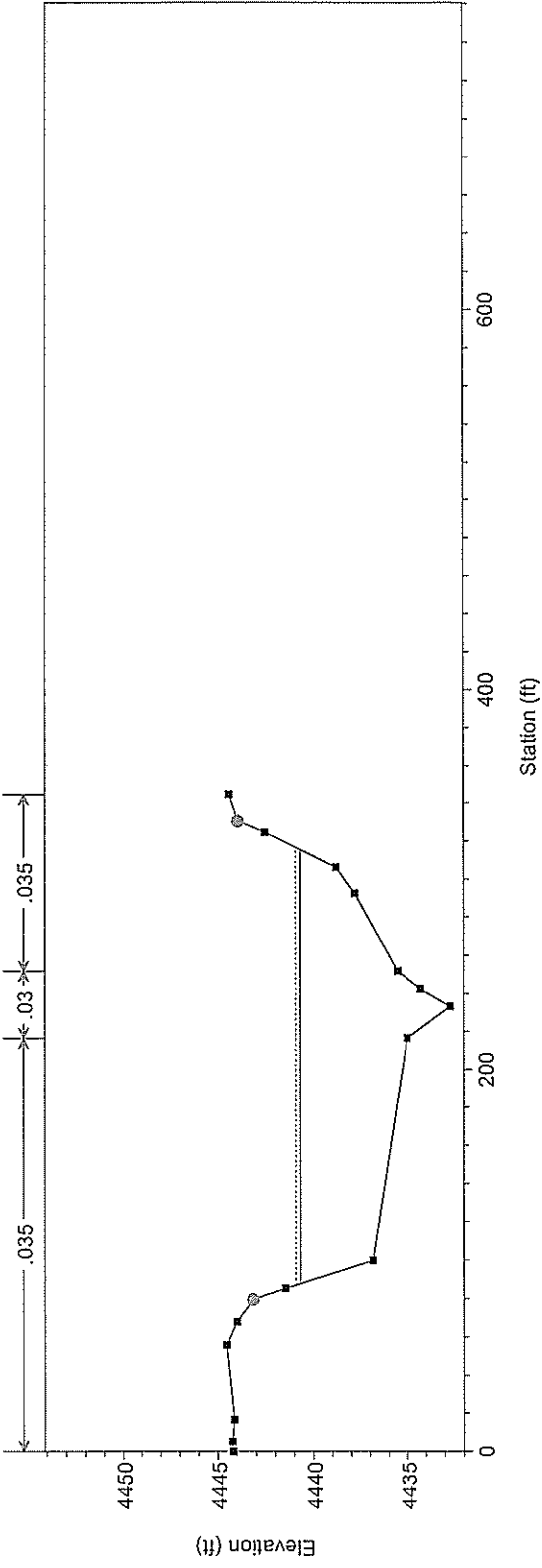


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 74

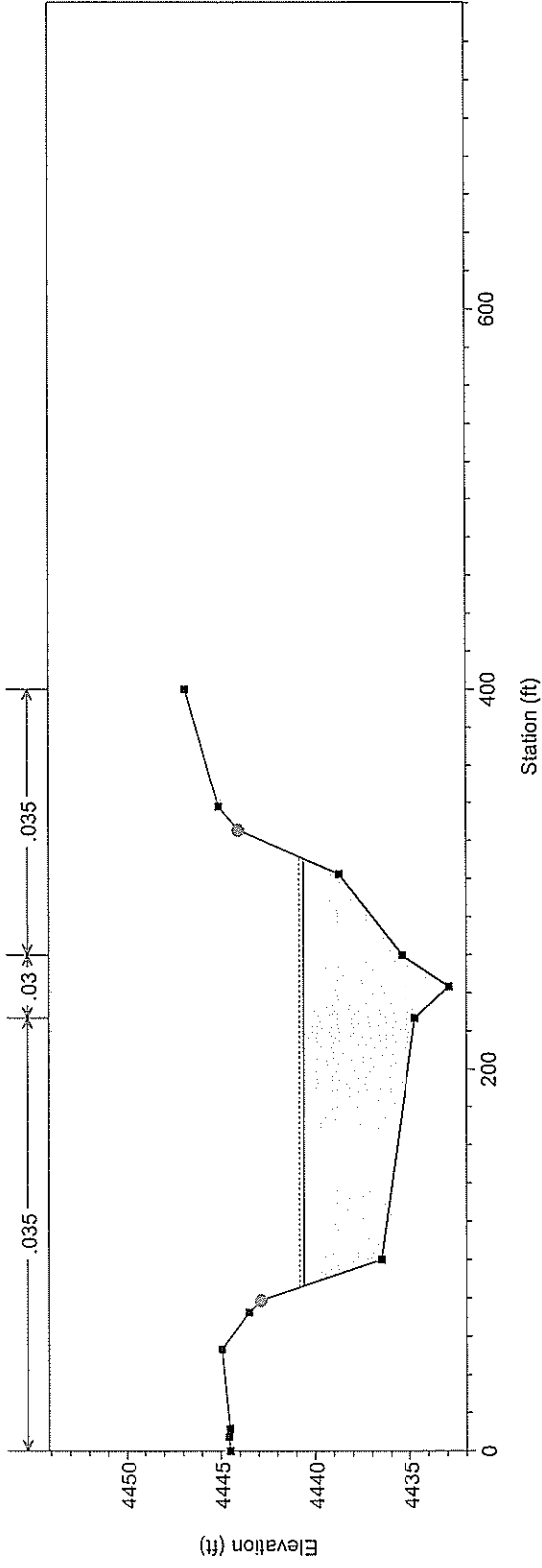


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 73

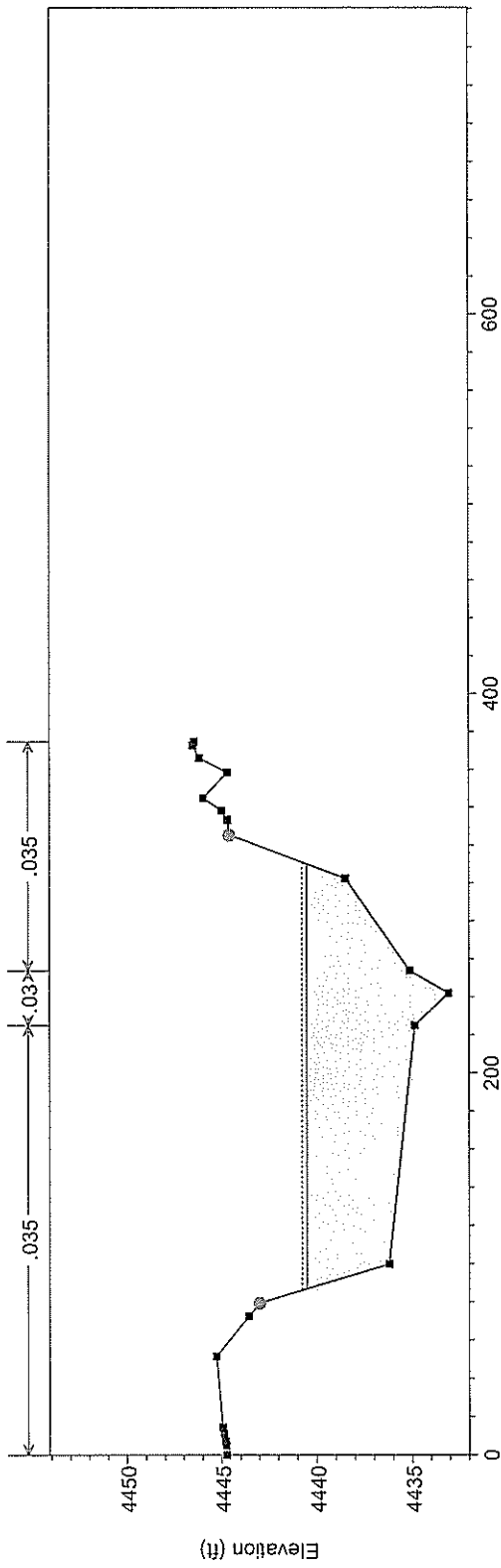


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 72

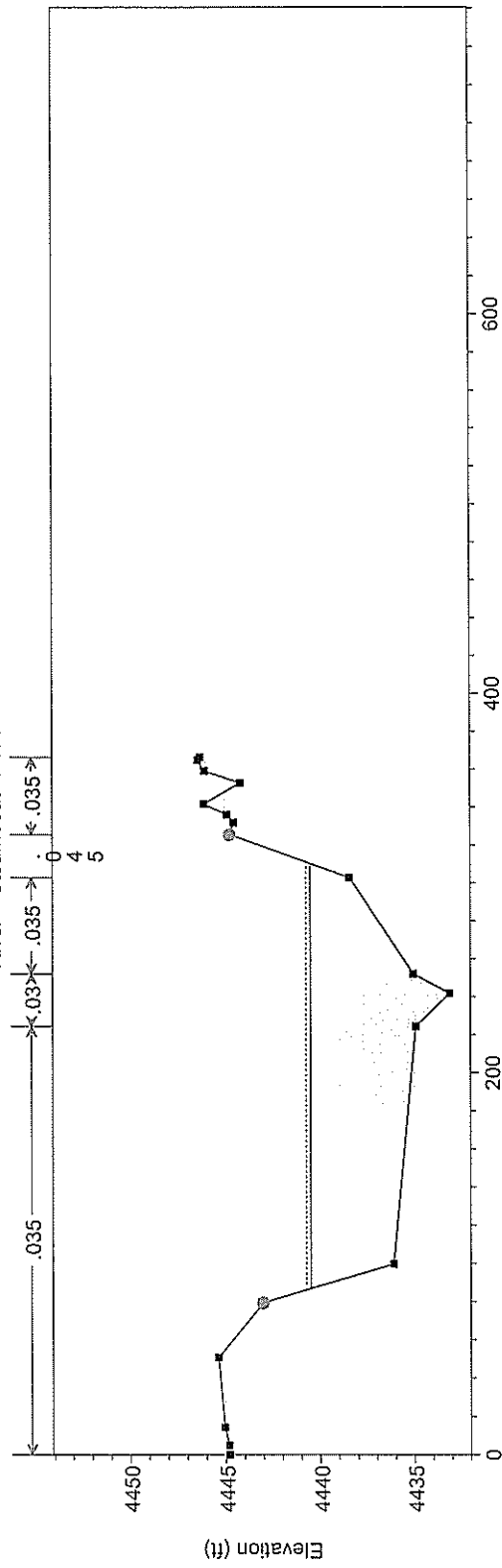


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 71.25

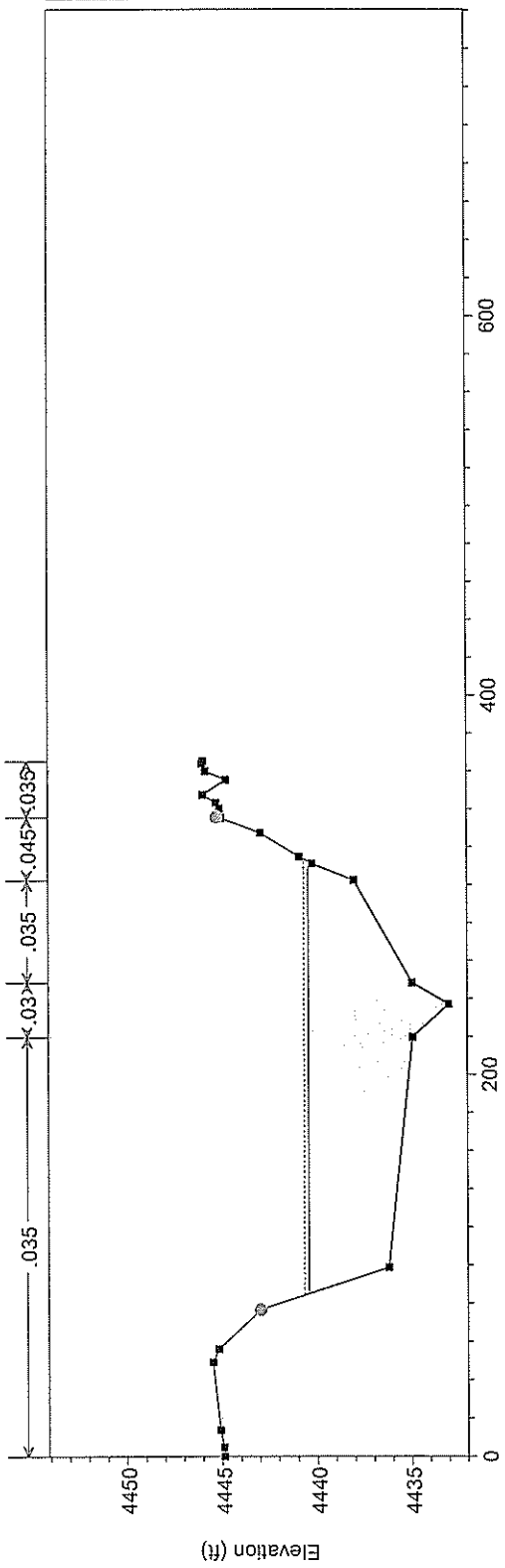


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 71



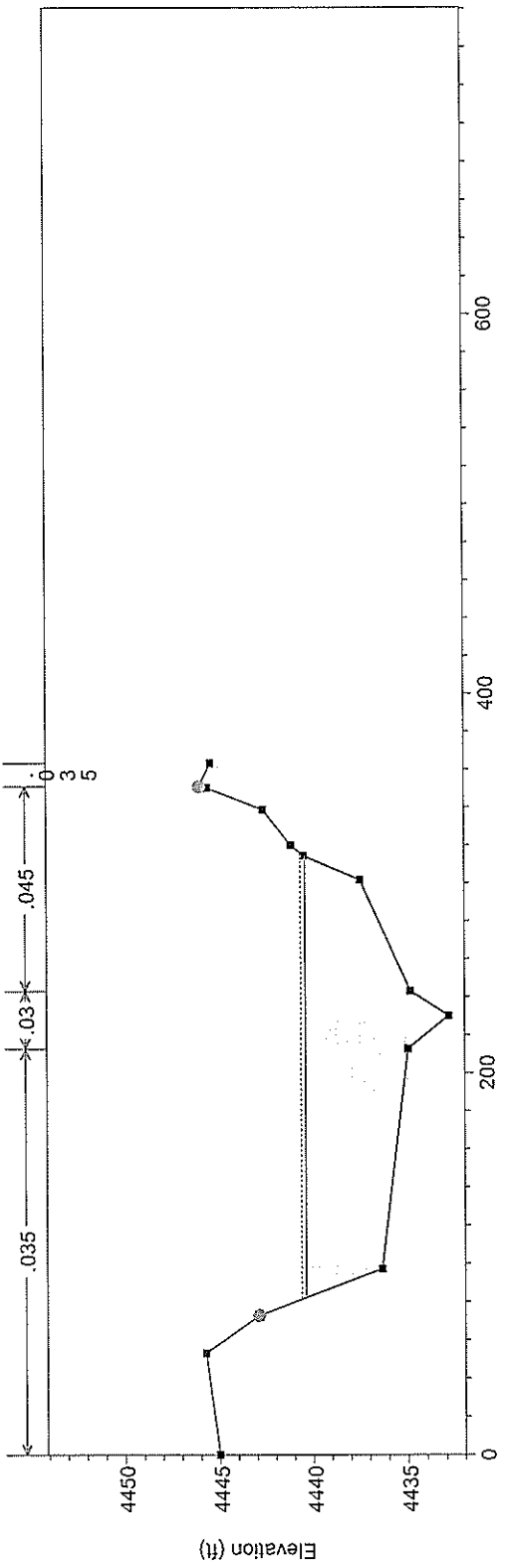
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 70.6



.035
 .03
 .045
 .035

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 70



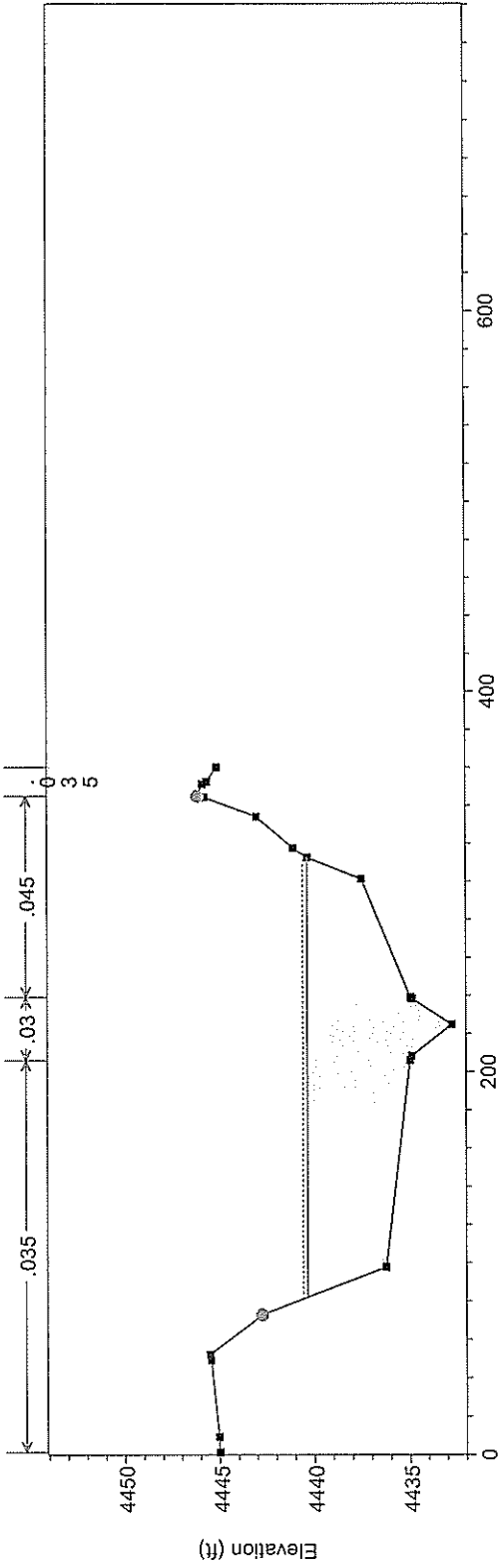
.035
 .03
 .045
 0
 3
 5

1 in Horiz. = 100 ft 1 in Vert. = 10 ft

Plan: LOMR Submittal 1/8/2008
 Reach = Bella Vista RS = 69.75

From as-built topo

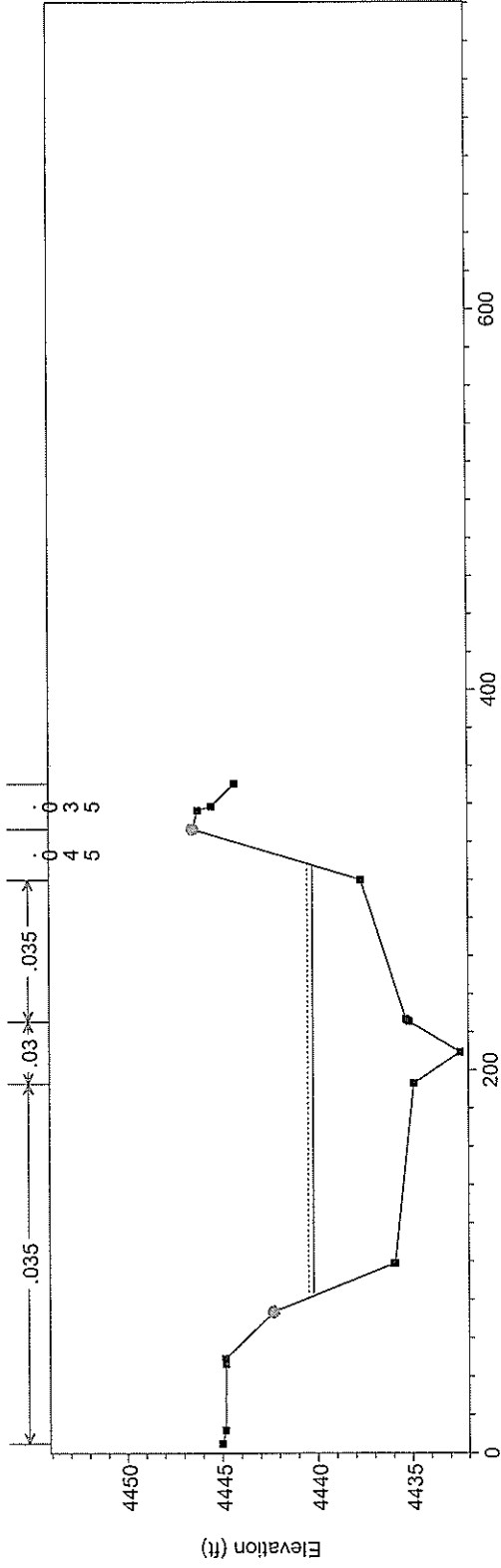
River = Steamboat
 .035
 .03
 .045
 0
 3
 5



Plan: LOMR Submittal 1/8/2008
 Reach = Bella Vista RS = 69

From as-built topo

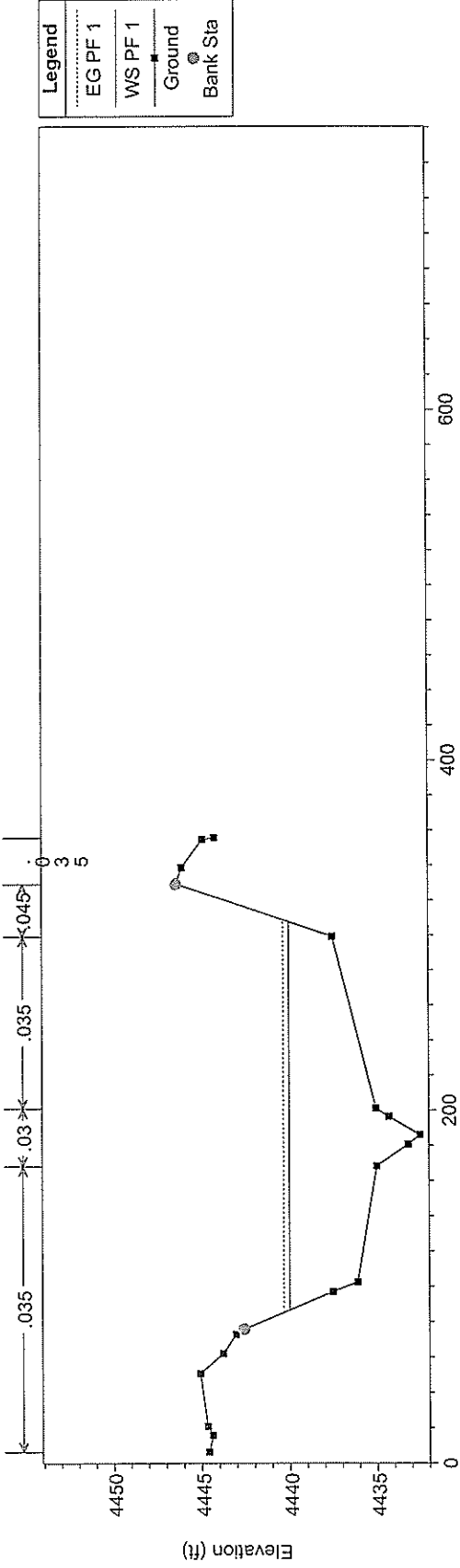
River = Steamboat
 .035
 .03
 .045
 0
 4
 3
 5



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

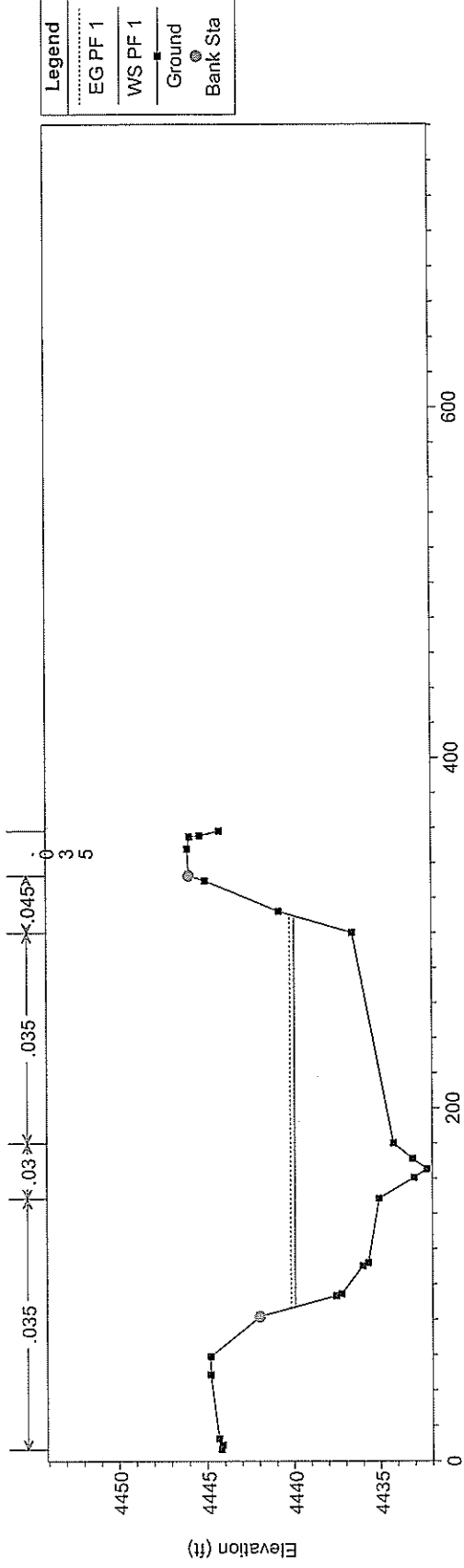
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 68



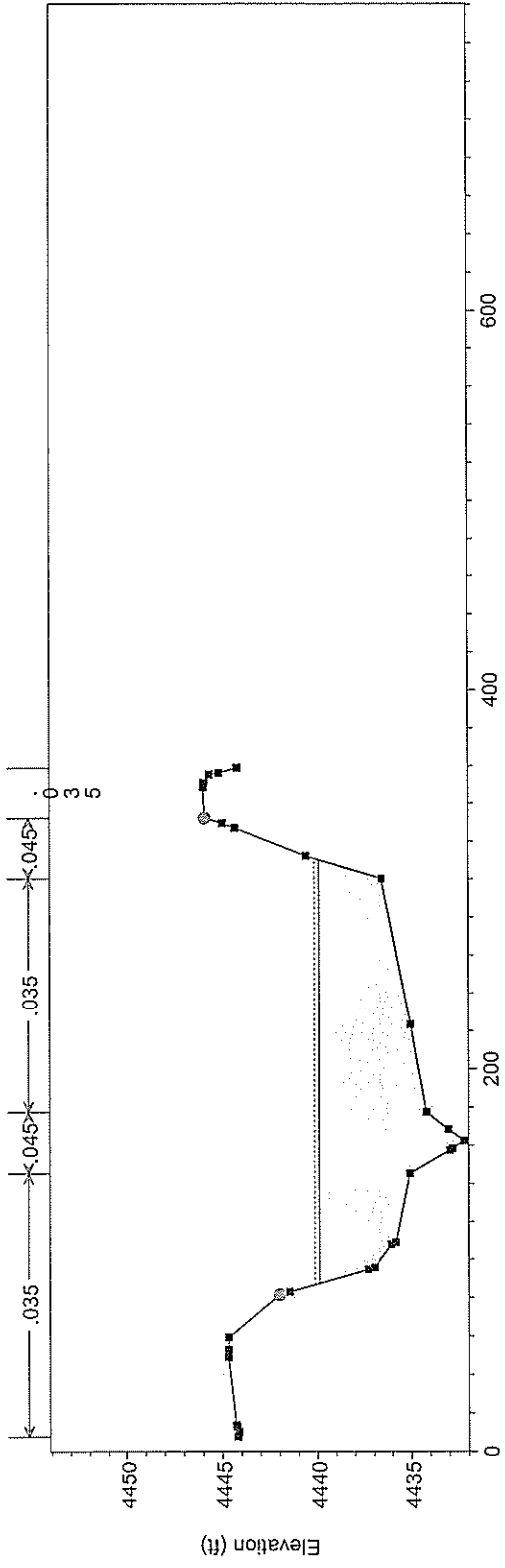
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 67

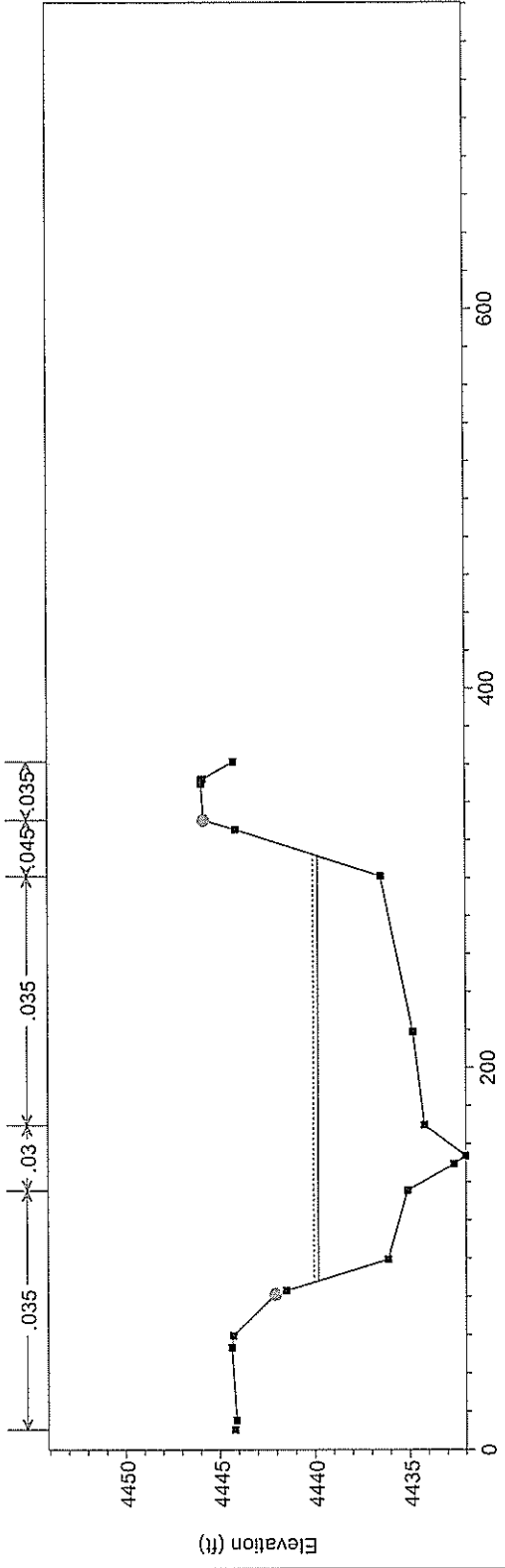


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 66.75

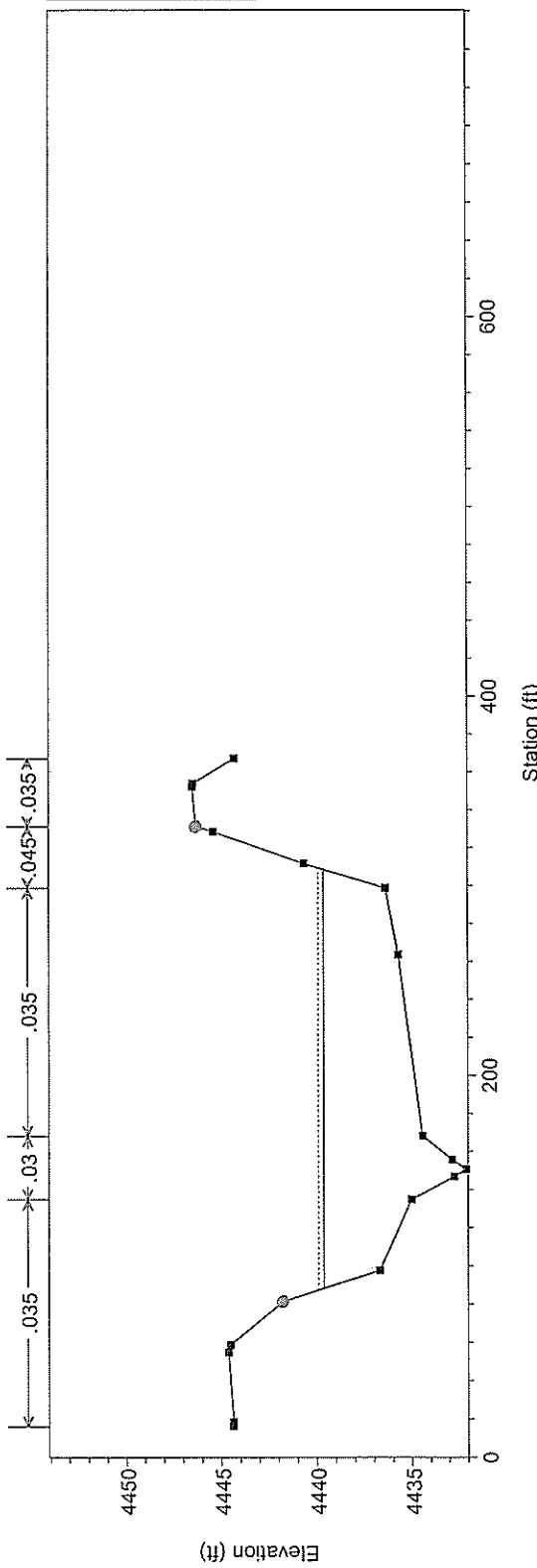


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 66



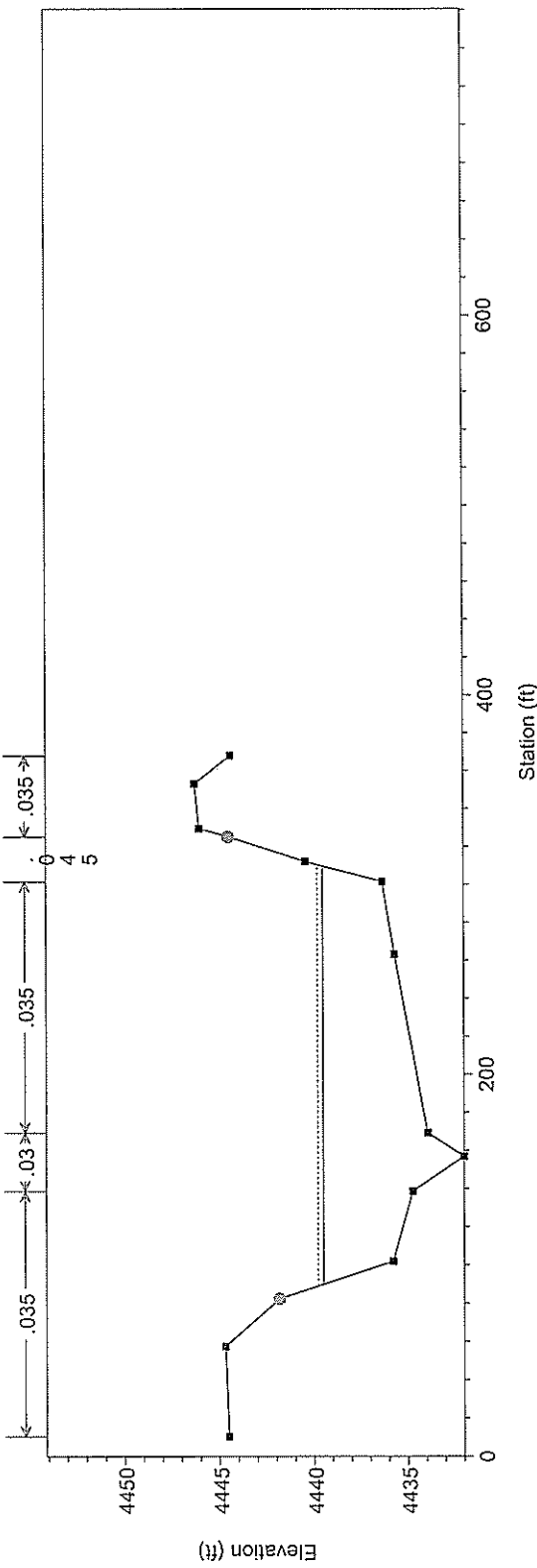
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 65



Legend	
.....	EG PF 1
————	WS PF 1
—●—	Ground
—■—	Bank Sta

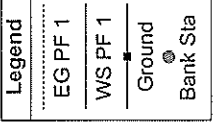
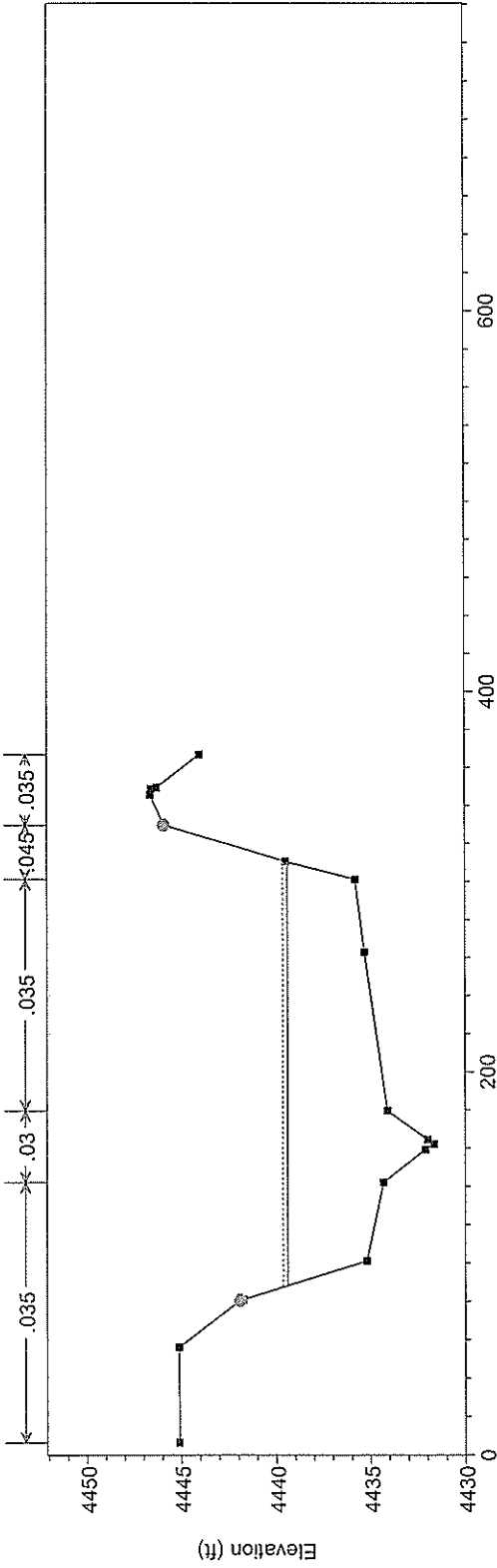
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 64



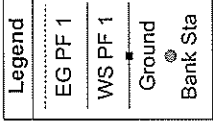
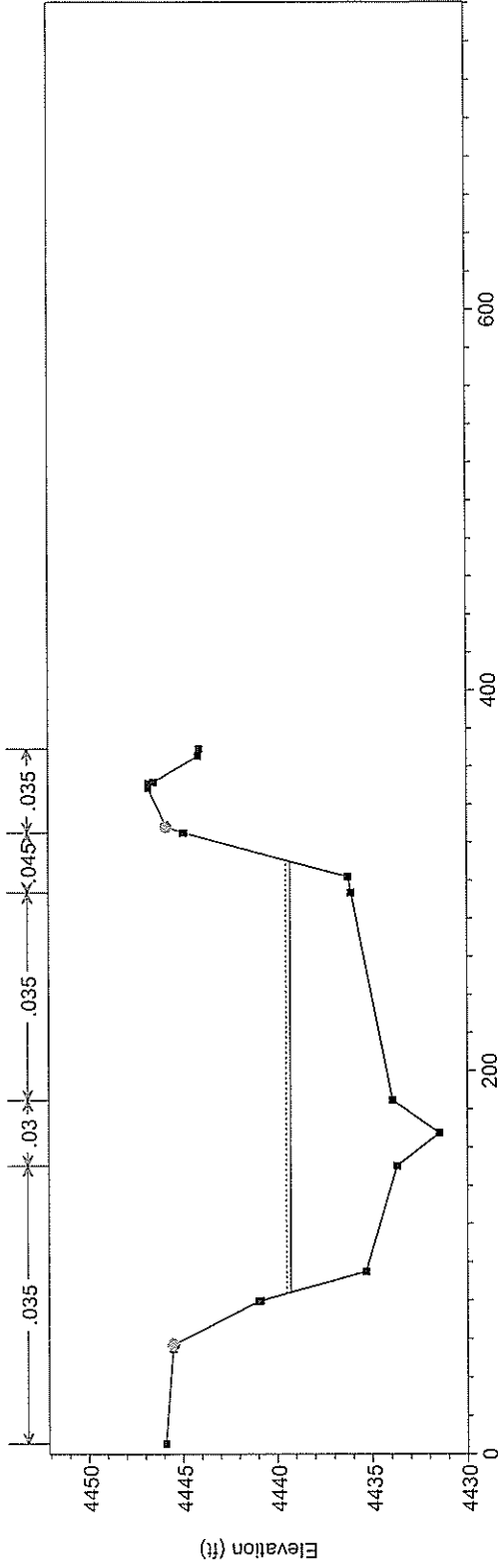
Legend	
.....	EG PF 1
————	WS PF 1
—●—	Ground
—■—	Bank Sta

1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 63

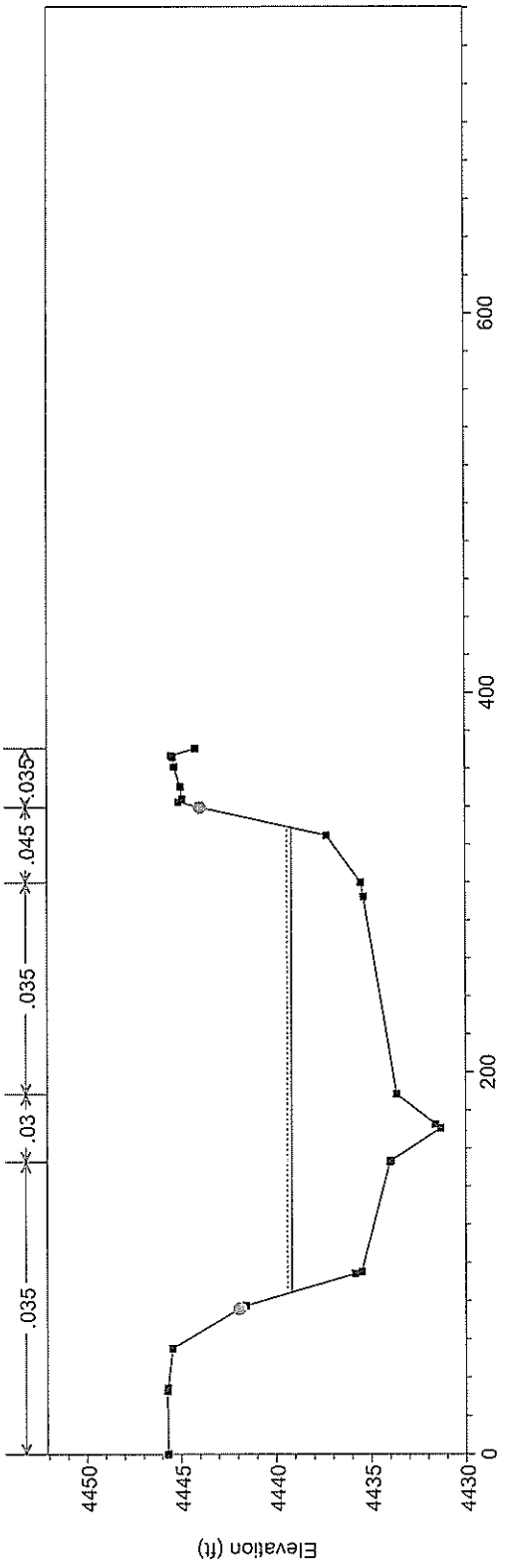


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 62

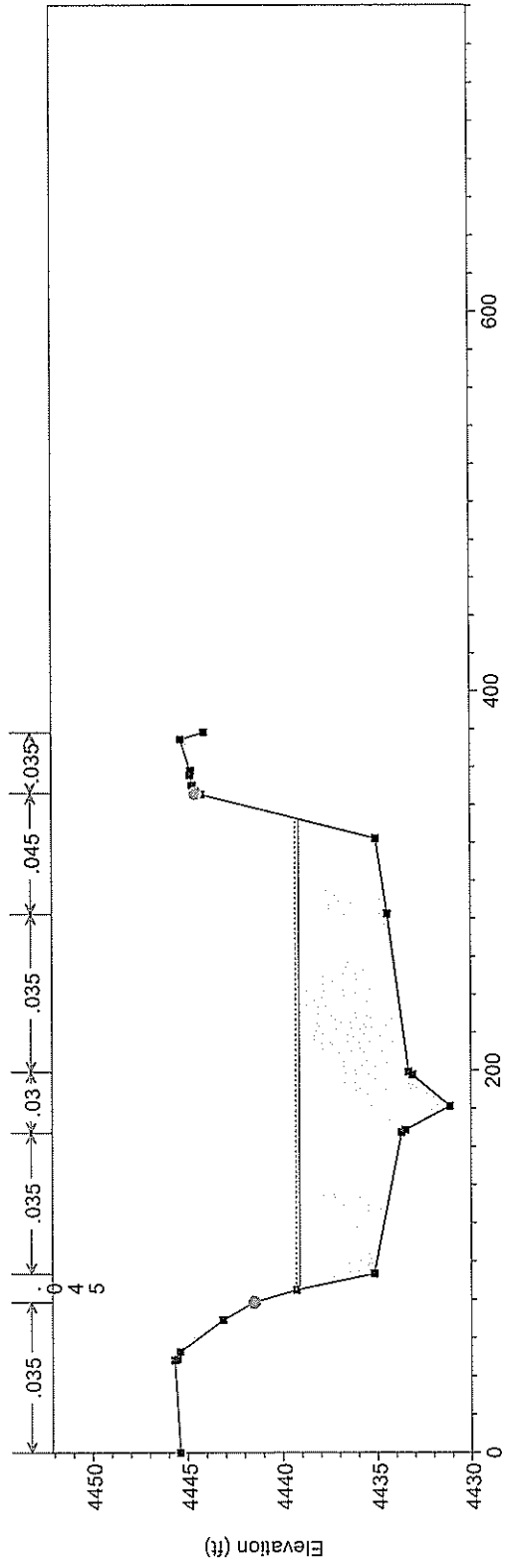


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 61



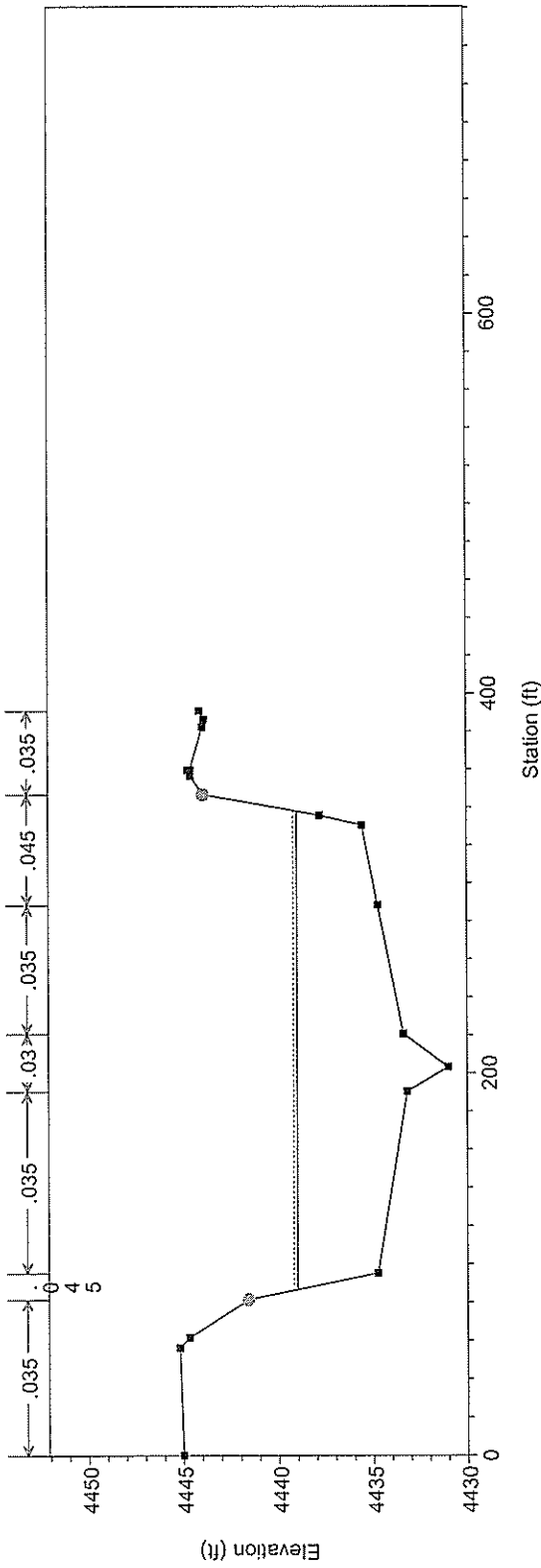
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 60



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

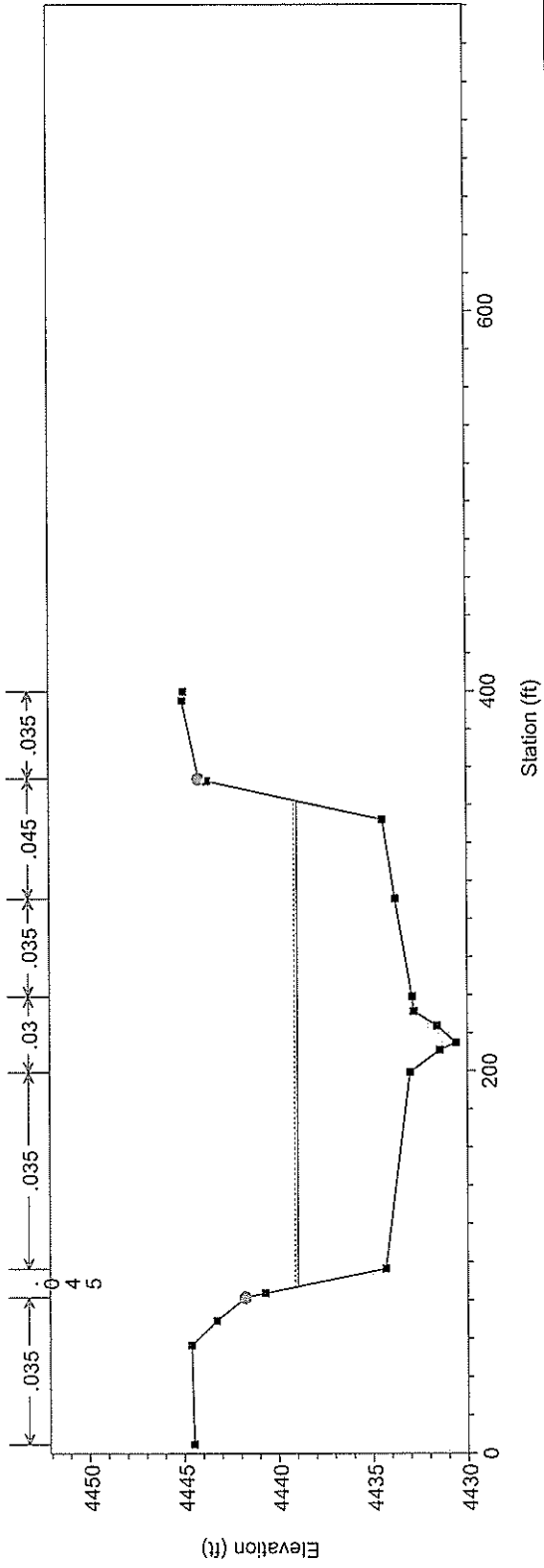
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 59



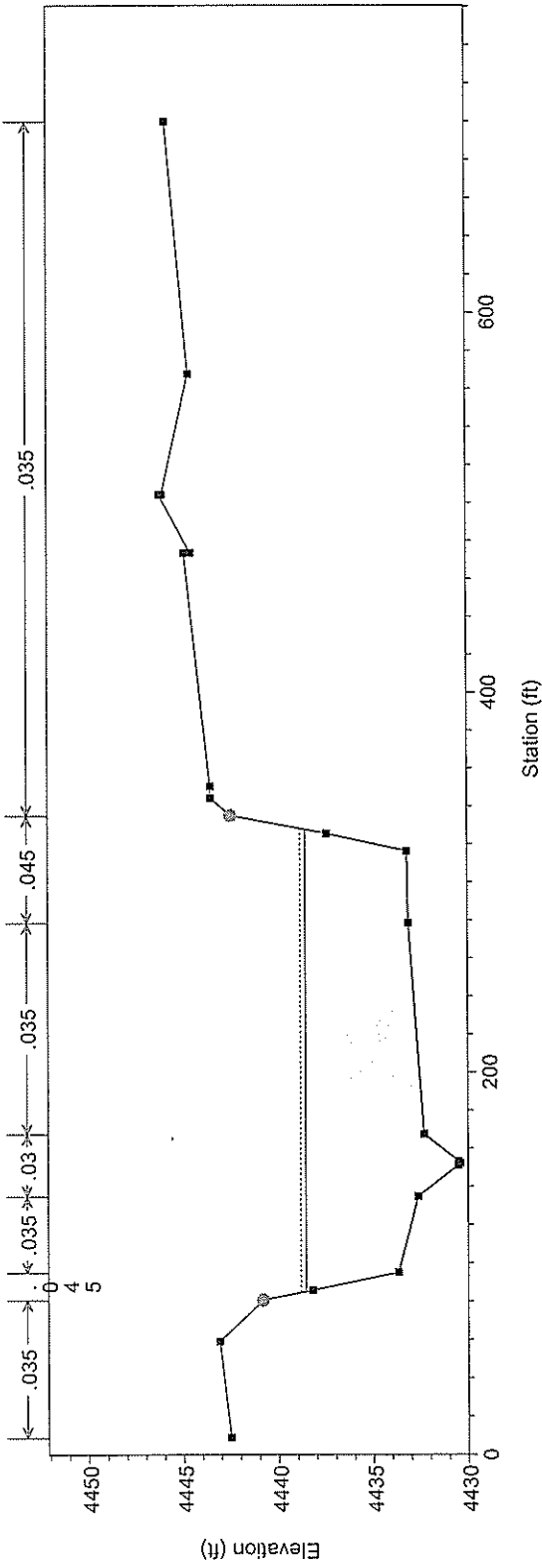
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 58

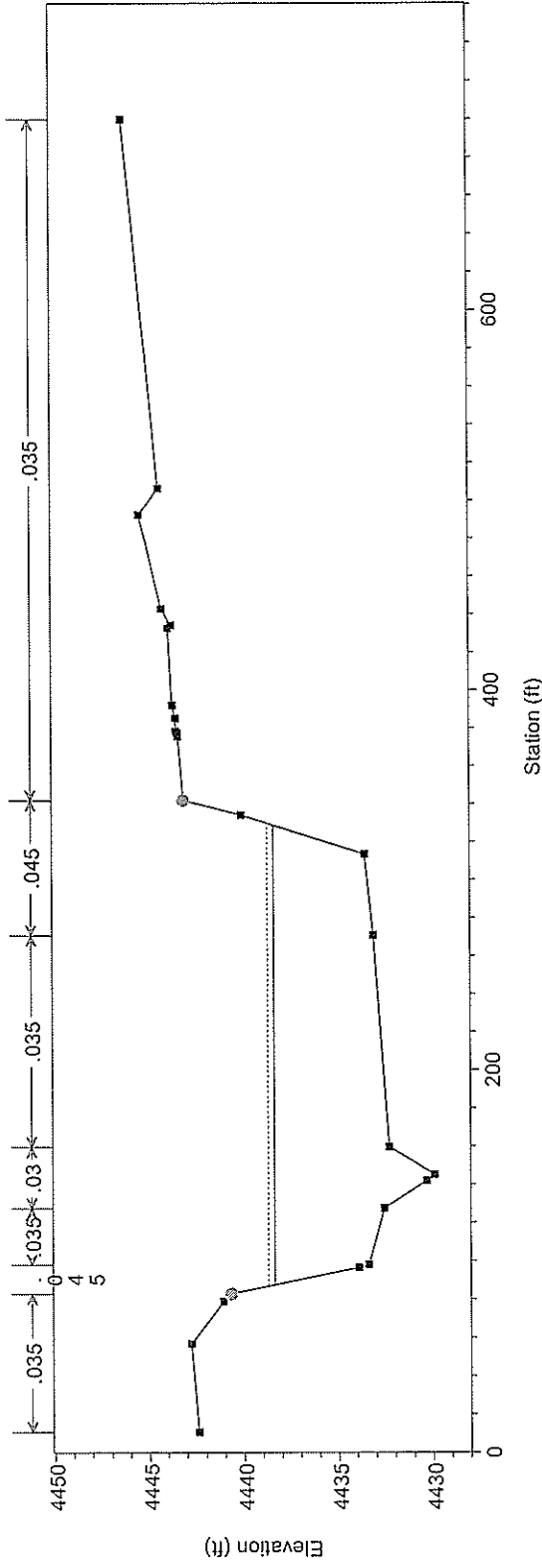


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 55



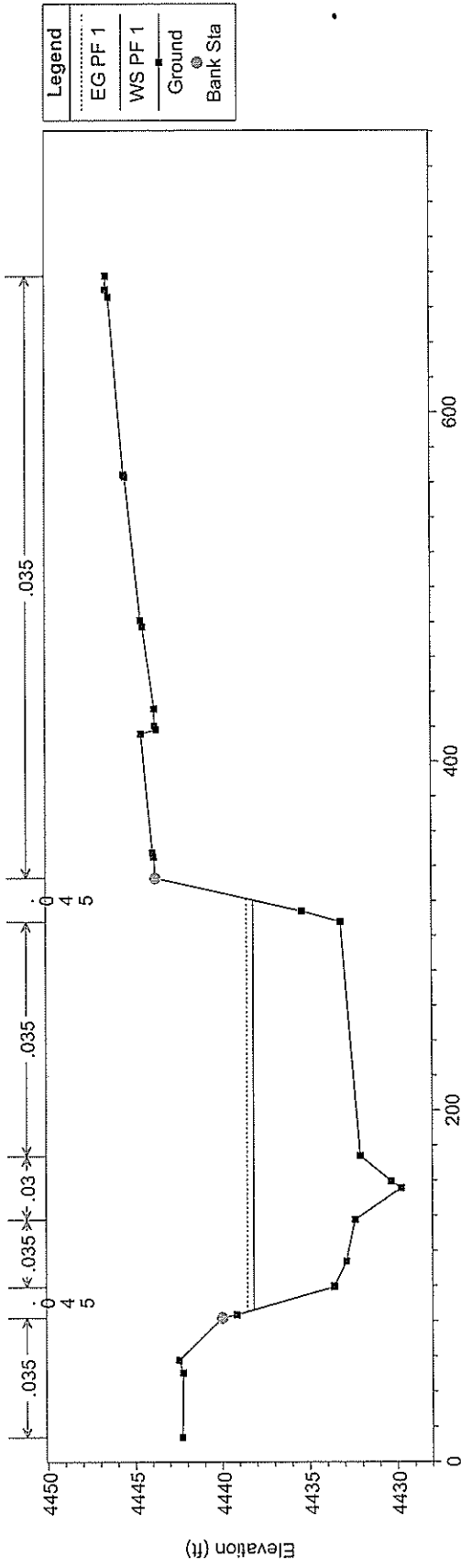
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 54



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

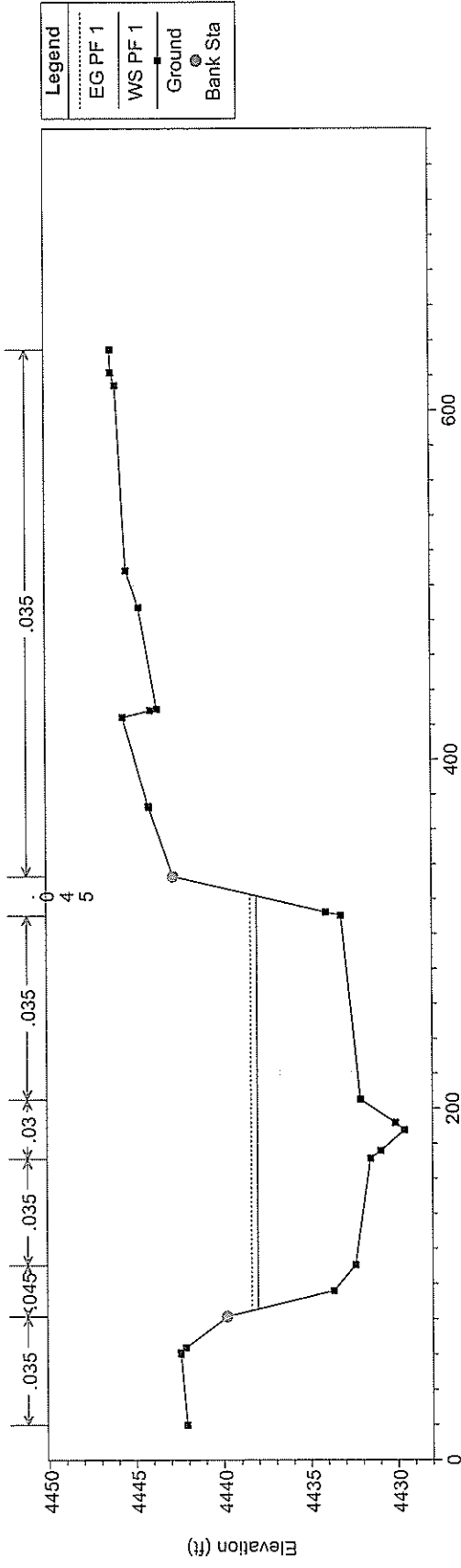
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 53



From as-built topo Plan: LOMR Submittal 1/8/2008

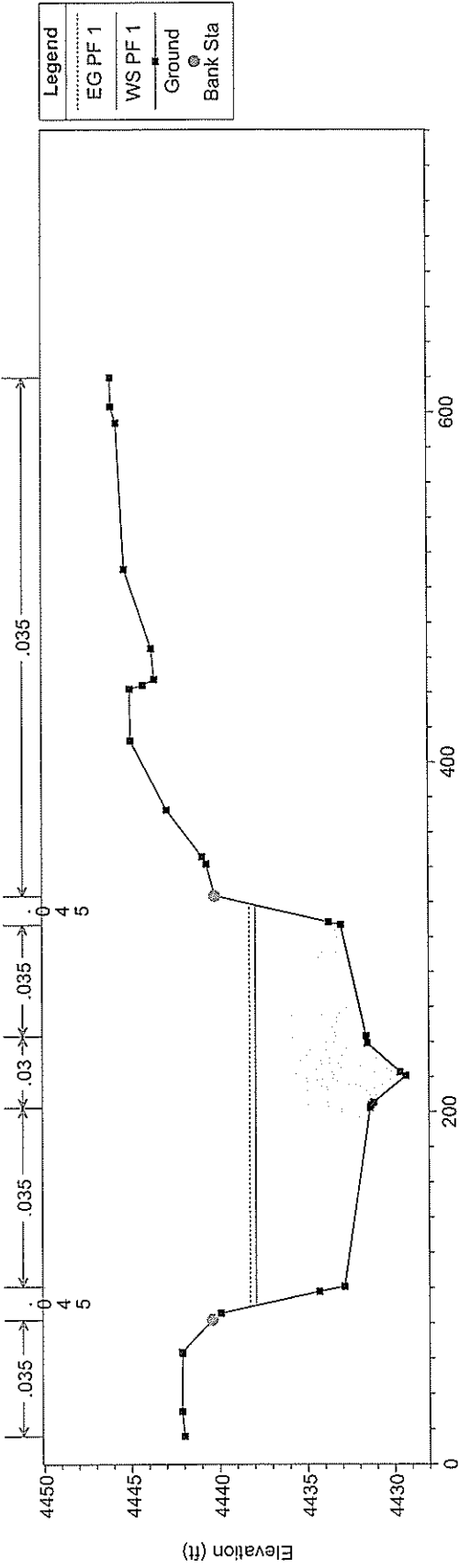
River = Steamboat Reach = Bella Vista RS = 52



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

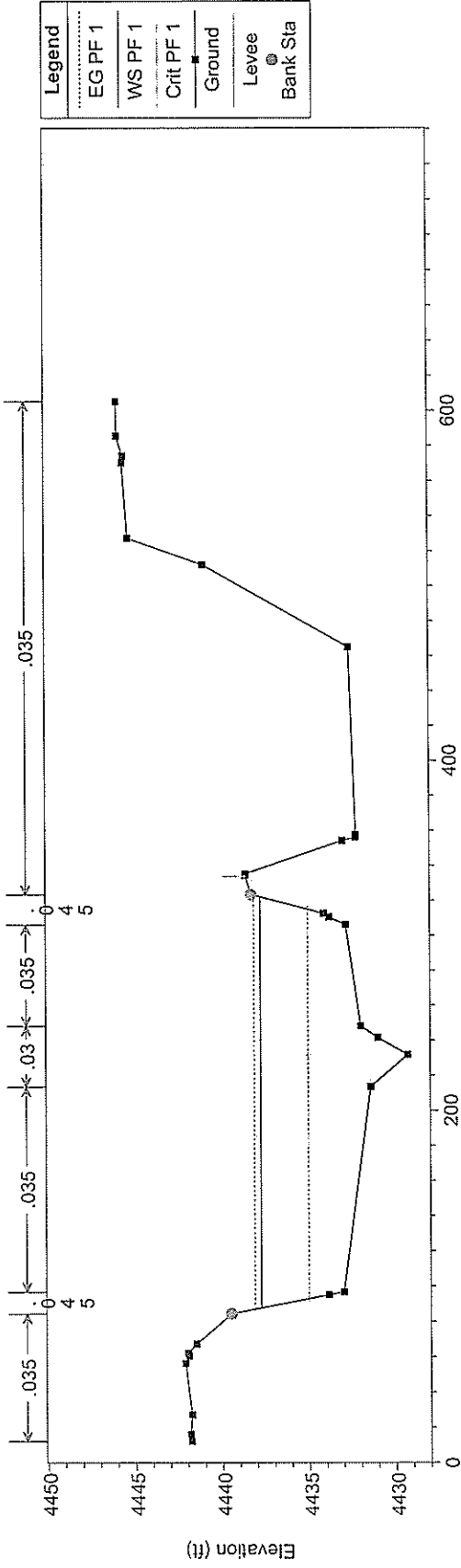
Plan: LOMR Submittal 1/8/2008

From as-built topo River = Steamboat Reach = Bella Vista RS = 51



Plan: LOMR Submittal 1/8/2008

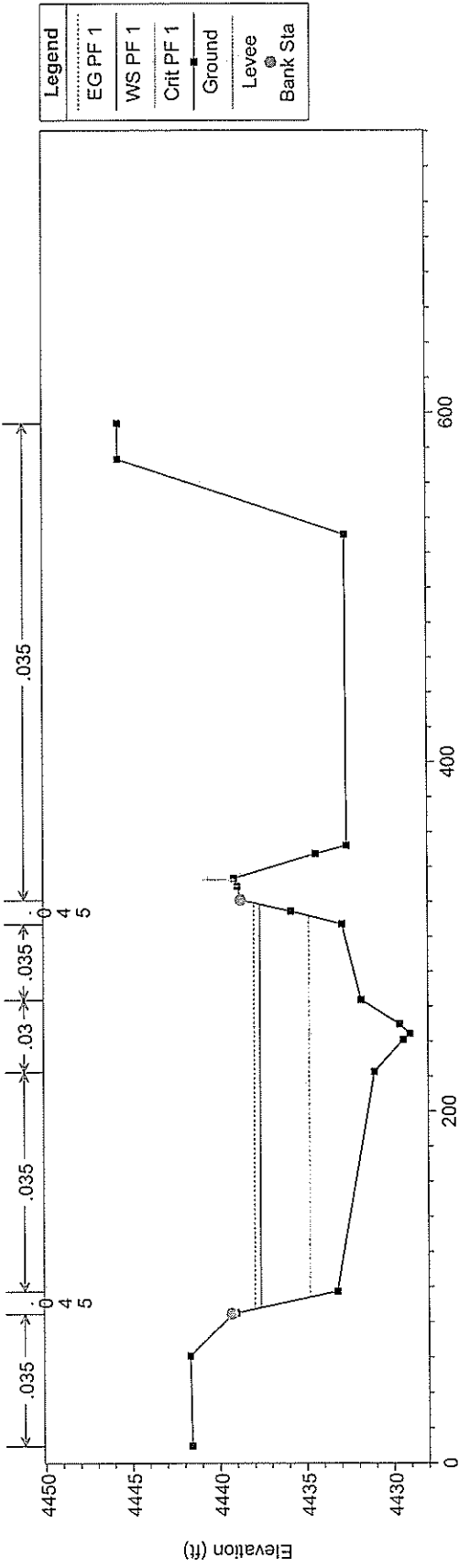
From as-built topo River = Steamboat Reach = Bella Vista RS = 50



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

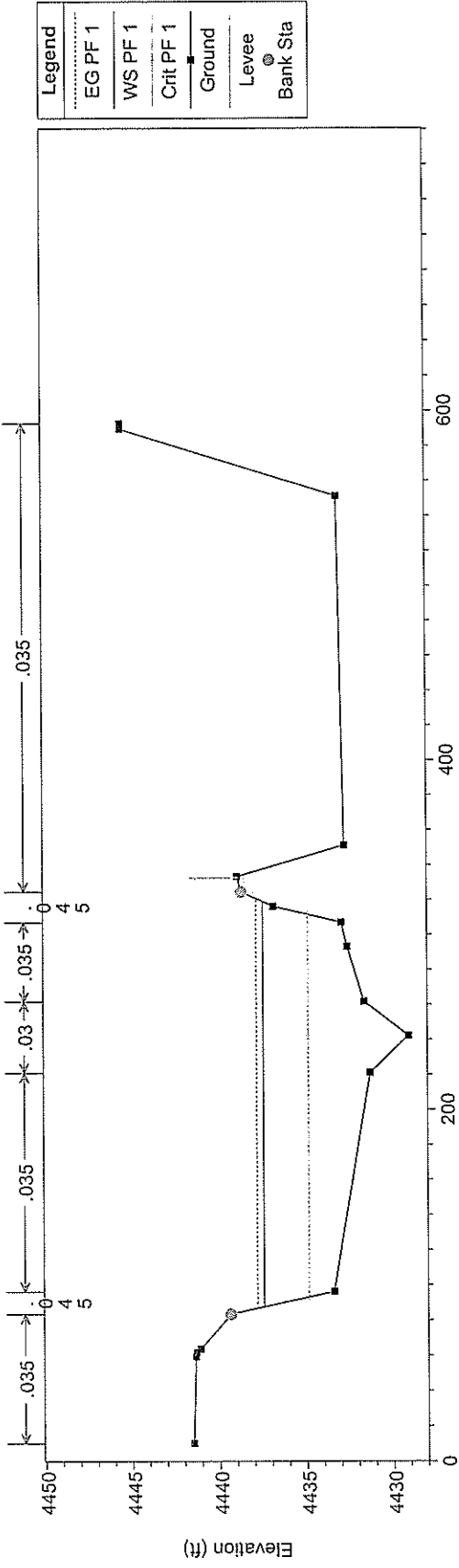
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 49



From as-built topo Plan: LOMR Submittal 1/8/2008

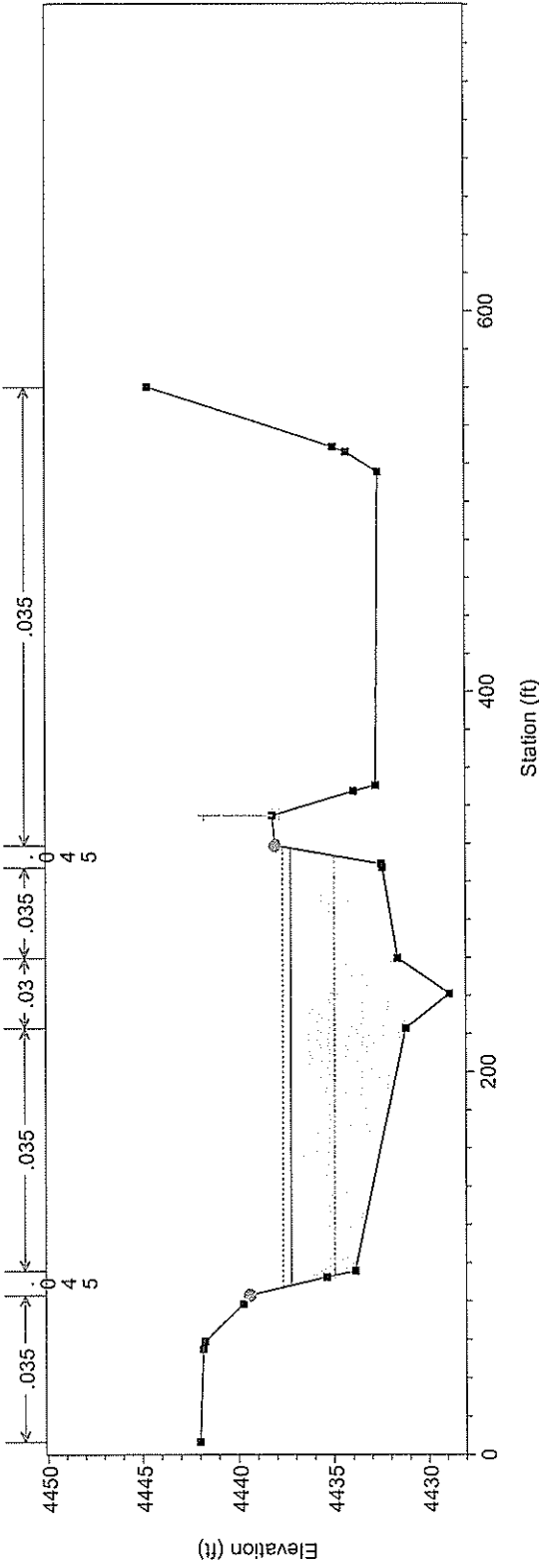
River = Steamboat Reach = Bella Vista RS = 48



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

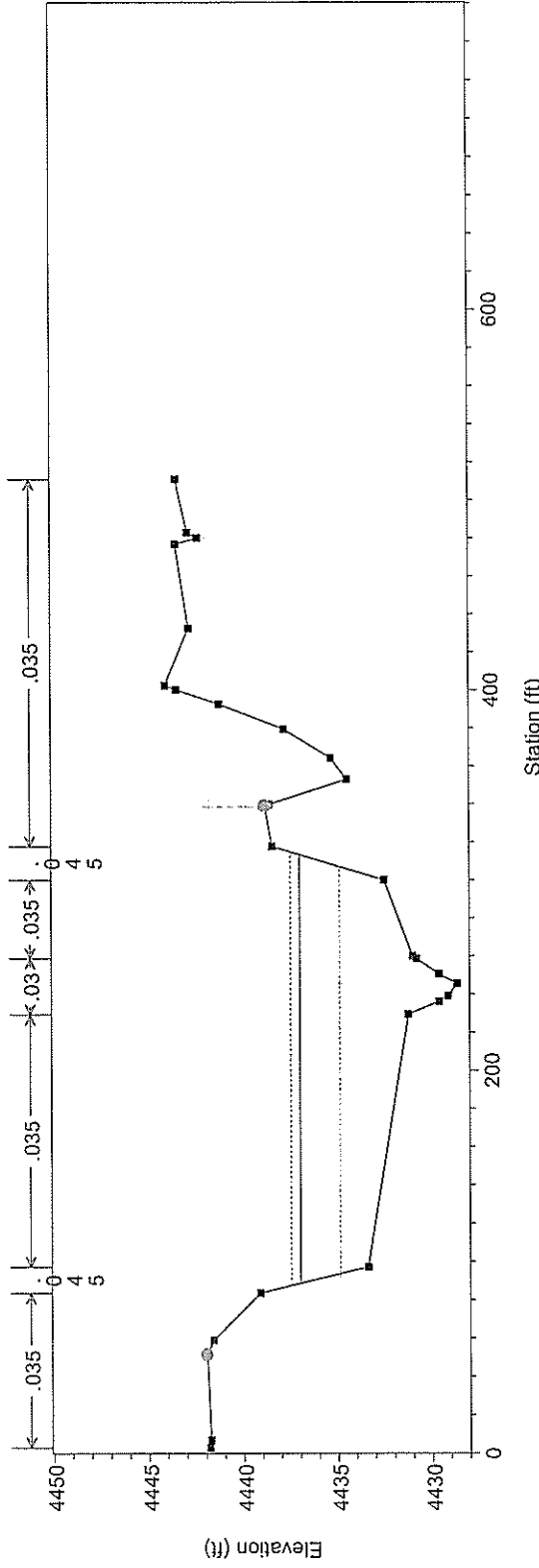
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 47



From as-built topo Plan: LOMR Submittal 1/8/2008

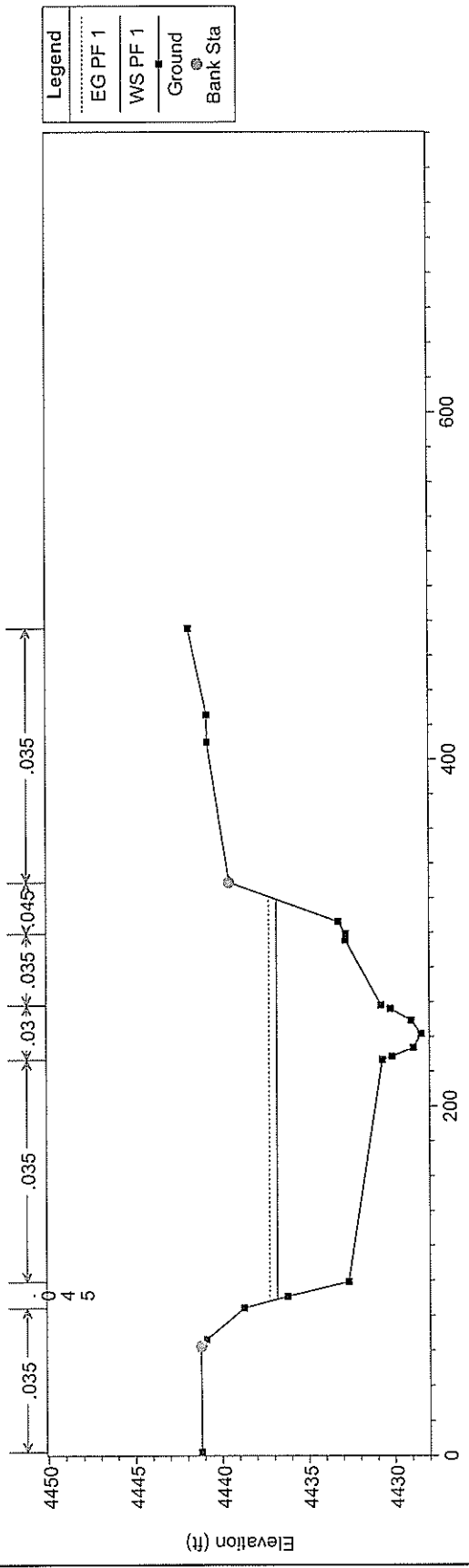
River = Steamboat Reach = Bella Vista RS = 46



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

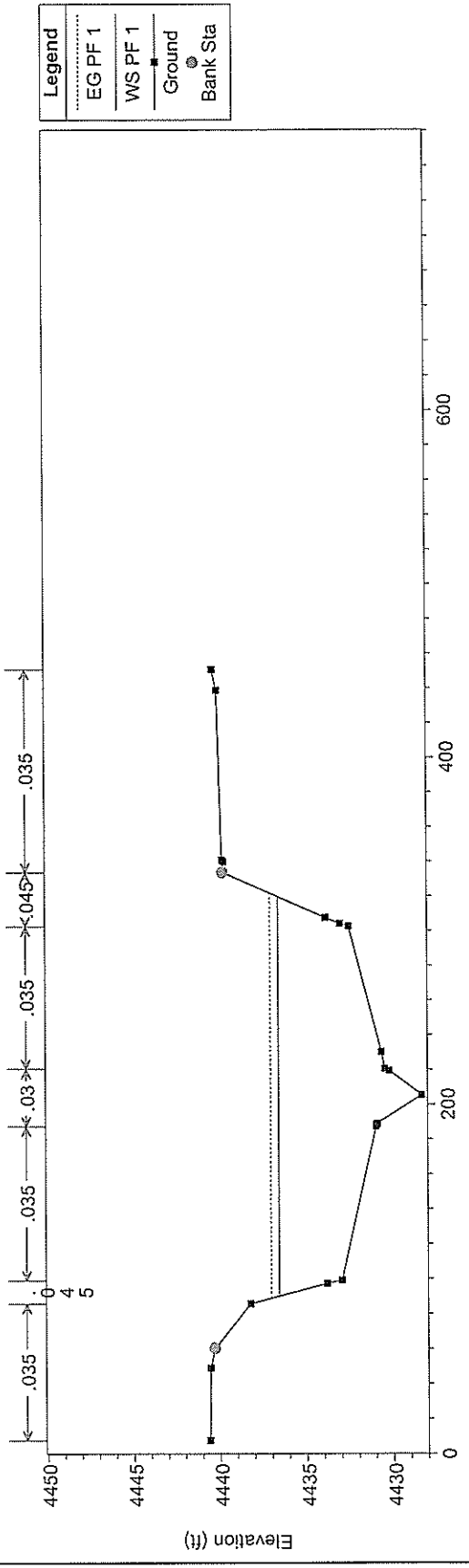
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 45



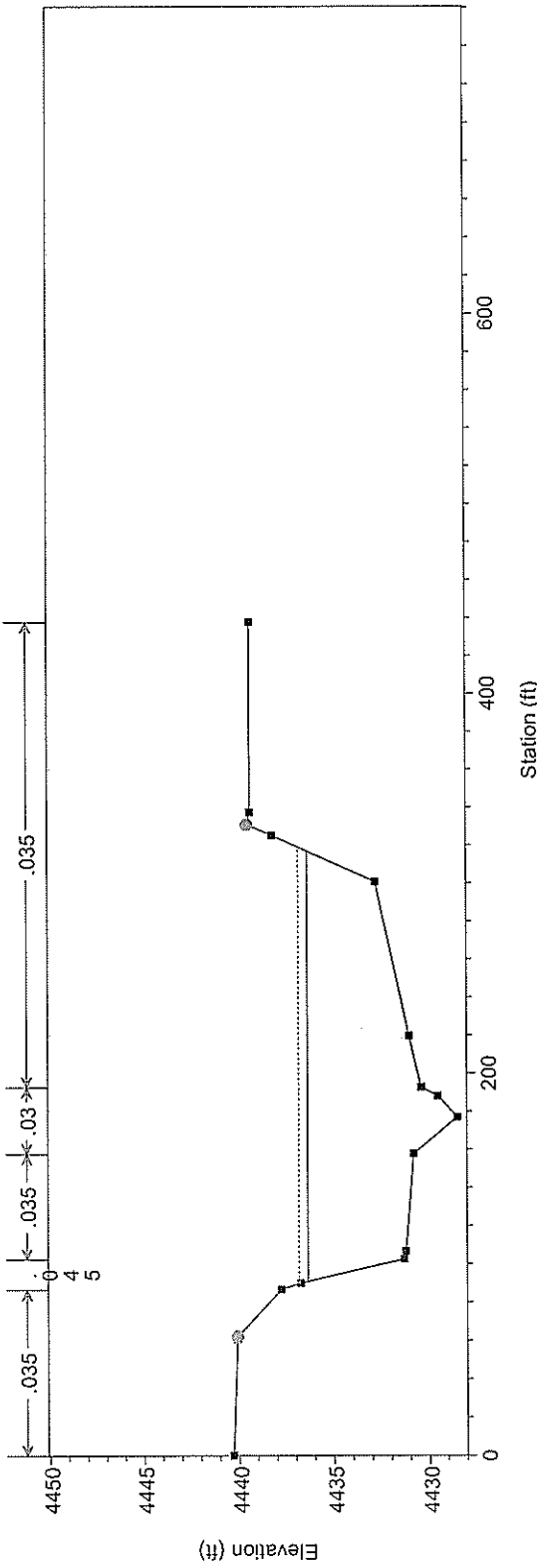
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 44

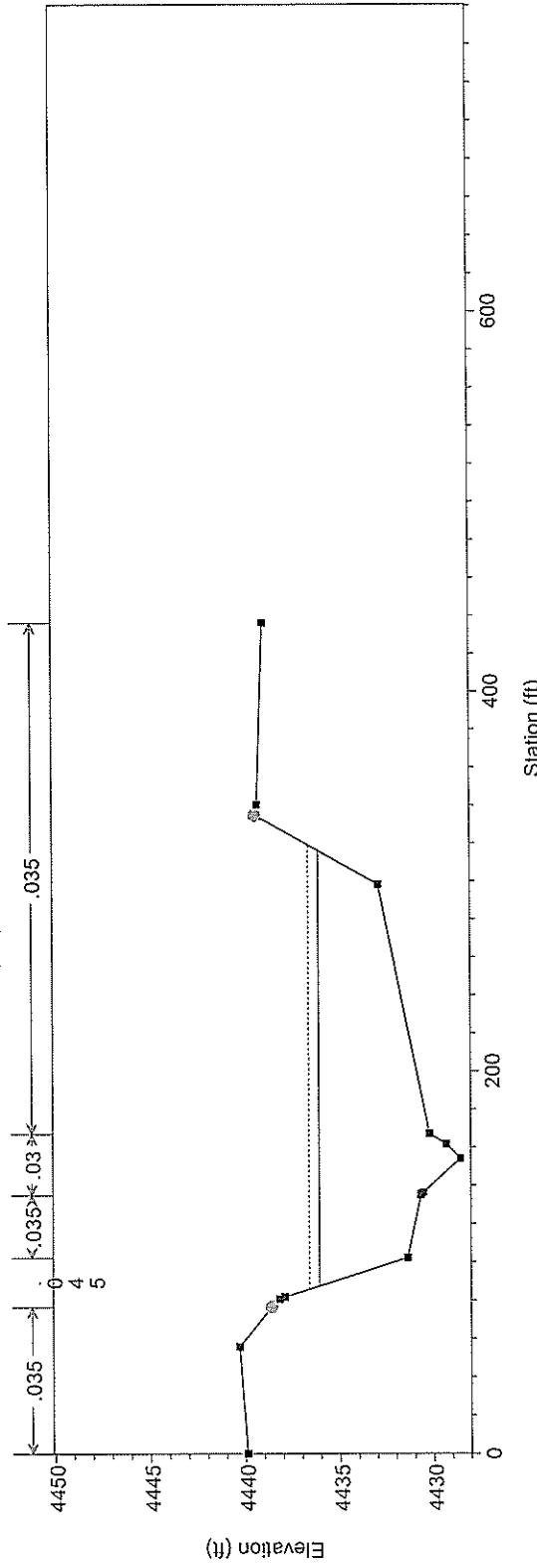


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 43

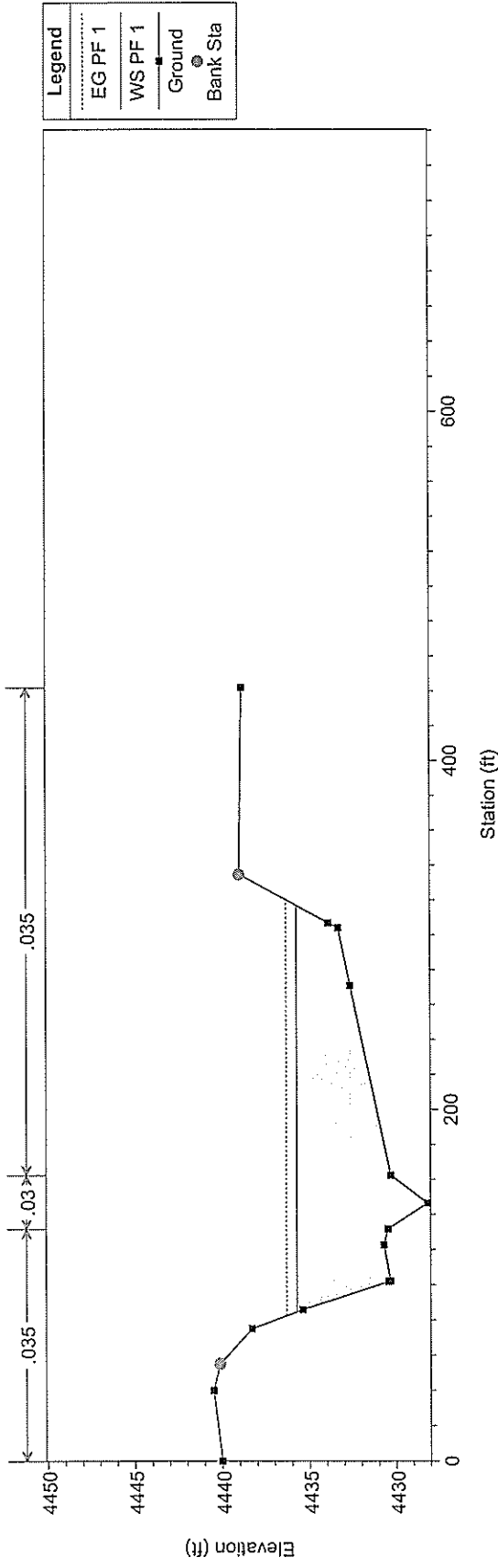


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 42

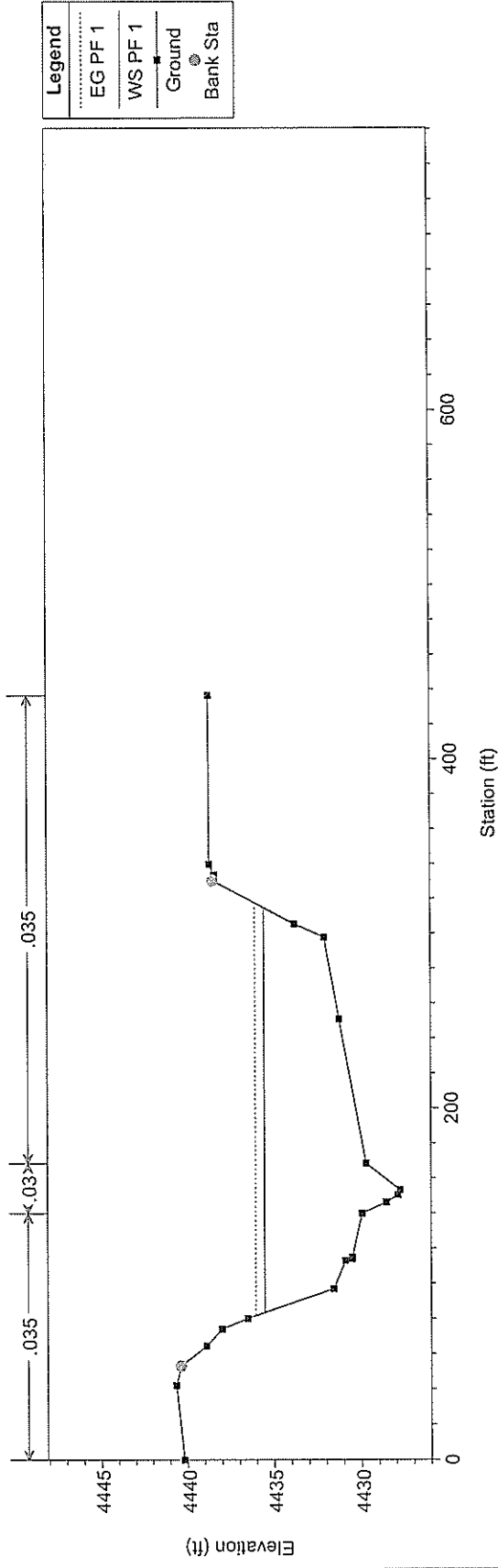


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 41

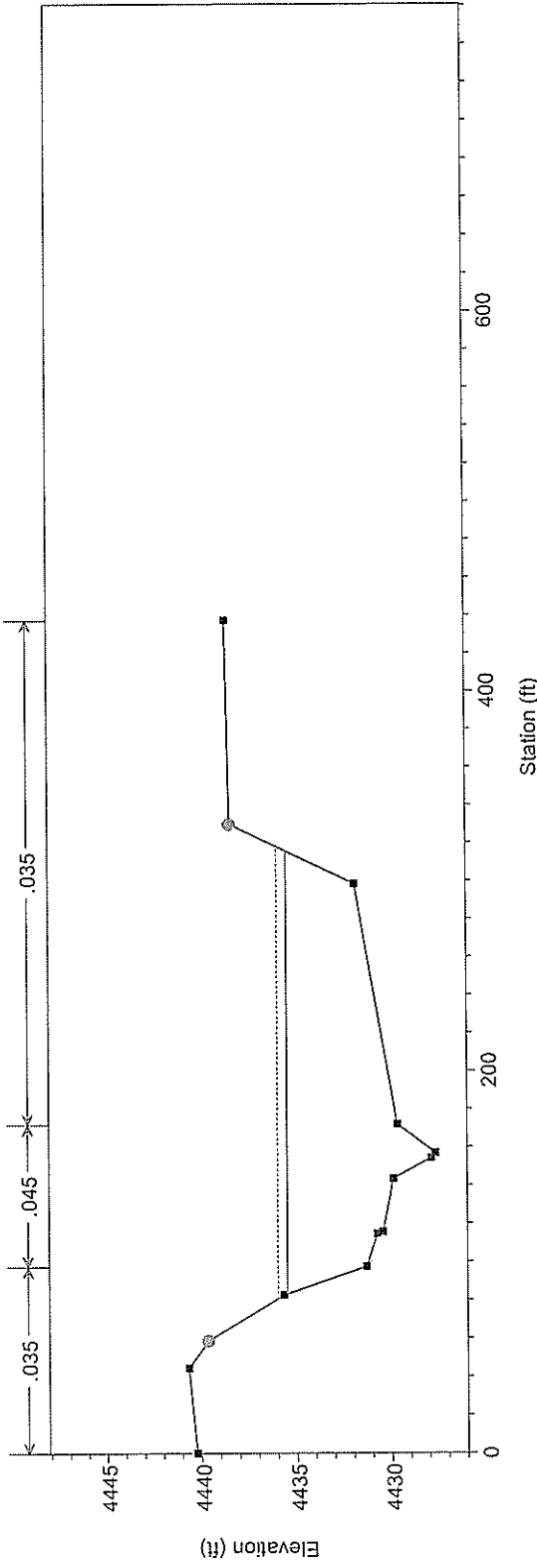


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 40

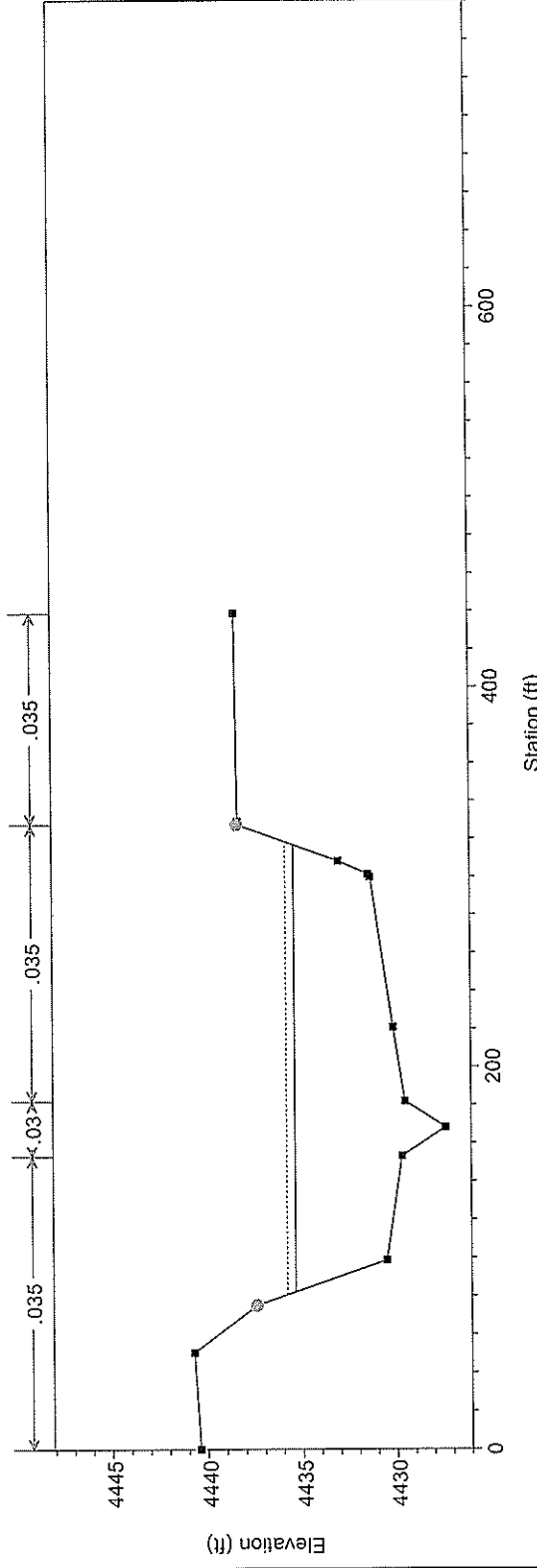


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 39.75

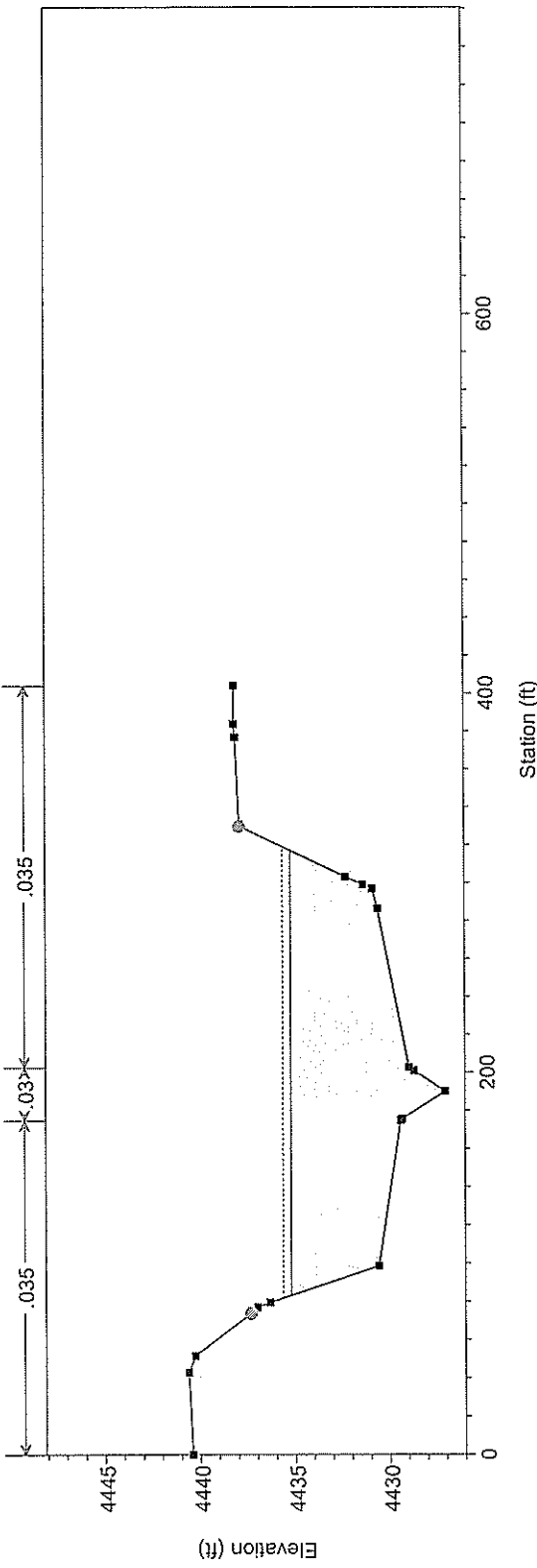


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 39



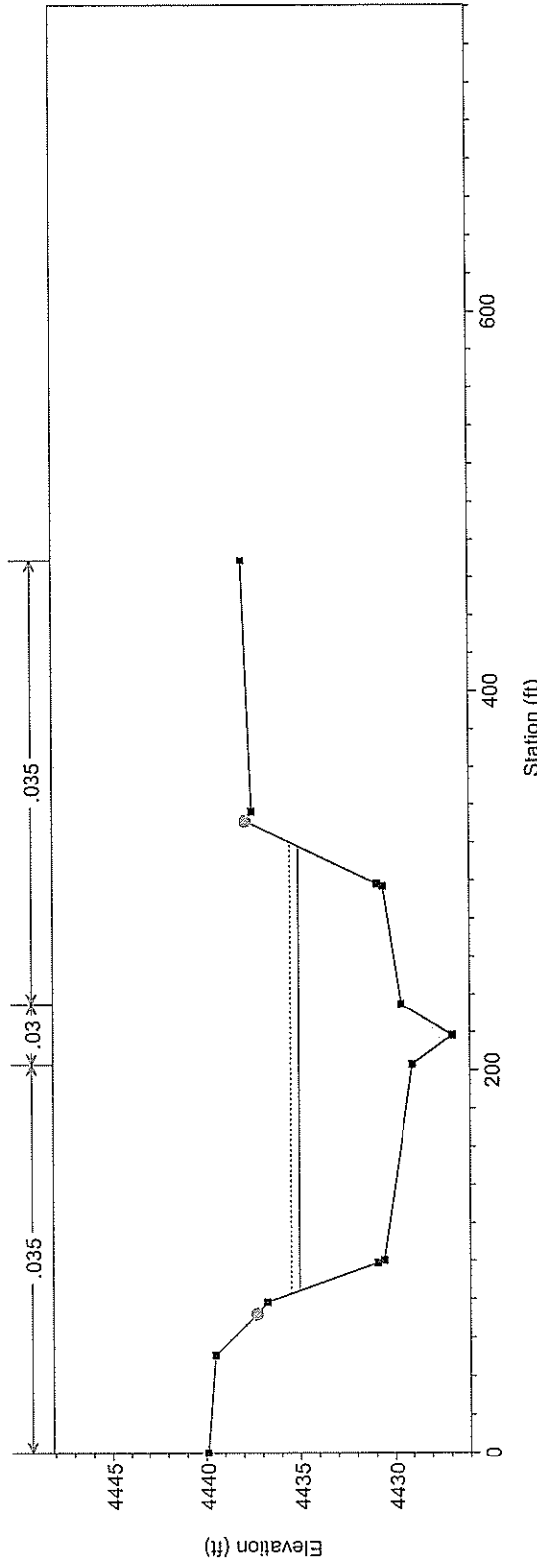
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 38



Legend
 EG PF 1
 WS PF 1
 Ground
 Bank Sta

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 37

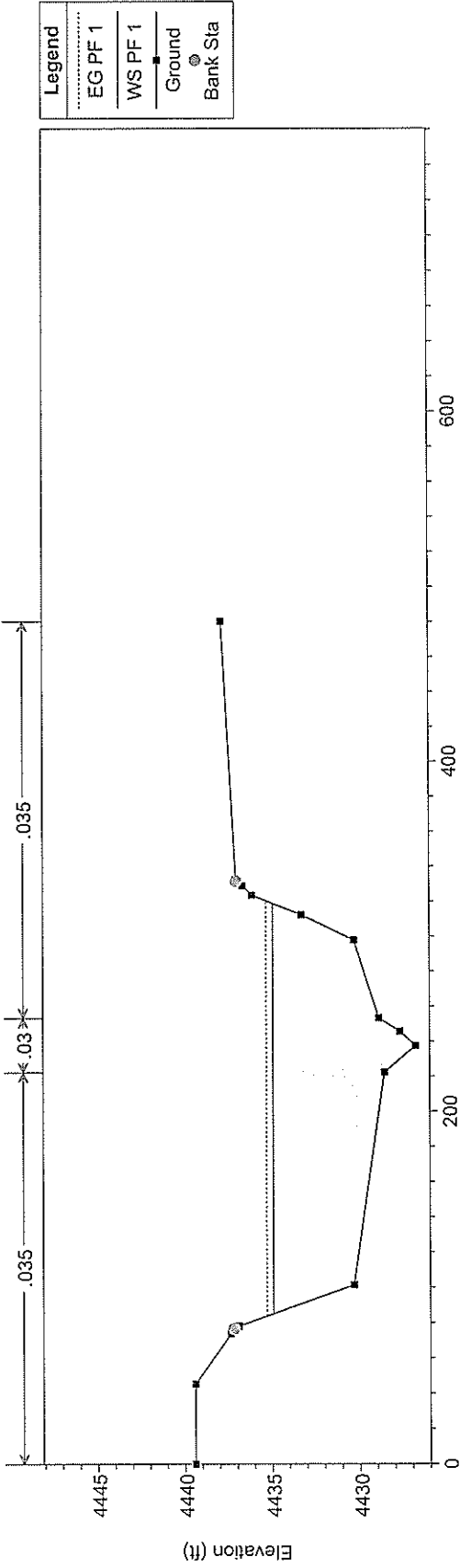


Legend
 EG PF 1
 WS PF 1
 Ground
 Bank Sta

1 in Horiz. = 100 ft 1 in Vert. = 10 ft

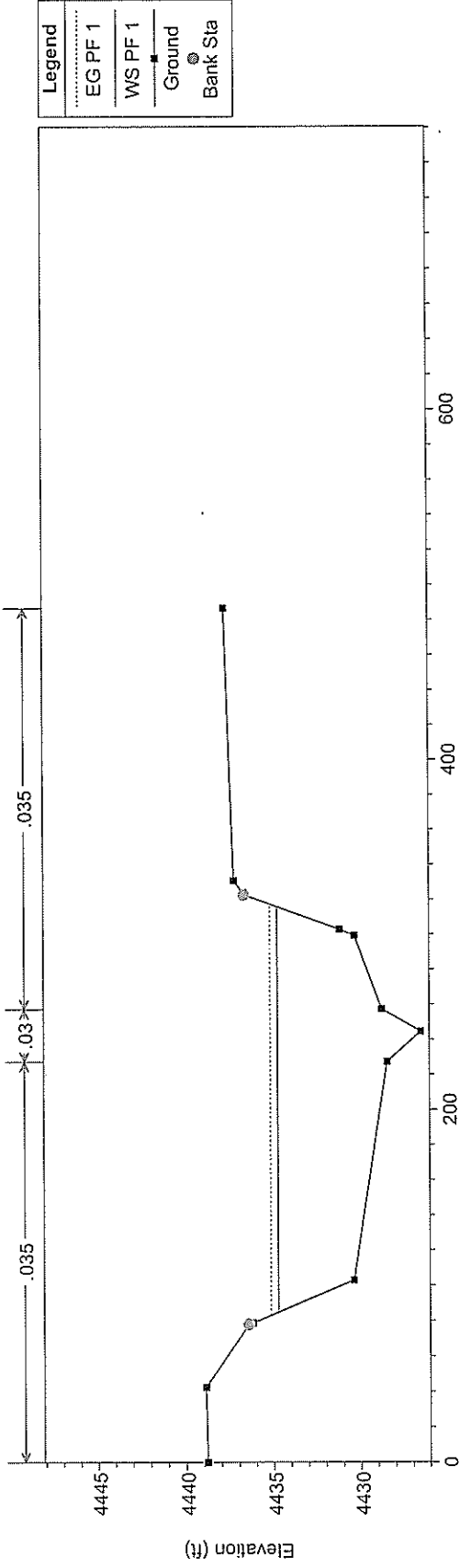
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 36



From as-built topo Plan: LOMR Submittal 1/8/2008

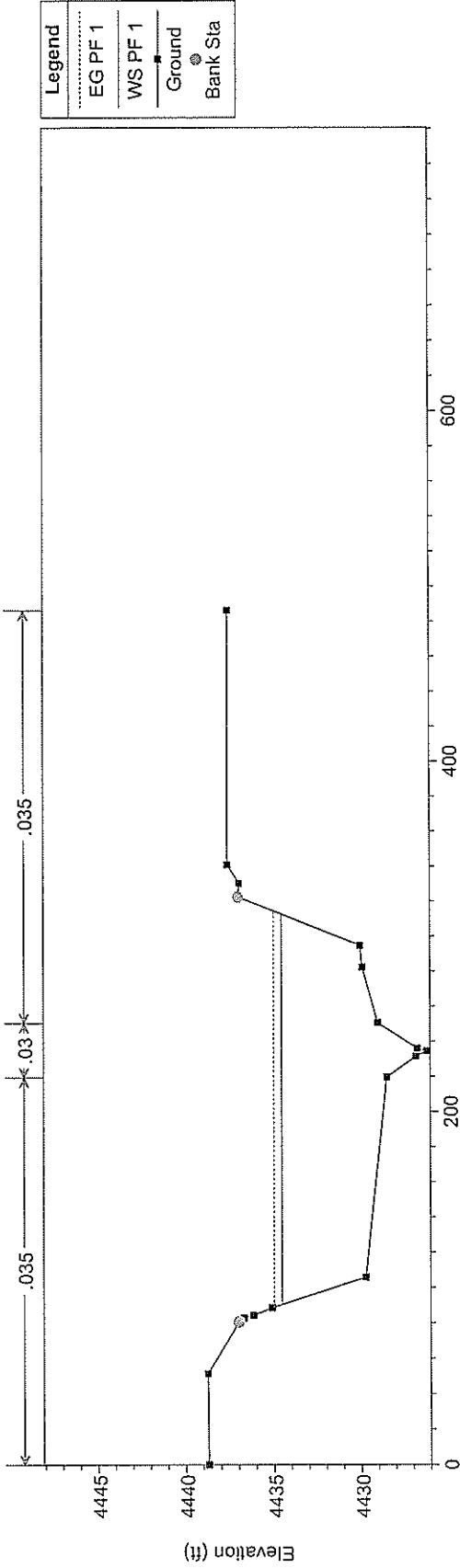
River = Steamboat Reach = Bella Vista RS = 35



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

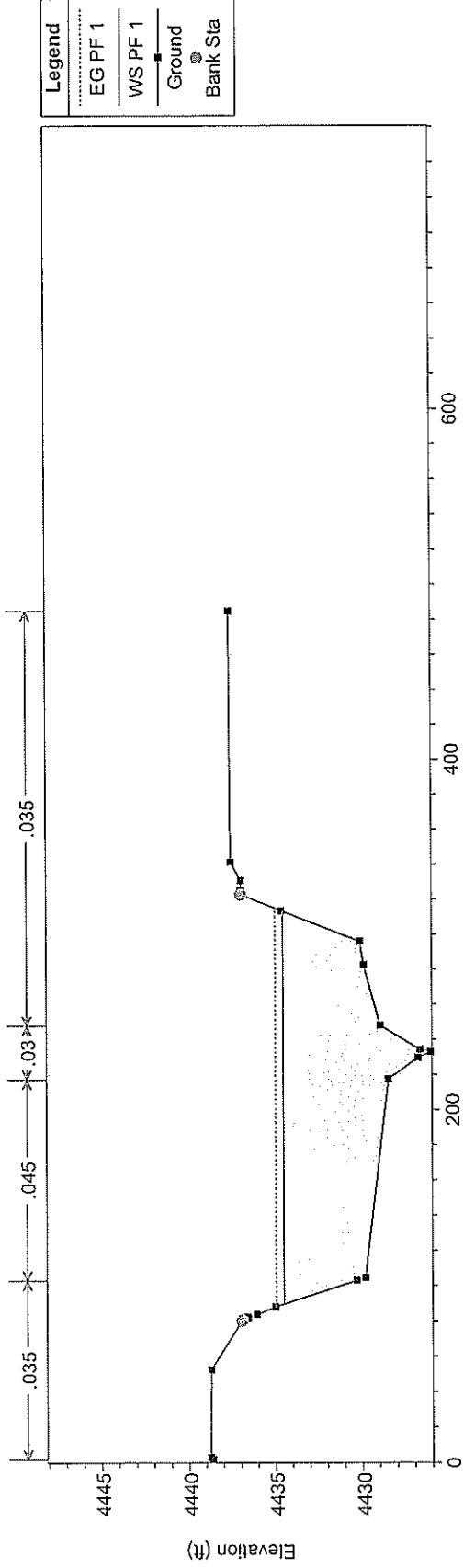
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 34



From as-built topo Plan: LOMR Submittal 1/8/2008

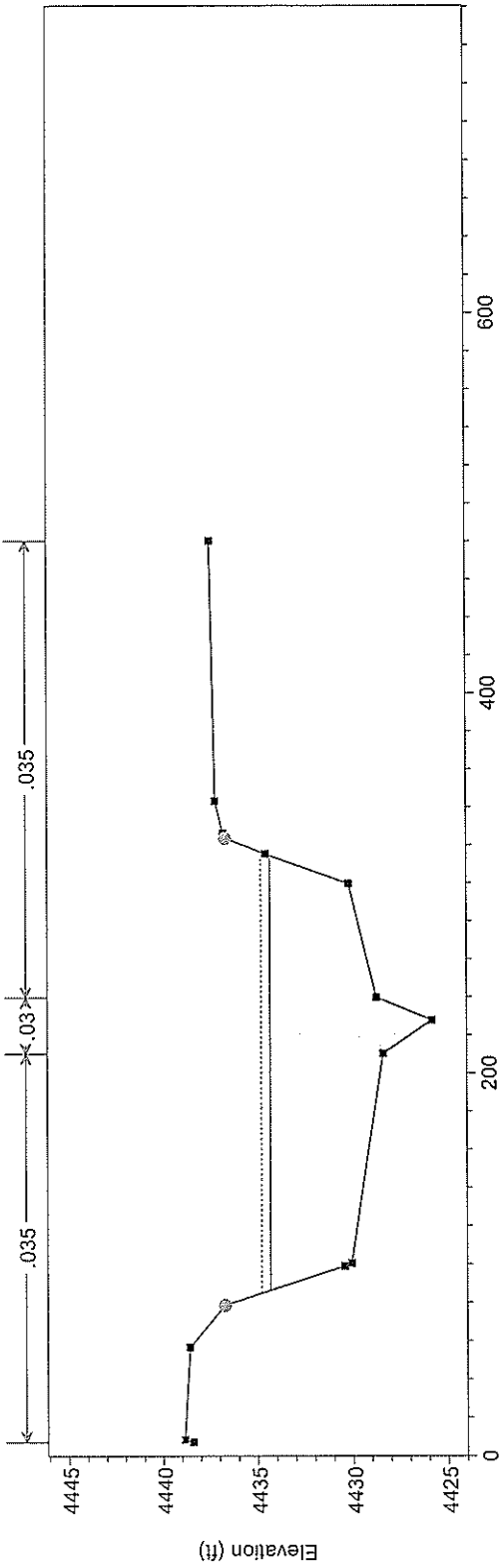
River = Steamboat Reach = Bella Vista RS = 33.75



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

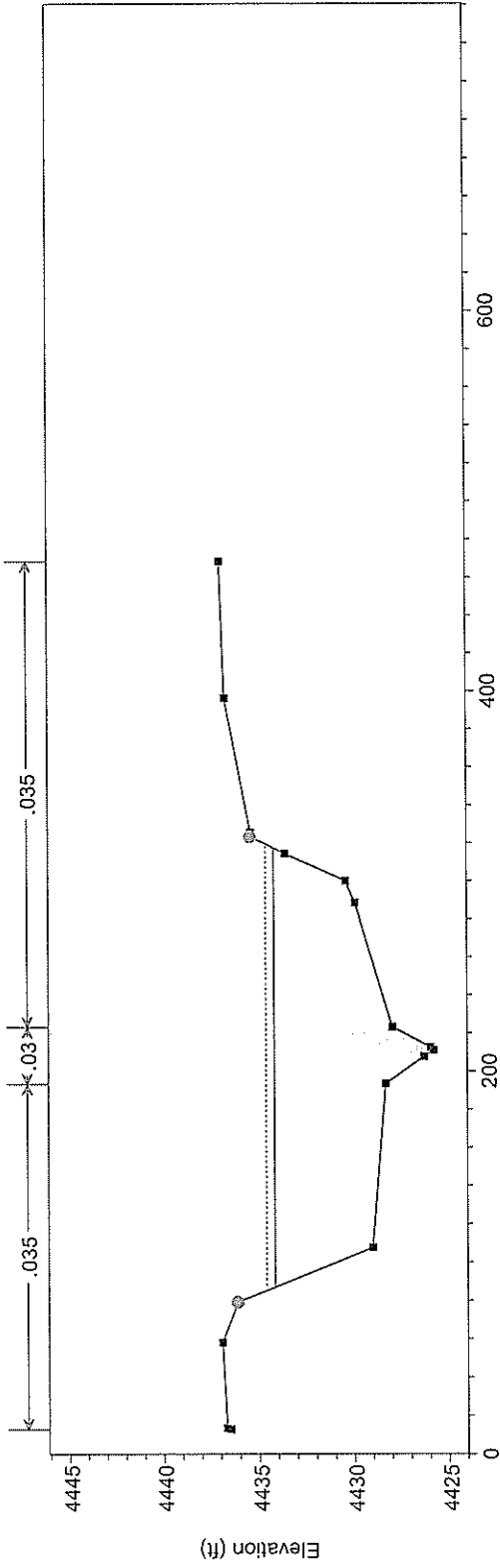
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 33



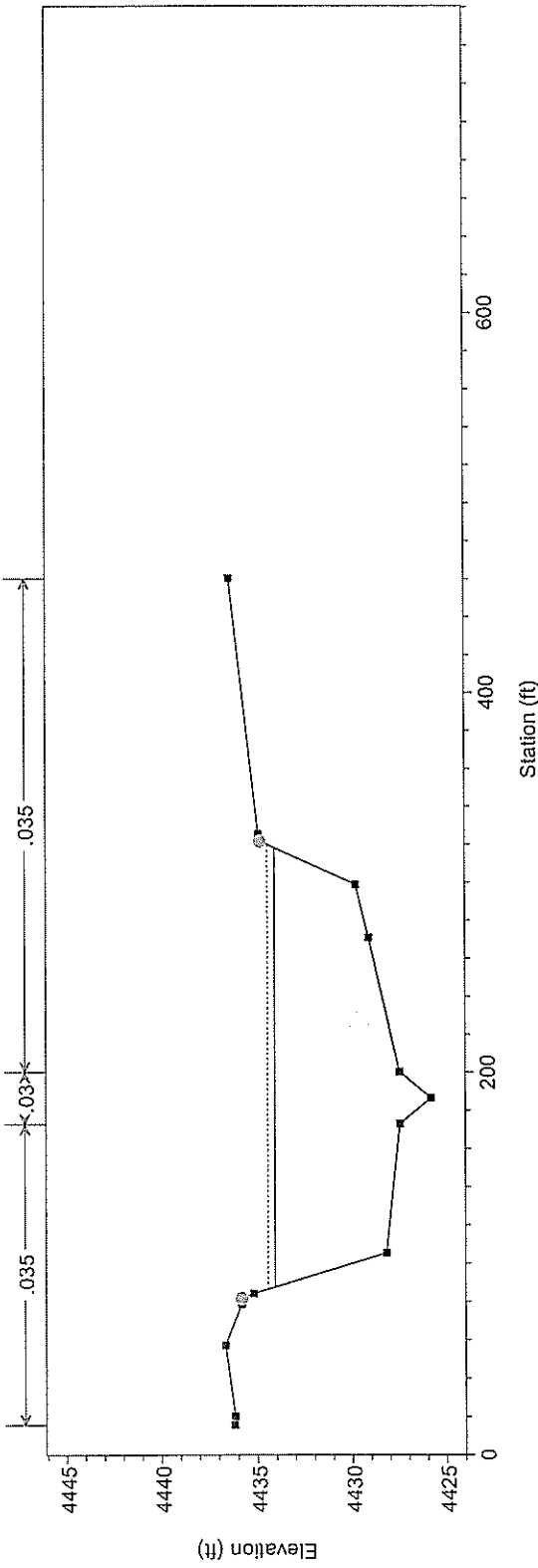
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 32

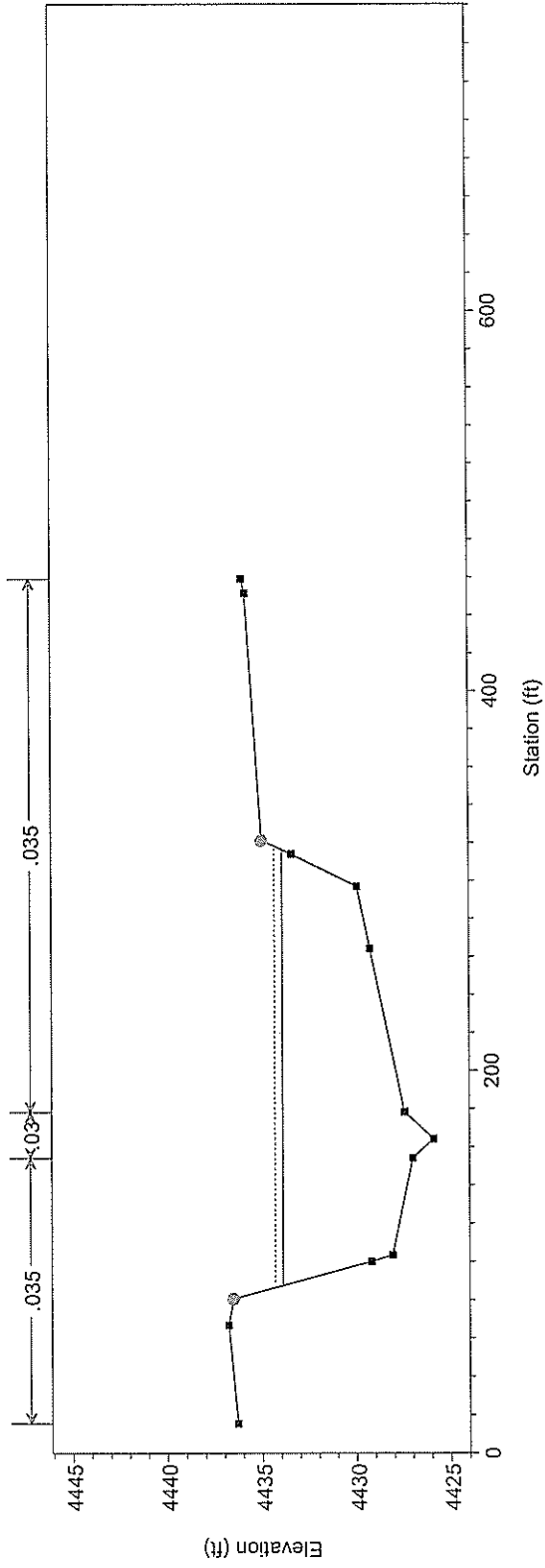


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 31



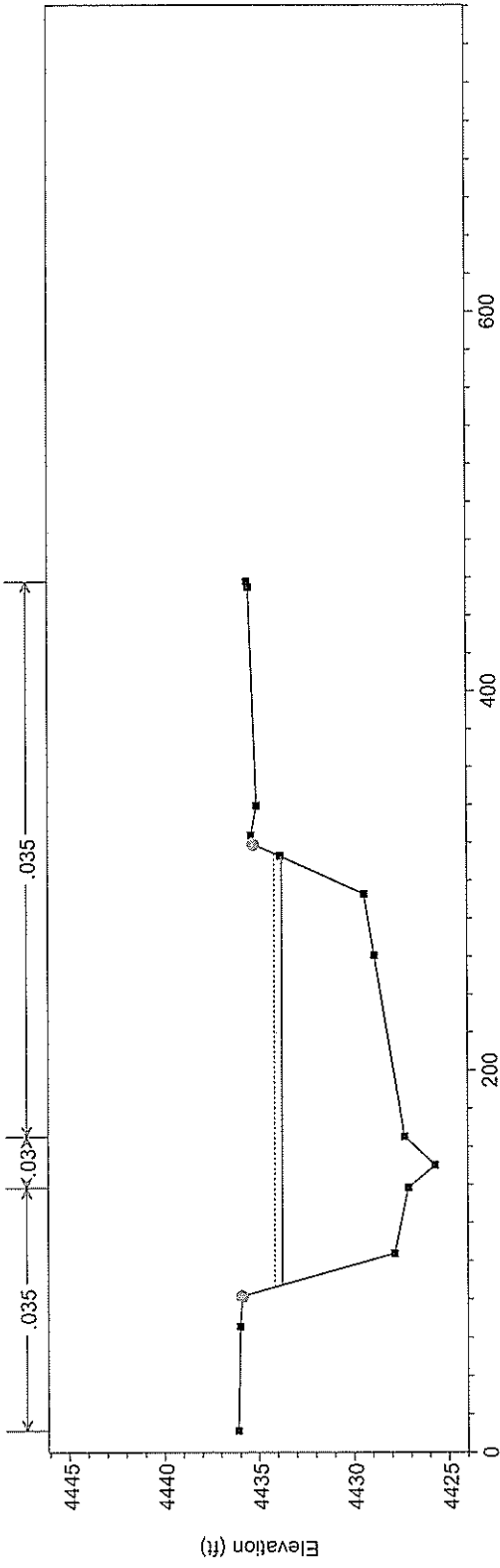
From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 30



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

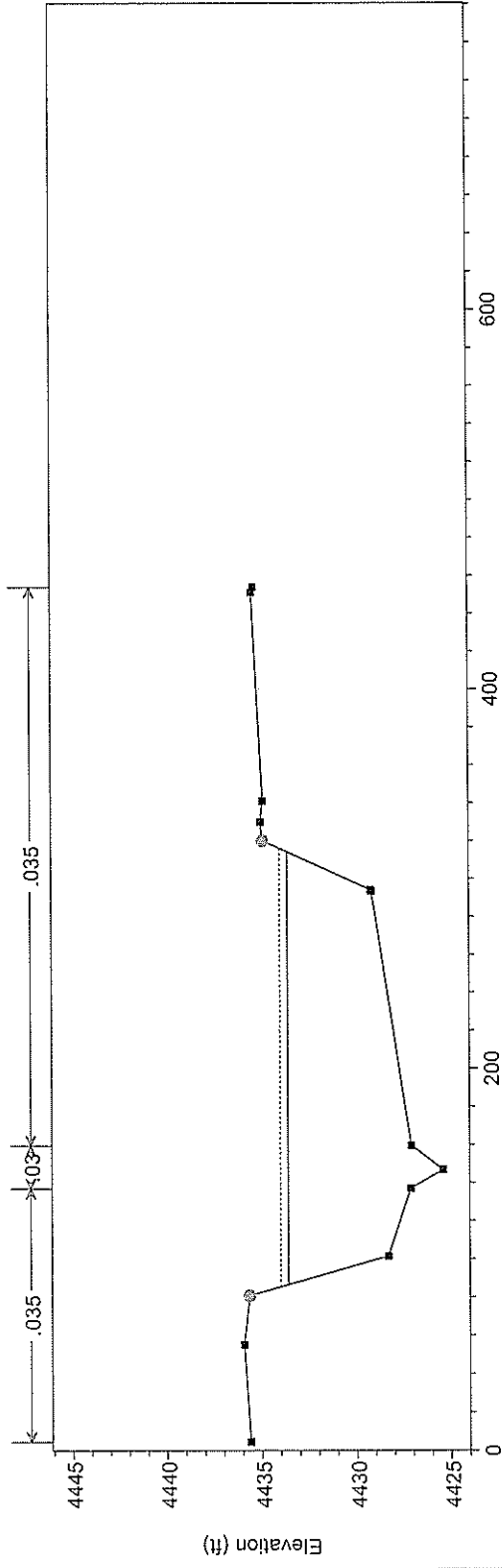
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 29



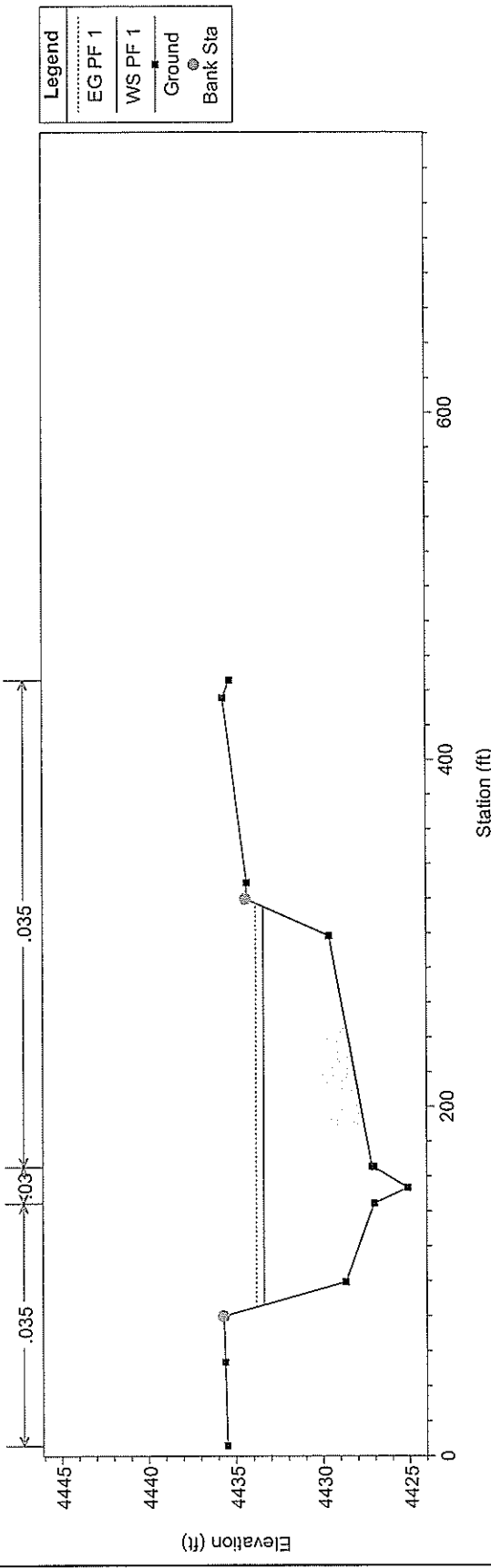
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 28

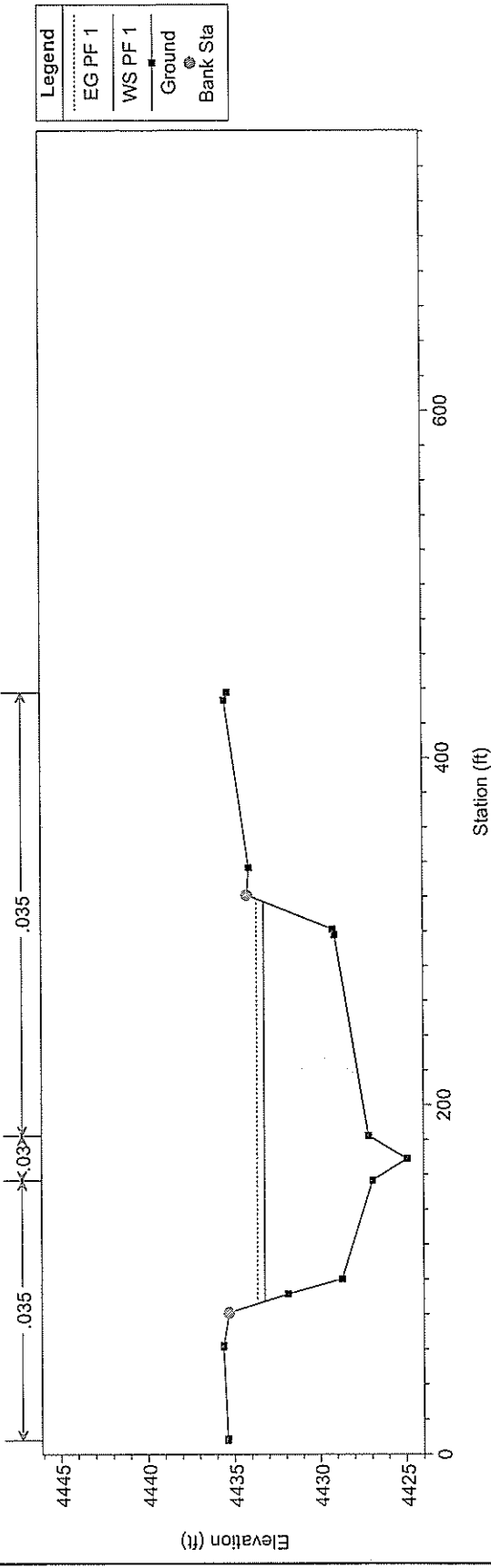


1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 27

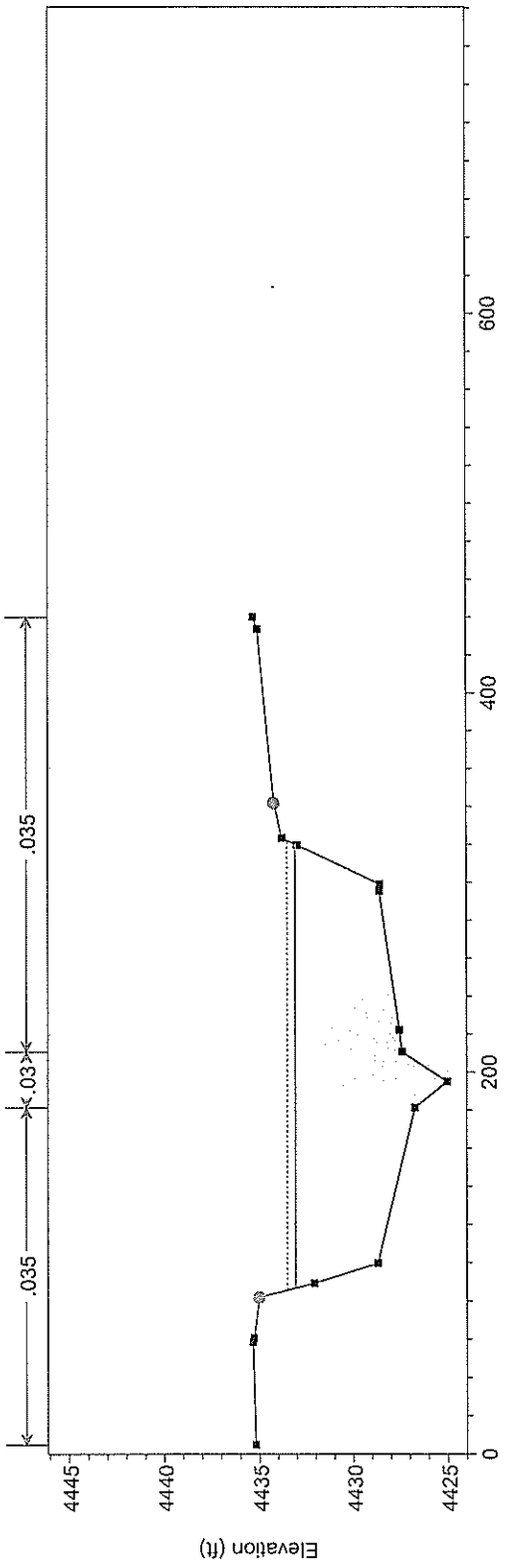


From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 26



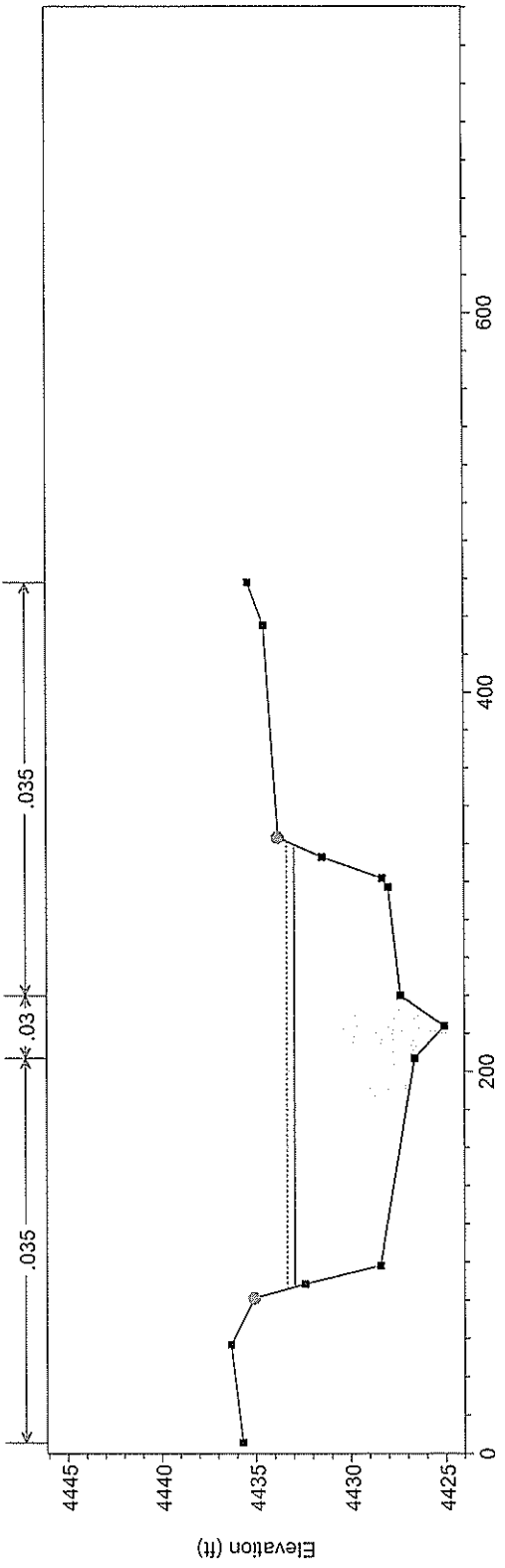
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 25



Legend	
.....	EG PF 1
—————	WS PF 1
—————	Ground
●	Bank Sta

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 24

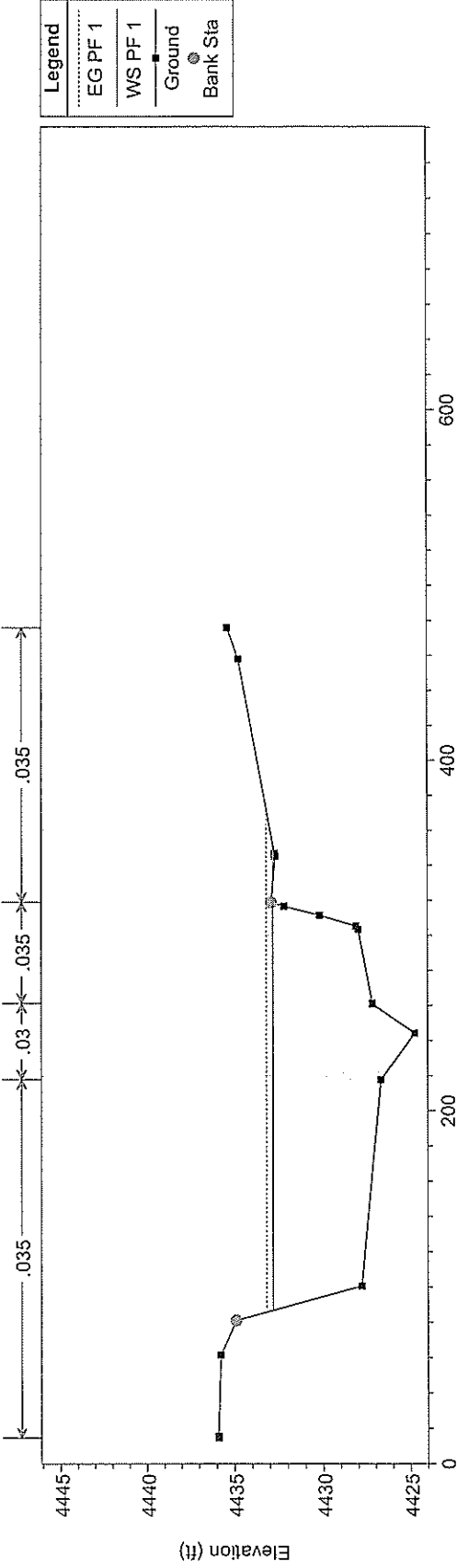


Legend	
.....	EG PF 1
—————	WS PF 1
—————	Ground
●	Bank Sta

1 in Horiz. = 100 ft 1 in Vert. = 10 ft

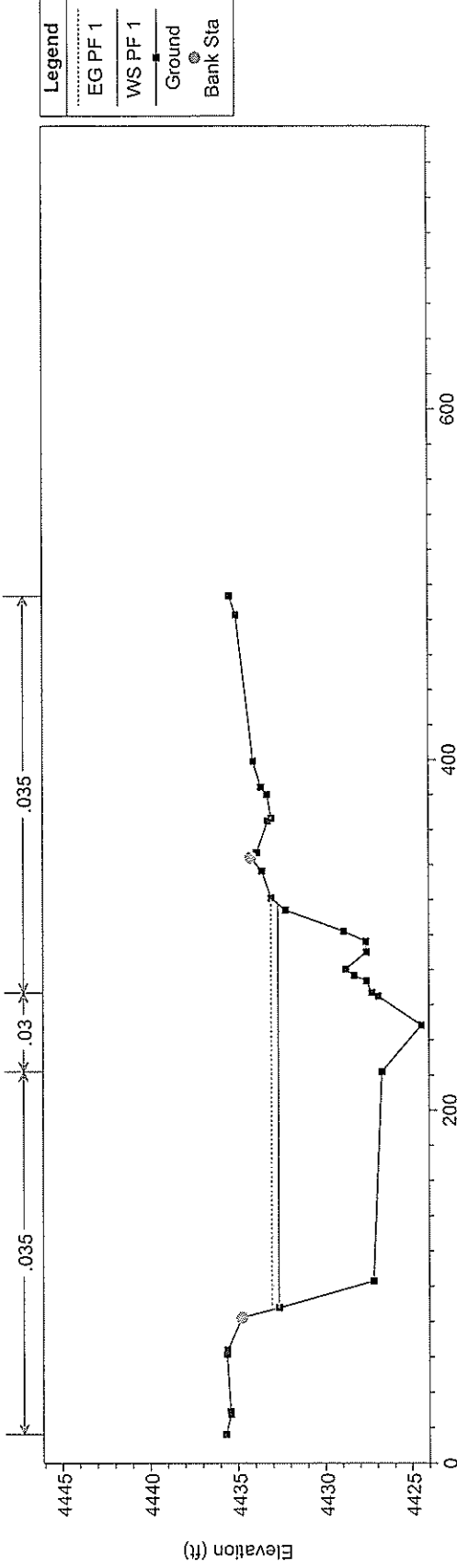
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 23



From as-built topo Plan: LOMR Submittal 1/8/2008

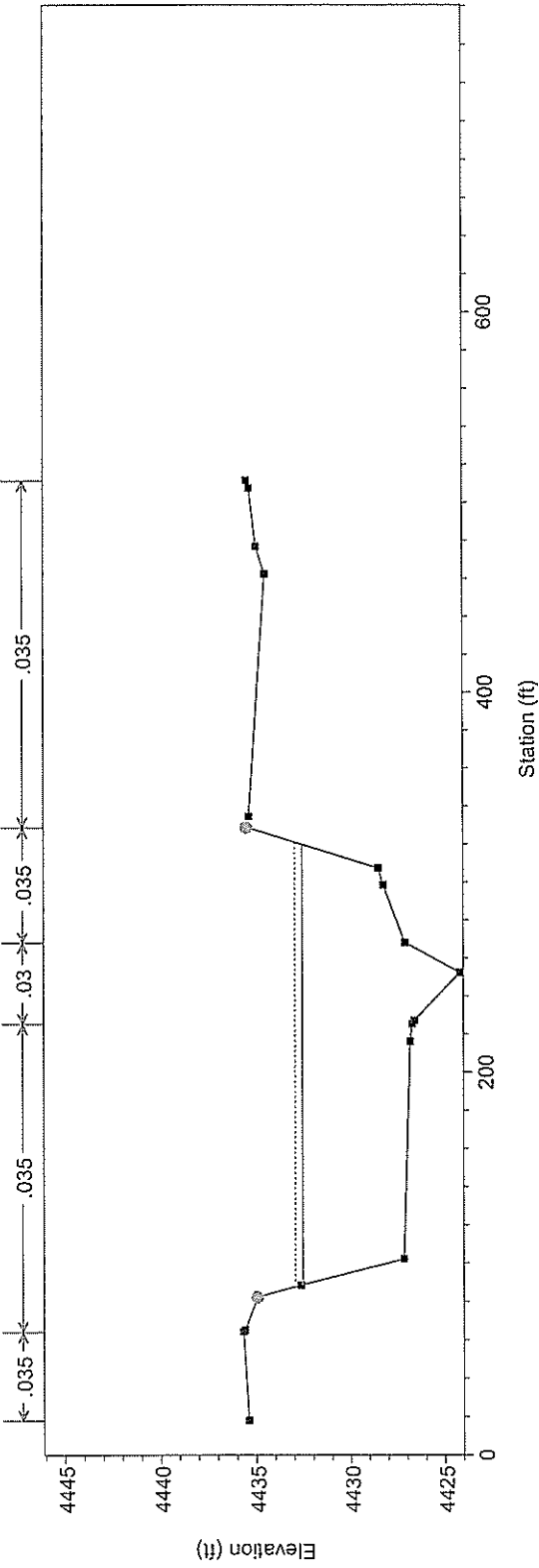
River = Steamboat Reach = Bella Vista RS = 22



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

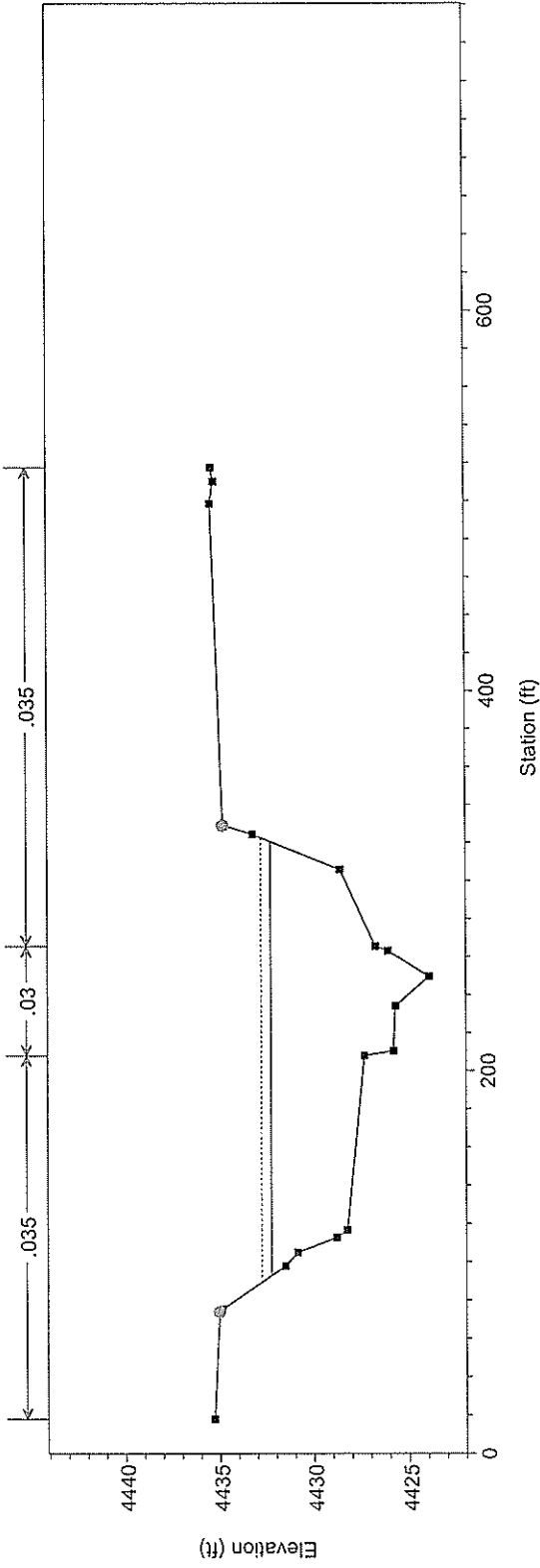
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 21



From as-built topo Plan: LOMR Submittal 1/8/2008

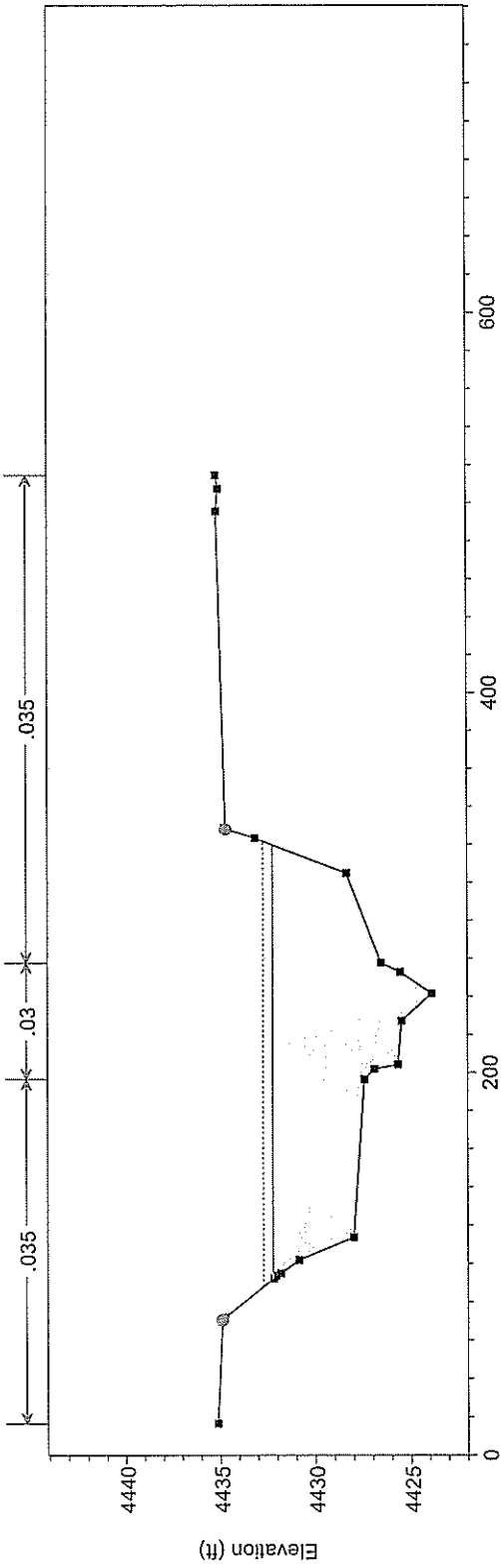
River = Steamboat Reach = Bella Vista RS = 20



1 in Horiz. = 100 ft 1 in Vert. = 10 ft

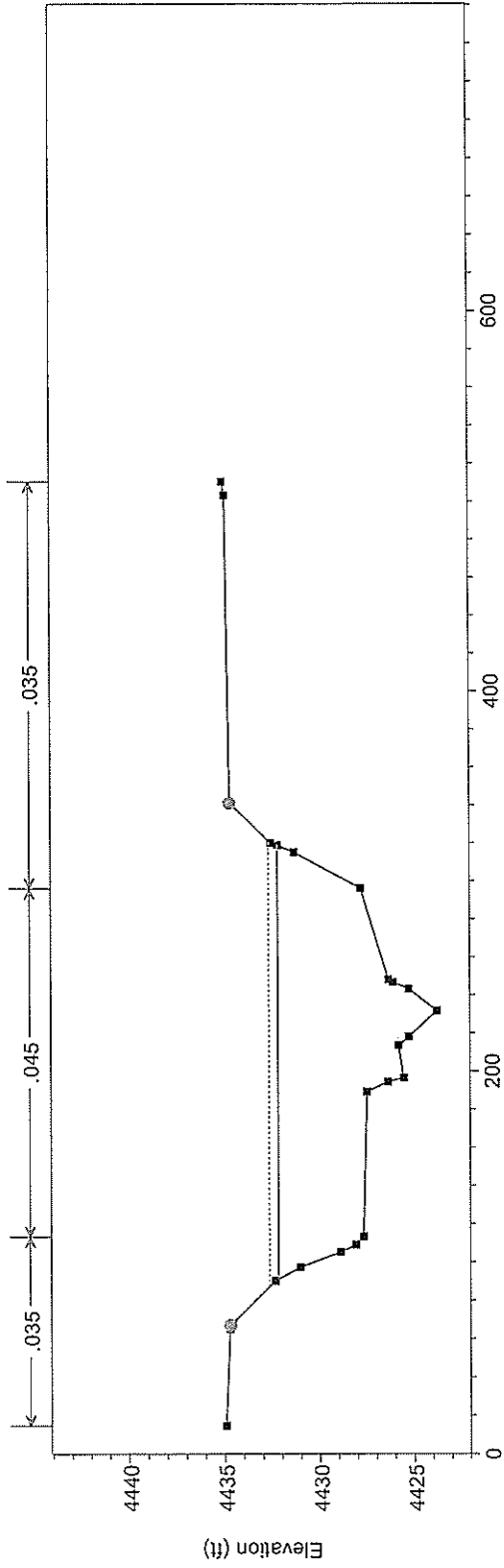
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 19.8



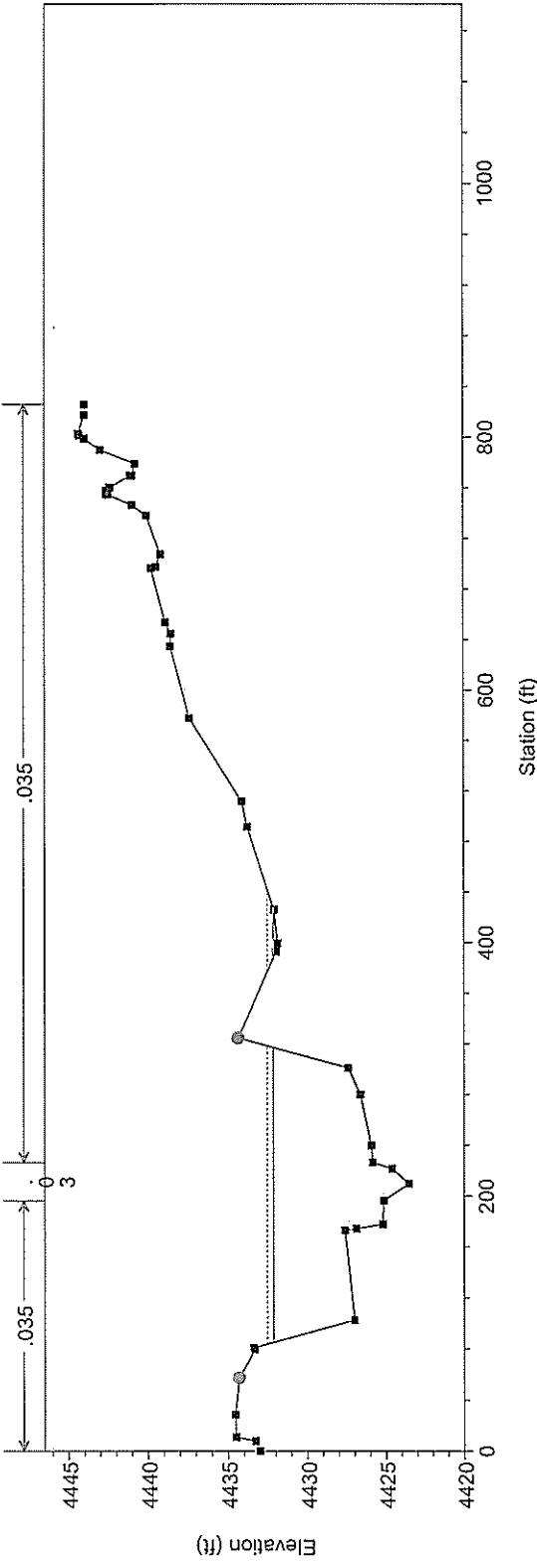
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 19.55



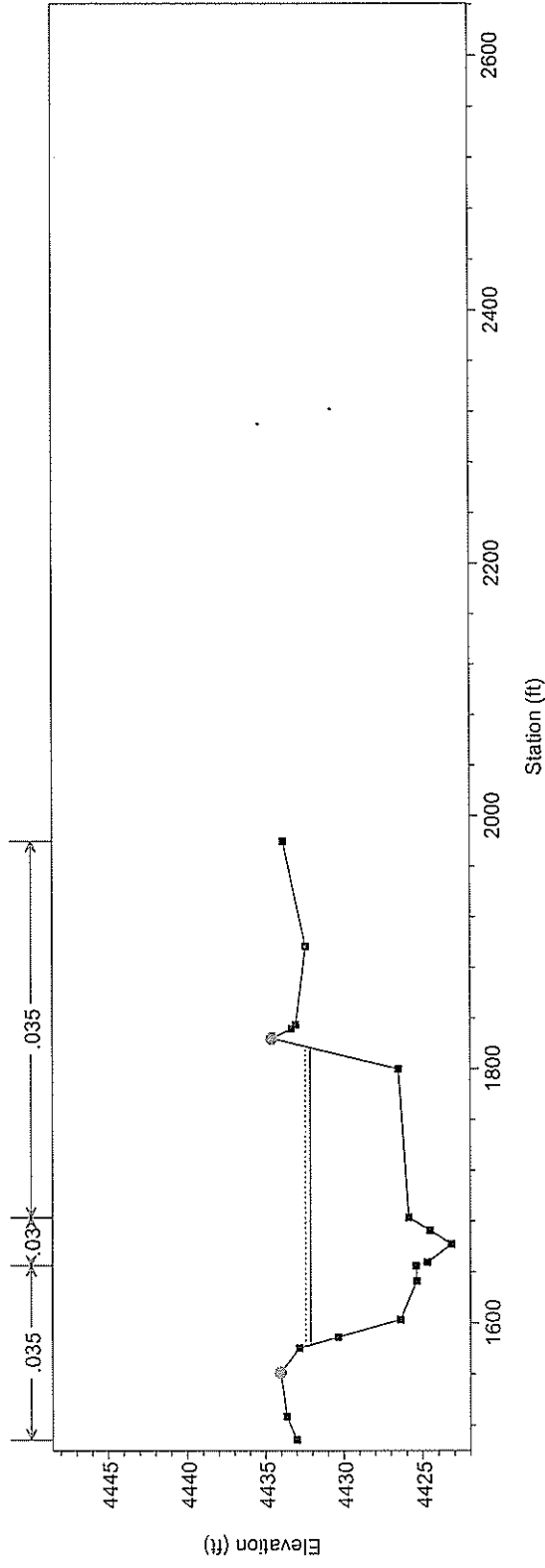
1 in Horiz. = 100 ft 1 in Vert. = 10 ft

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 19



Legend
 EG PF 1
 WS PF 1
 Ground
 Bank Sta

From as-built topo Plan: LOMR Submittal 1/8/2008
 River = Steamboat Reach = Bella Vista RS = 18.25

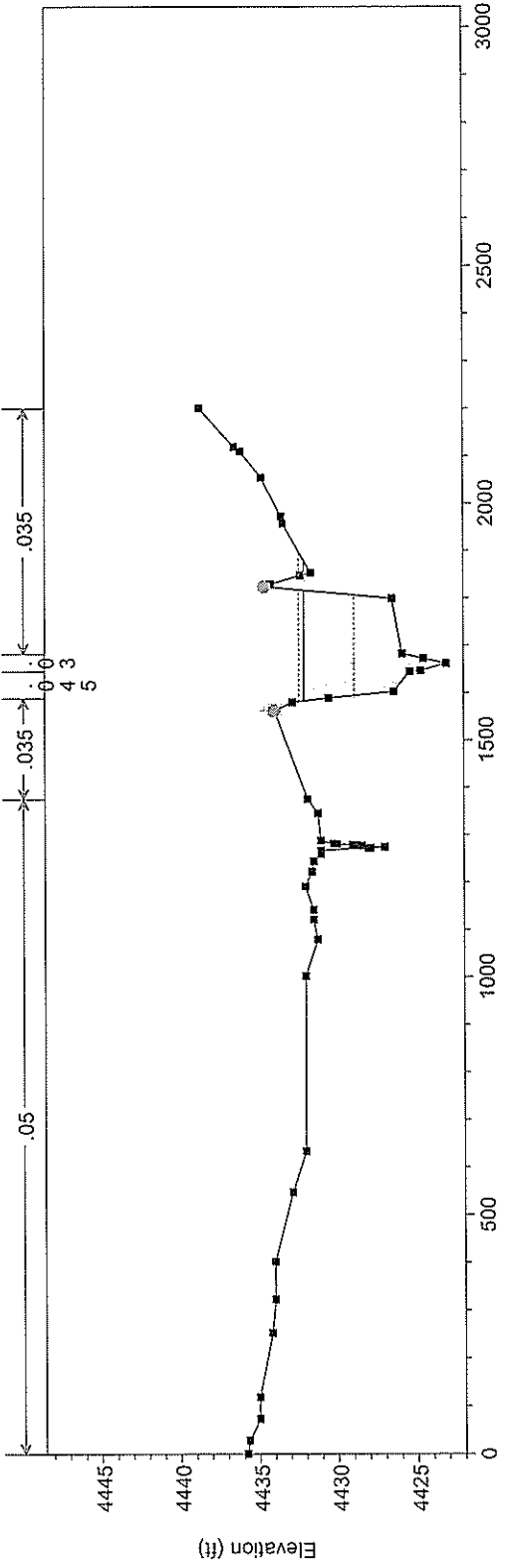


Legend
 EG PF 1
 WS PF 1
 Ground
 Bank Sta

1 in Horiz. = 150 ft 1 in Vert. = 12 ft

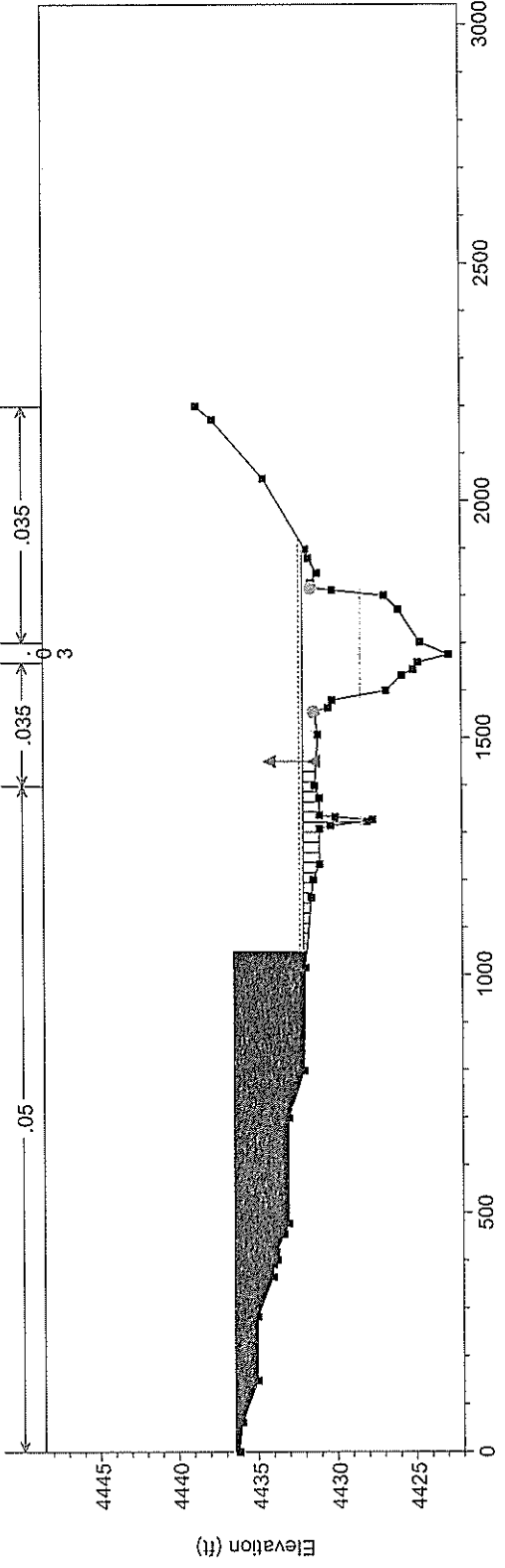
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 18



From as-built topo Plan: LOMR Submittal 1/8/2008

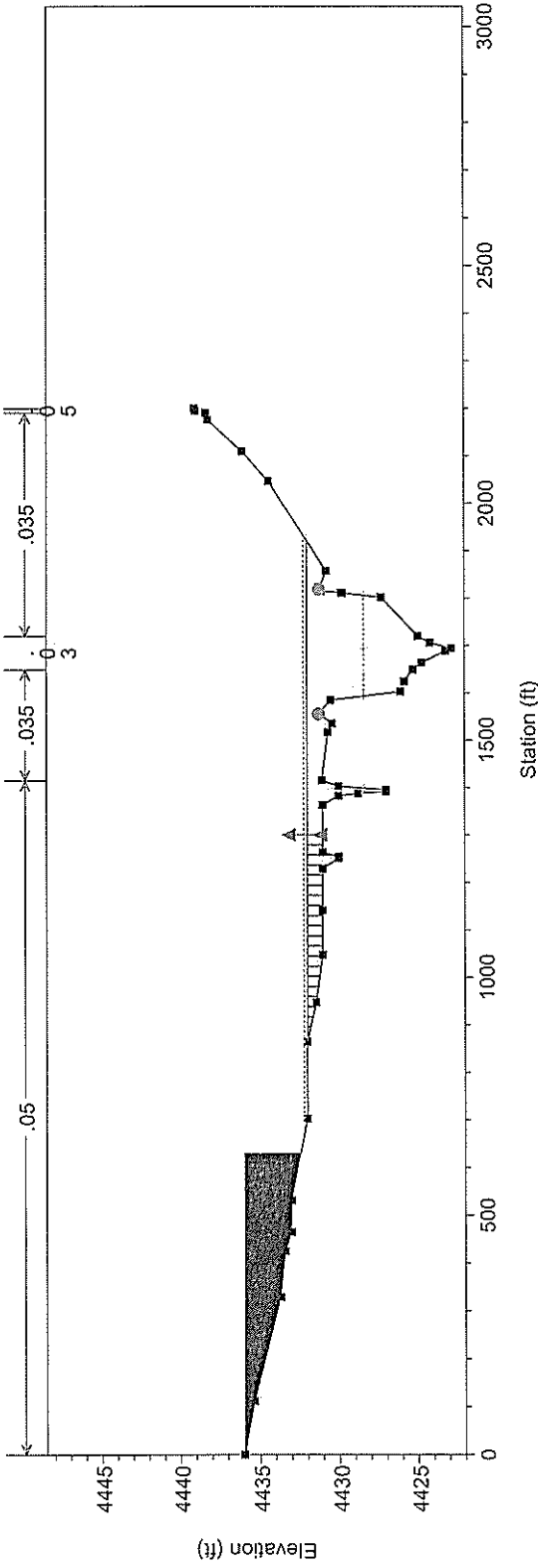
River = Steamboat Reach = Bella Vista RS = 17



1 in Horiz. = 400 ft 1 in Vert. = 12 ft

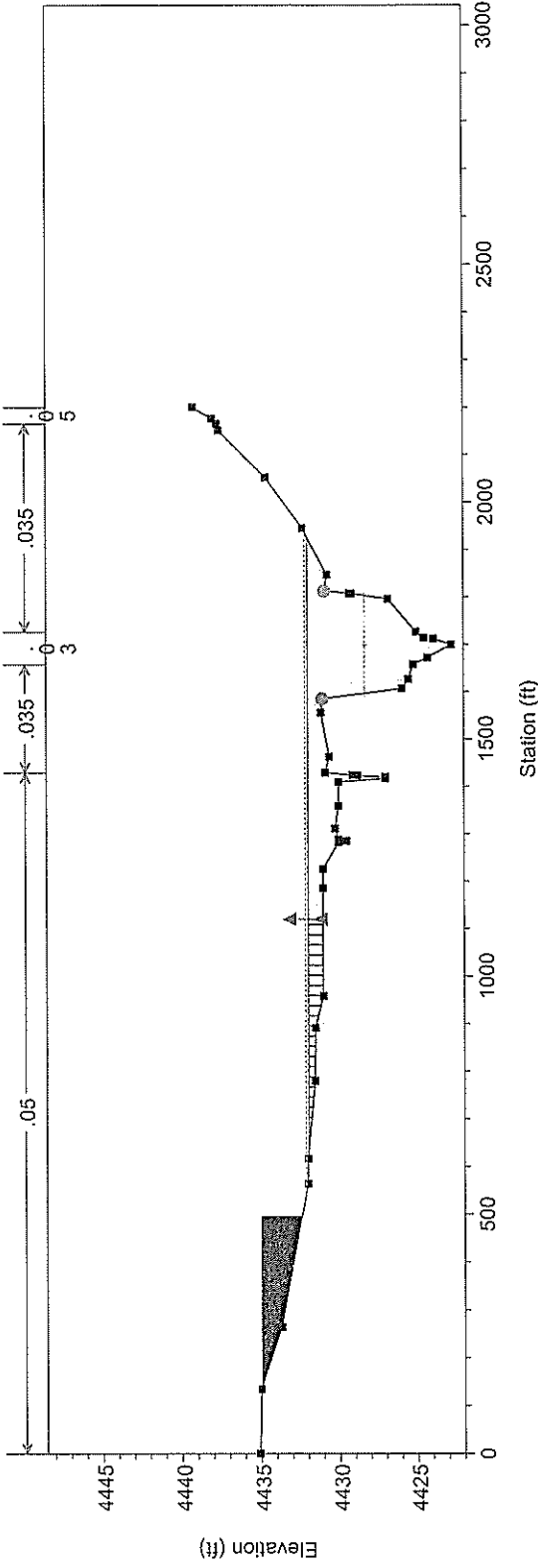
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 16



From as-built topo Plan: LOMR Submittal 1/8/2008

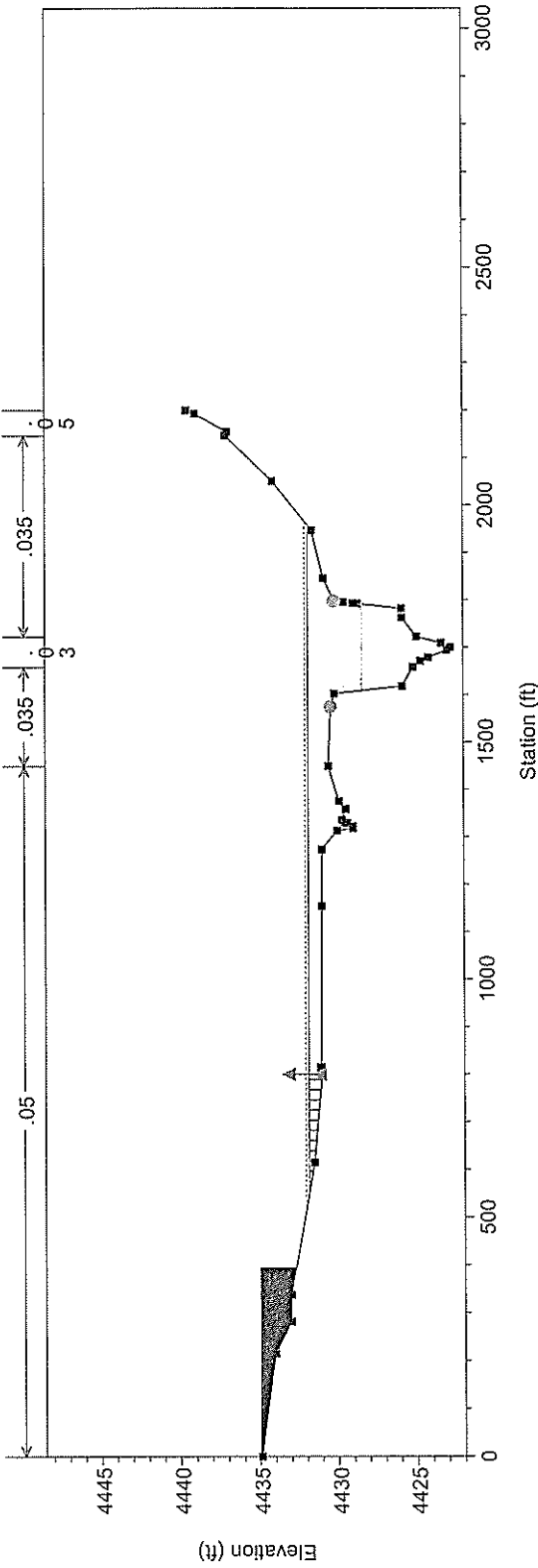
River = Steamboat Reach = Bella Vista RS = 15



1 in Horiz. = 400 ft 1 in Vert. = 12 ft

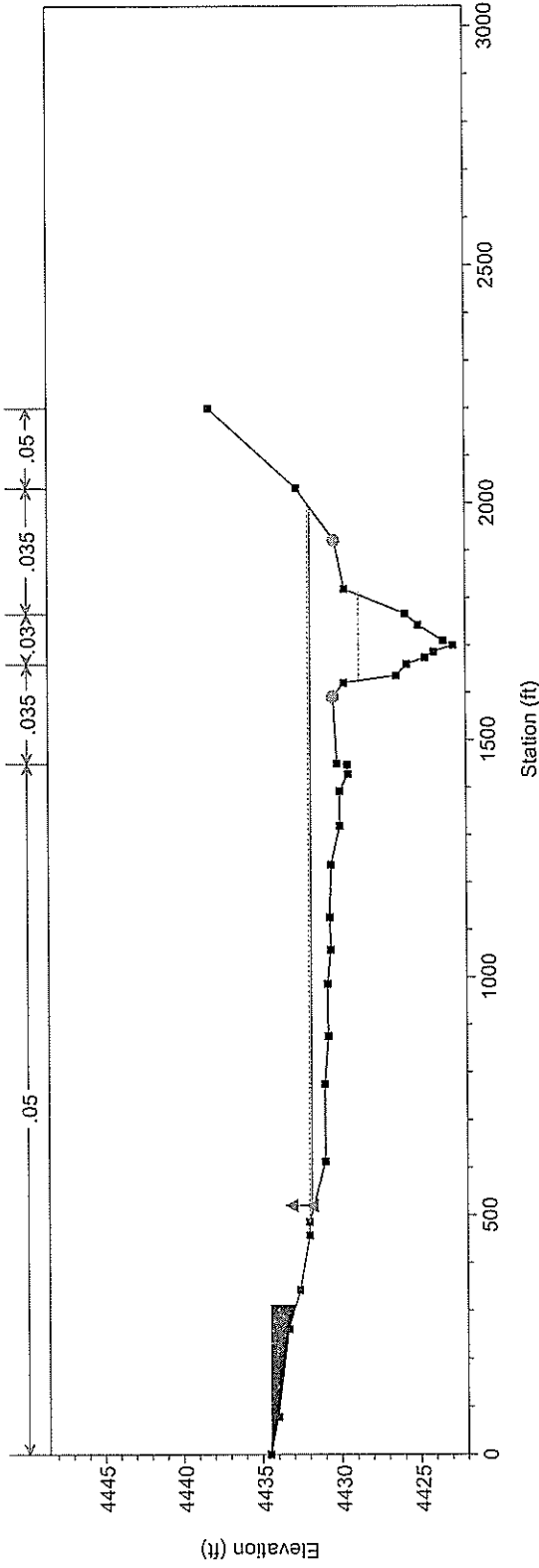
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 14



From as-built topo Plan: LOMR Submittal 1/8/2008

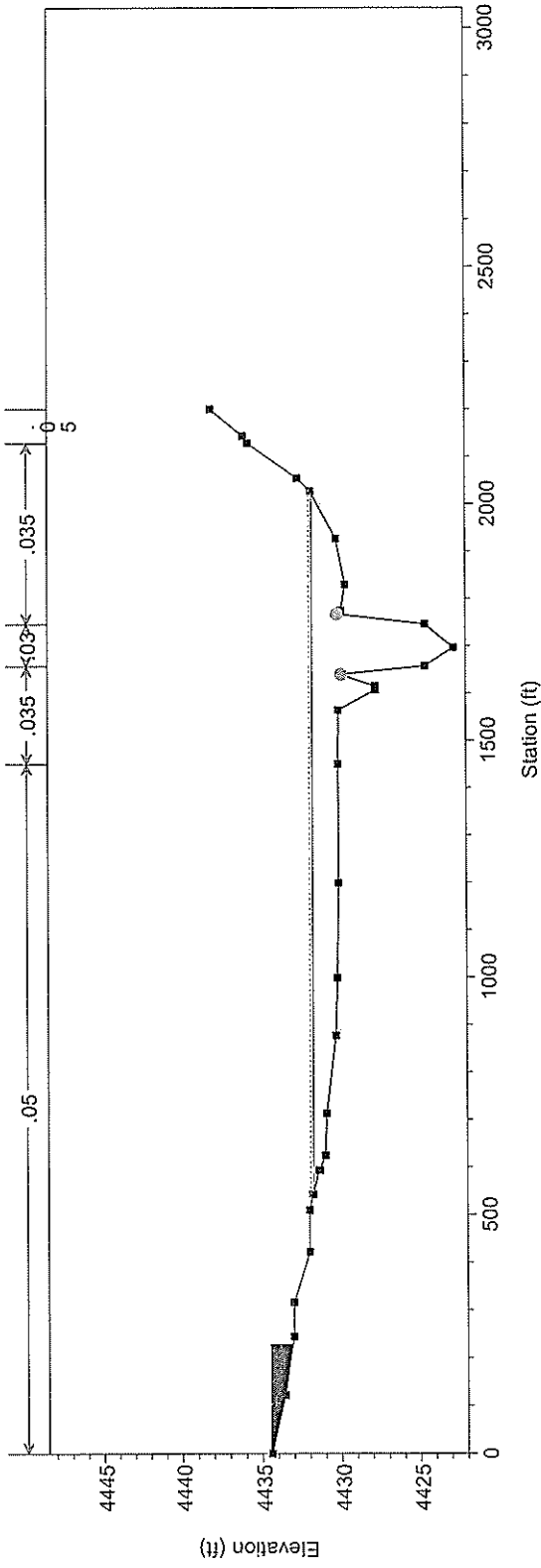
River = Steamboat Reach = Bella Vista RS = 13



1 in Horiz. = 400 ft 1 in Vert. = 12 ft

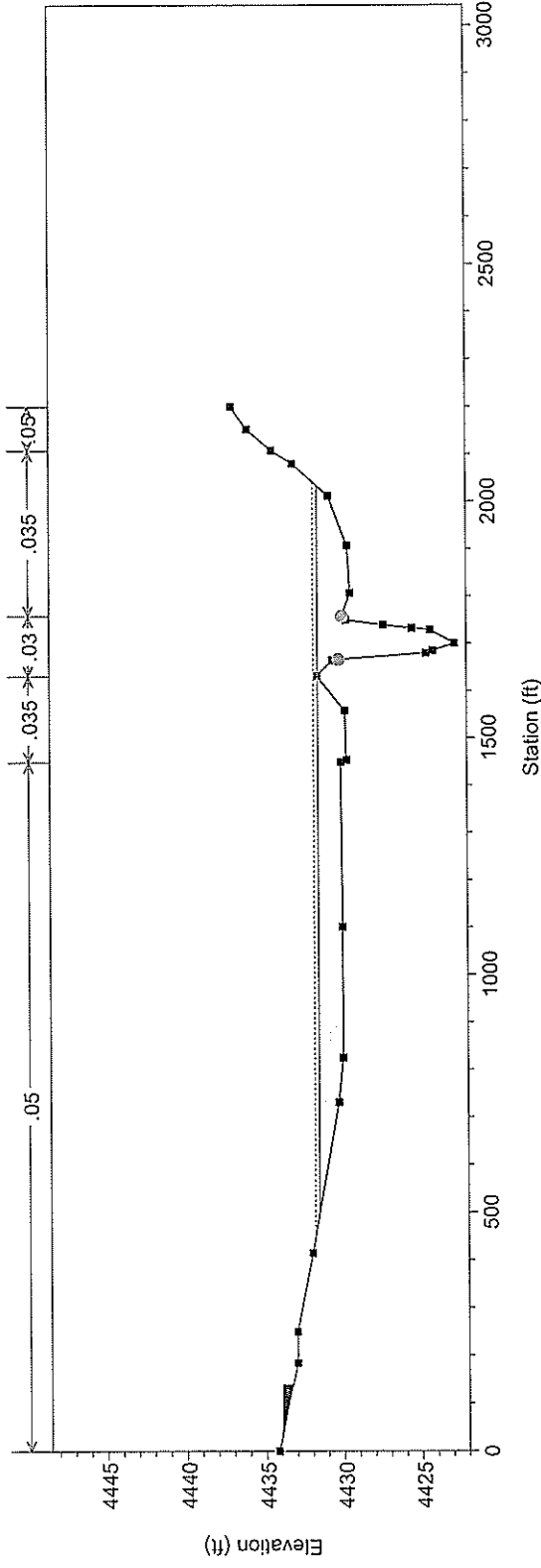
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 12



From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 11



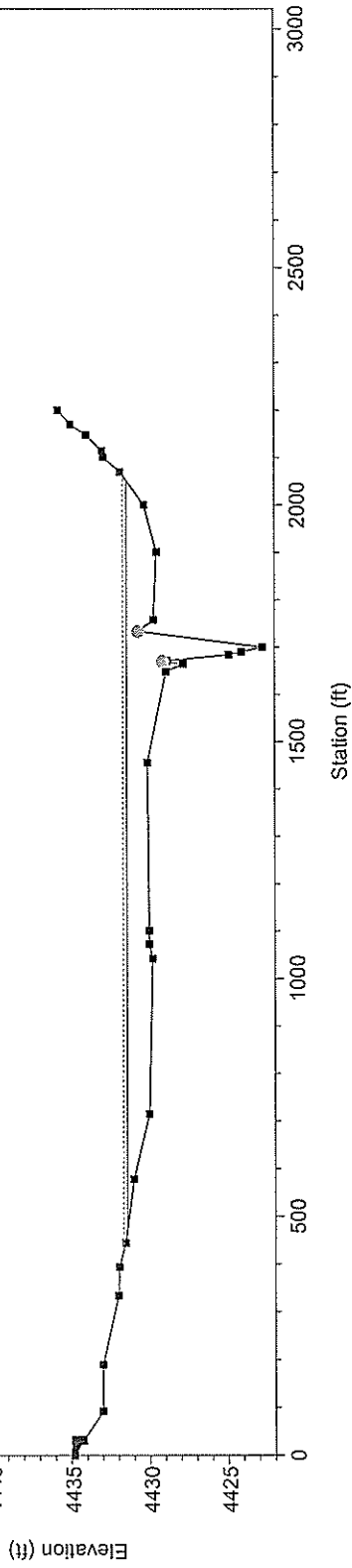
1 in Horiz. = 400 ft 1 in Vert. = 12 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 10



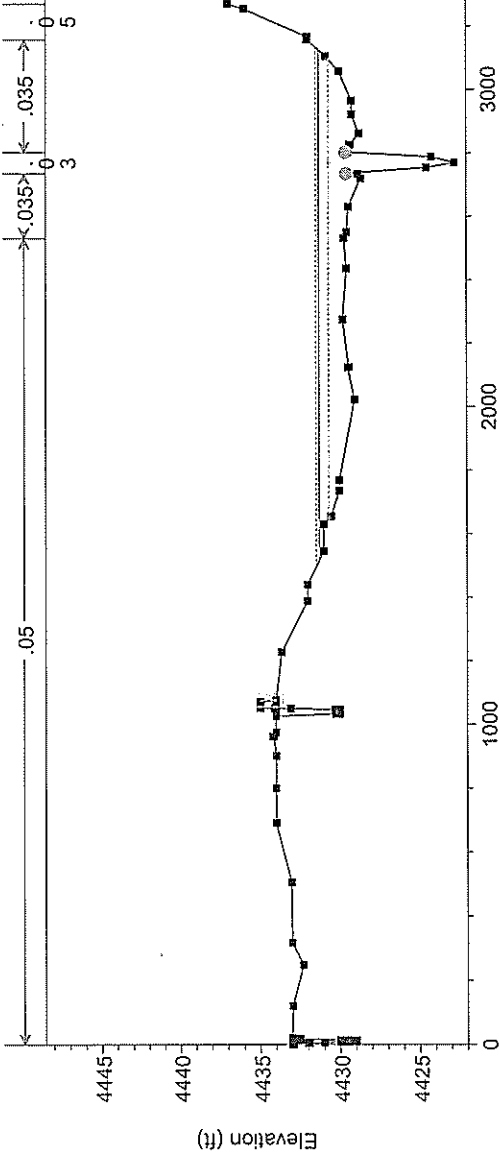
Legend	
-----	EG PF 1
-----	WS PF 1
—■—	Ground
⊙	Bank Sta



1 in Horiz. = 400 ft 1 in Vert. = 12 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

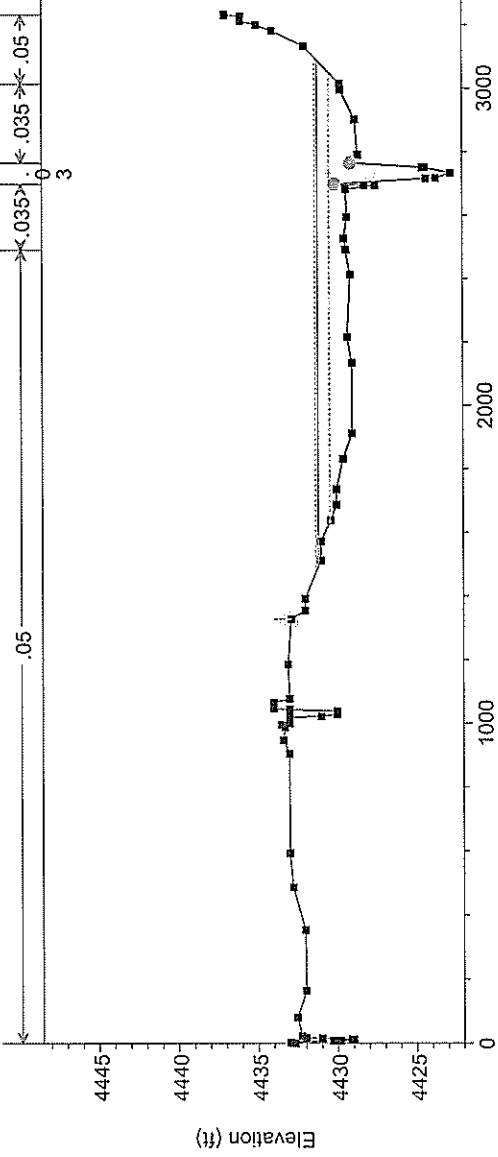
River = Steamboat Reach = Bella Vista RS = 9



Legend	
EG PF 1	-----
WS PF 1	-----
Crit PF 1	-----
Ground	—■—
Levee	—○—
Bank Sta	●

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 8

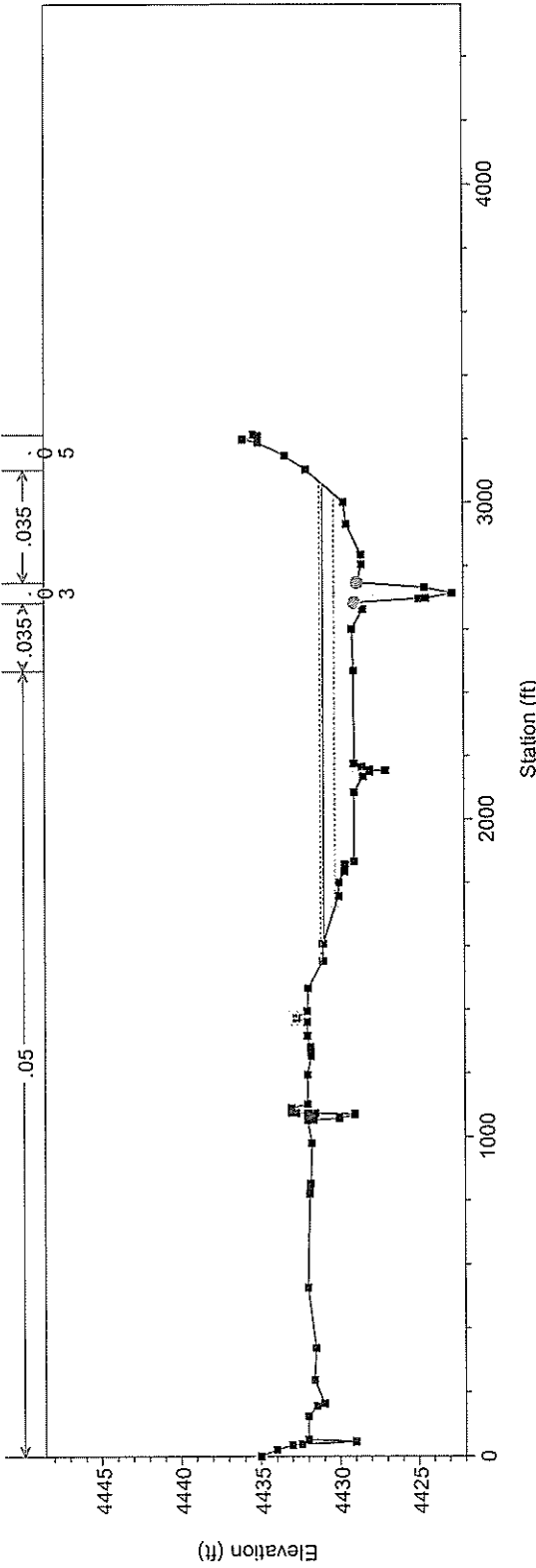


Legend	
EG PF 1	-----
WS PF 1	-----
Crit PF 1	-----
Ground	—■—
Levee	—○—
Bank Sta	●

1 in Horiz. = 600 ft 1 in Vert. = 12 ft

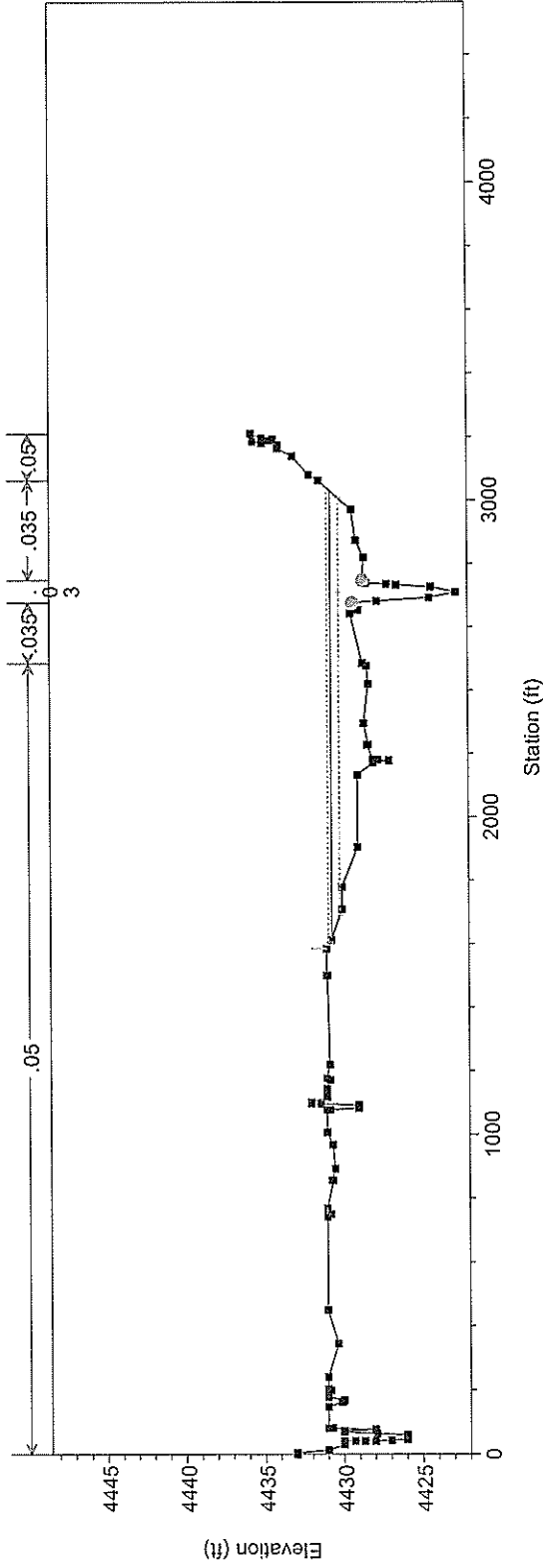
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 7



From as-built topo Plan: LOMR Submittal 1/8/2008

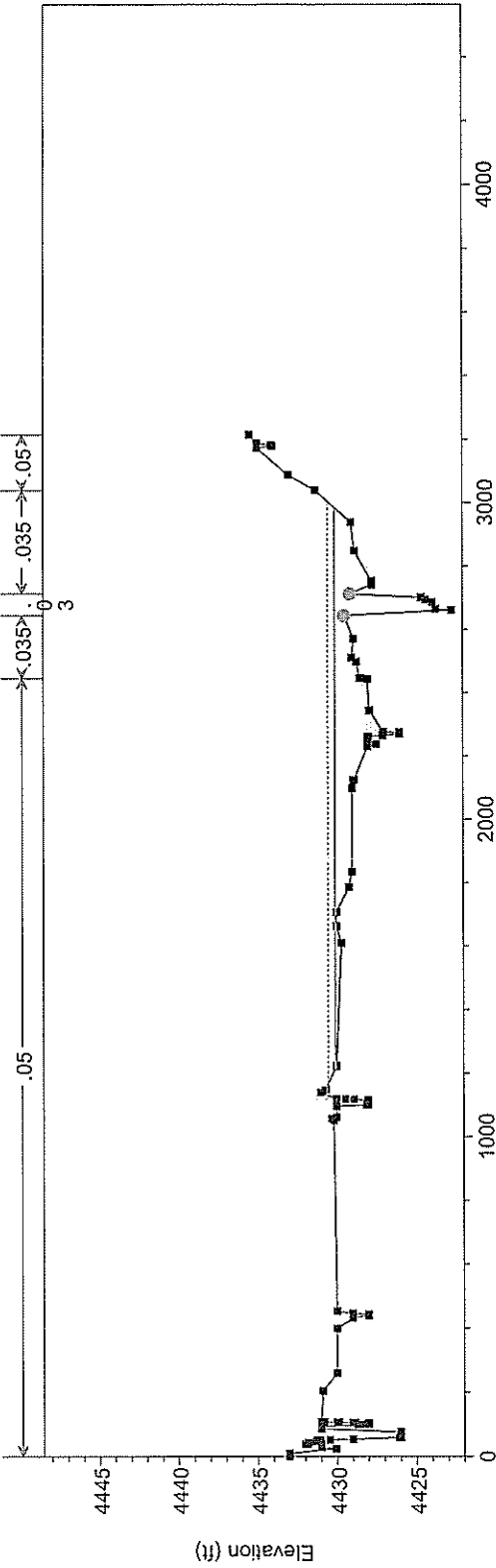
River = Steamboat Reach = Bella Vista RS = 6



1 in Horiz. = 600 ft 1 in Vert. = 12 ft

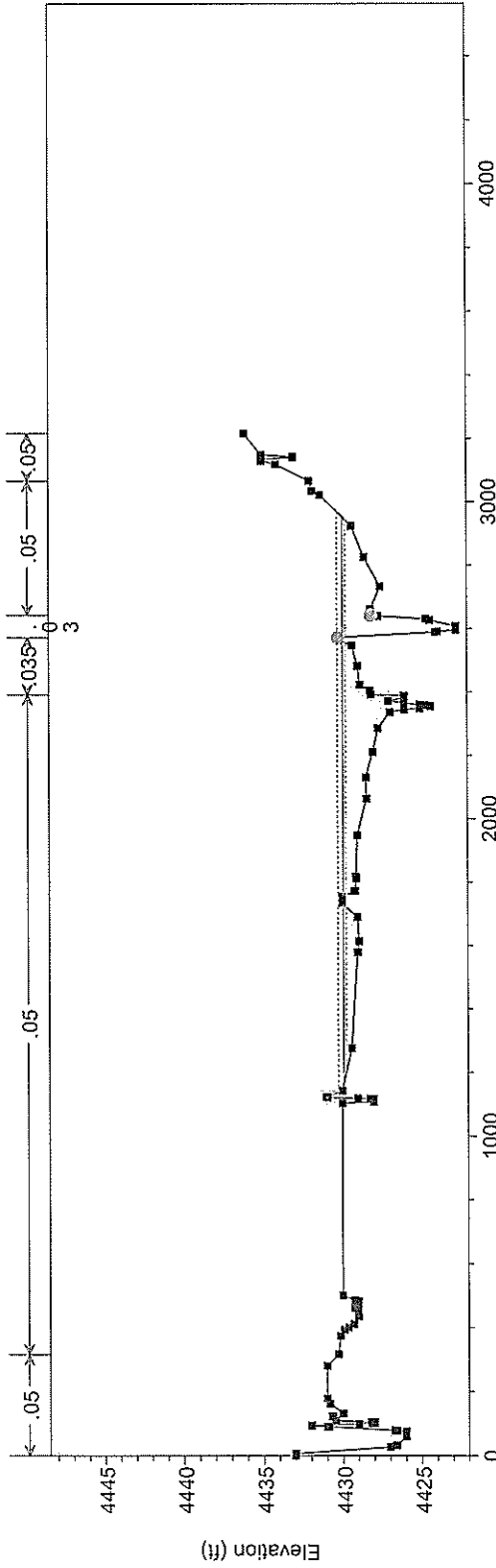
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 5



From as-built topo Plan: LOMR Submittal 1/8/2008

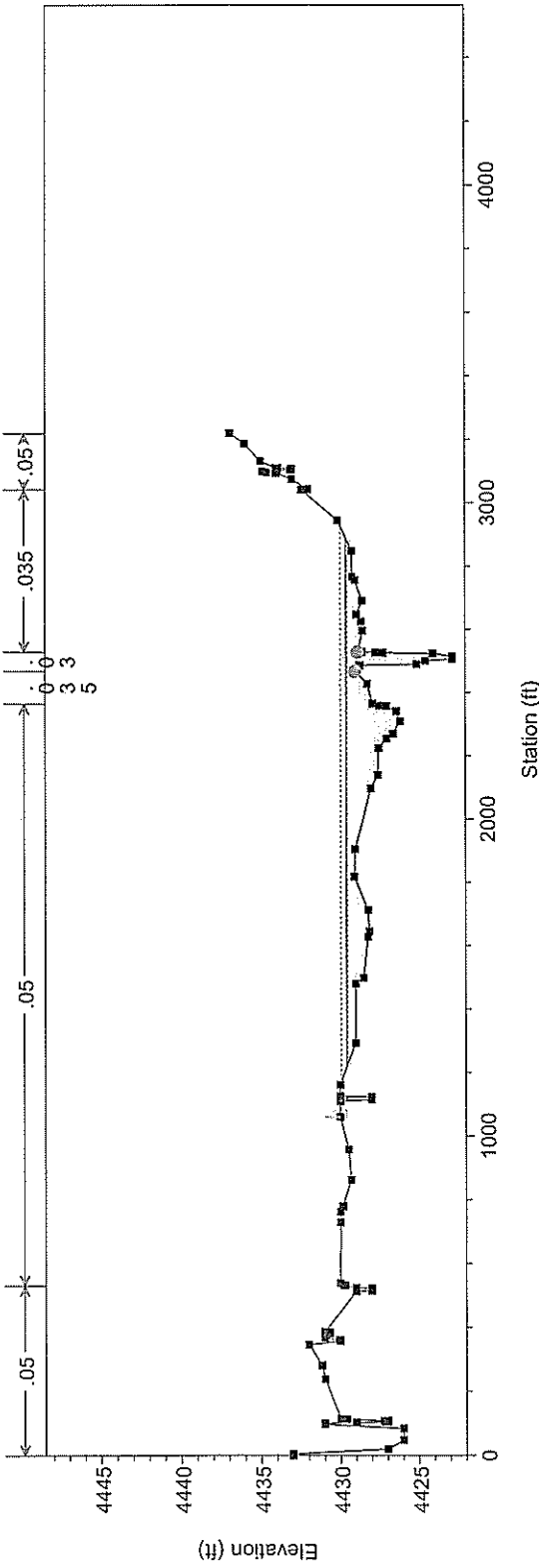
River = Steamboat Reach = Bella Vista RS = 4



1 in Horiz. = 600 ft 1 in Vert. = 12 ft

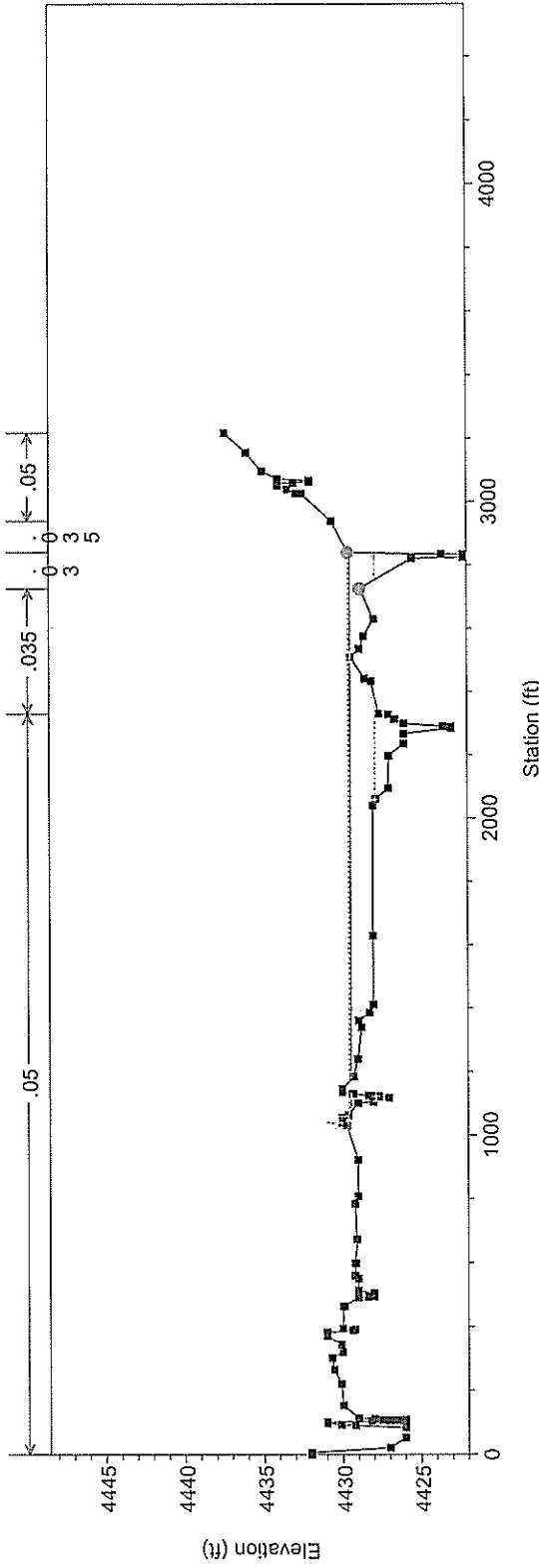
From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 3



From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 2



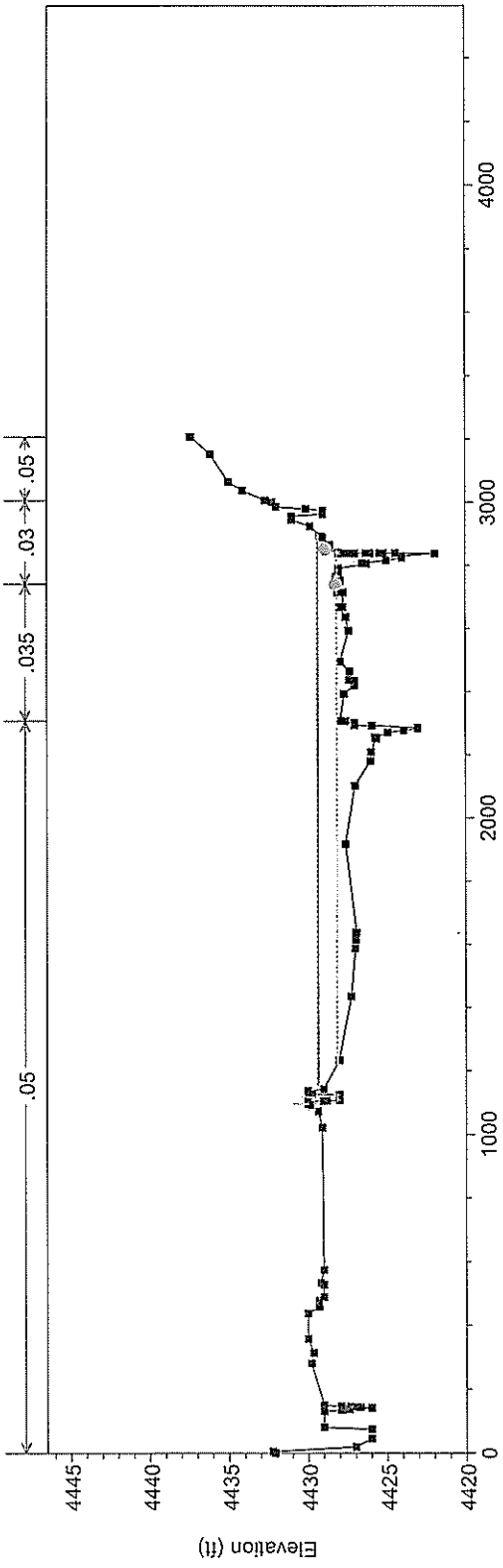
1 in Horiz. = 600 ft 1 in Vert. = 12 ft

From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = 1



Legend	
.....	EG PF 1
-----	WS PF 1
-----	Crit PF 1
-----	Ground
-----	Levee
●	Bank Sta

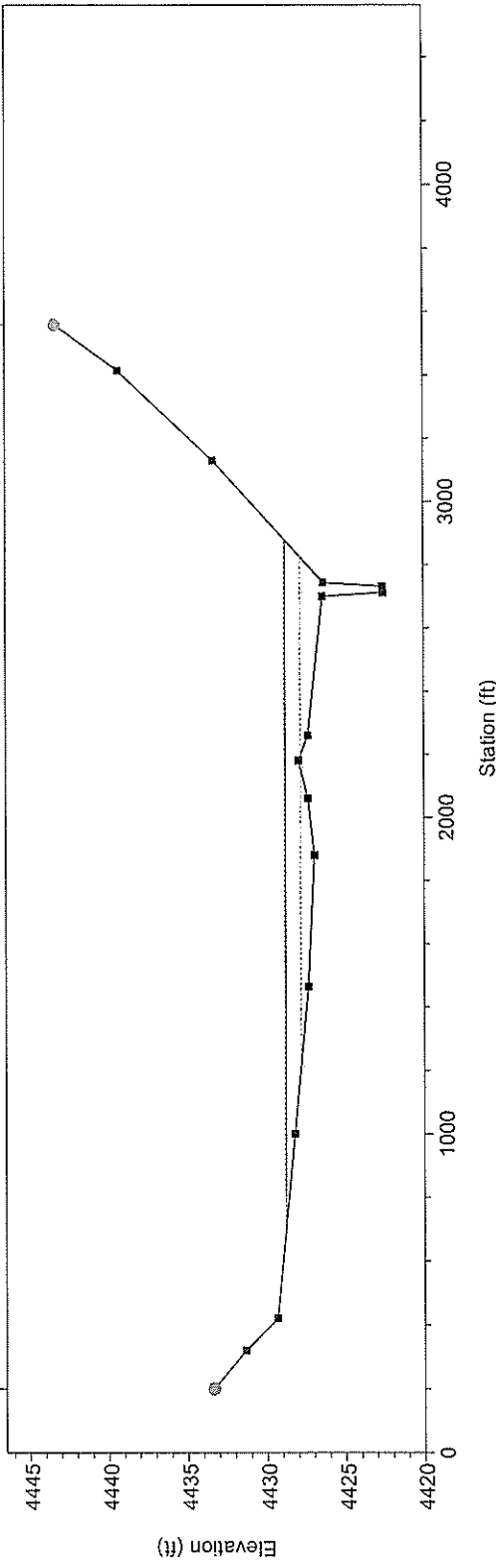


From as-built topo Plan: LOMR Submittal 1/8/2008

River = Steamboat Reach = Bella Vista RS = .225 From Old Damonte LOMR



Legend	
.....	EG PF 1
-----	WS PF 1
-----	Crit PF 1
-----	Ground
●	Bank Sta



1 in Horiz. = 600 ft 1 in Vert. = 12 ft

HEC-RAS Plan: DamVStm River: RIVER-1 Reach: Reach-1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Cnl
Reach-1	16	PF 1	2762.00	4449.00	4454.69	4452.88	4454.94	0.002158	3.96	696.91	199.13	0.37
Reach-1	16	PF 2	2194.00	4449.00	4454.22	4452.56	4454.43	0.002142	3.63	603.59	195.34	0.36
Reach-1	15	PF 1	2762.00	4449.00	4454.14	4452.39	4454.38	0.002172	3.87	713.12	212.09	0.37
Reach-1	15	PF 2	2194.00	4449.00	4453.68	4452.11	4453.88	0.002107	3.55	617.26	204.14	0.36
Reach-1	14	PF 1	2762.00	4448.80	4453.61	4452.07	4453.88	0.002600	4.15	665.31	204.12	0.41
Reach-1	14	PF 2	2194.00	4448.80	4453.15	4451.75	4453.38	0.002628	3.83	573.36	200.45	0.40
Reach-1	13	PF 1	2762.00	4448.50	4453.54	4451.53	4453.75	0.001705	3.65	756.81	204.92	0.33
Reach-1	13	PF 2	2194.00	4448.50	4453.09	4451.25	4453.26	0.001619	3.30	664.59	201.25	0.32
Reach-1	12	PF 1	2762.00	4447.81	4453.30	4451.00	4453.49	0.001428	3.50	788.59	198.95	0.31
Reach-1	12	PF 2	2194.00	4447.81	4452.87	4450.65	4453.02	0.001289	3.12	703.08	195.46	0.29
Reach-1	11	PF 1	2762.00	4448.23	4452.72	4451.47	4453.10	0.003662	4.96	556.33	175.55	0.49
Reach-1	11	PF 2	2194.00	4448.23	4452.36	4451.13	4452.67	0.003544	4.44	493.84	172.68	0.46
Reach-1	10	PF 1	2762.00	4447.00	4452.14	4450.66	4452.34	0.002300	3.64	758.71	257.89	0.37
Reach-1	10	PF 2	2194.00	4447.00	4451.81	4450.38	4451.98	0.002113	3.25	675.12	255.41	0.35
Reach-1	9	PF 1	2762.00	4446.88	4450.17	4450.17	4450.84	0.021243	6.56	421.27	315.73	1.00
Reach-1	9	PF 2	2194.00	4446.88	4449.93	4449.93	4450.55	0.022425	6.32	347.36	286.73	1.01
Reach-1	8	PF 1	2762.00	4443.82	4446.25	4445.13	4446.34	0.001799	2.31	1196.72	674.57	0.31
Reach-1	8	PF 2	2194.00	4443.82	4446.04	4444.99	4446.11	0.001722	2.09	1051.01	666.63	0.29
Reach-1	7	PF 1	2762.00	4443.40	4445.45	4445.45	4445.60	0.004495	3.01	916.28	688.12	0.46
Reach-1	7	PF 2	2194.00	4443.40	4445.26	4445.26	4445.38	0.004523	2.79	785.24	663.84	0.45
Reach-1	6	PF 1	2762.00	4442.00	4444.72	4444.72	4444.80	0.002302	2.24	1233.11	874.95	0.33
Reach-1	6	PF 2	2194.00	4442.00	4444.51	4444.51	4444.58	0.002335	2.08	1057.08	850.00	0.33
Reach-1	5	PF 1	2762.00	4441.43	4444.42	4444.42	4444.45	0.000602	1.32	2086.88	1191.85	0.18
Reach-1	5	PF 2	2194.00	4441.43	4444.24	4444.24	4444.26	0.000524	1.17	1875.50	1161.57	0.16
Reach-1	4	PF 1	2762.00	4441.95	4444.31	4444.31	4444.33	0.000463	1.24	2221.36	1182.00	0.16
Reach-1	4	PF 2	2194.00	4441.95	4444.14	4444.14	4444.16	0.000389	1.08	2034.69	1139.28	0.14

HEC-RAS Plan: DamVStm River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach-1	3	PF 1	2762.00	4441.00	4444.23		4444.25	0.000433	1.16	2388.33	1304.56	0.15
Reach-1	3	PF 2	2194.00	4441.00	4444.08		4444.10	0.000358	1.00	2197.64	1299.05	0.14
Reach-1	2	PF 1	2762.00	4441.00	4444.18		4444.19	0.000261	0.99	2781.10	1304.58	0.12
Reach-1	2	PF 2	2194.00	4441.00	4444.04		4444.05	0.000201	0.84	2604.62	1286.27	0.10
Reach-1	1.6	PF 1	2762.00	4441.00	4444.17		4444.19	0.000259	1.00	2771.32	1286.59	0.12
Reach-1	1.6	PF 2	2194.00	4441.00	4444.04		4444.05	0.000199	0.84	2598.34	1269.75	0.10
Reach-1	1.5	PF 1	2762.00	4442.64	4443.84	4443.84	4444.15	0.027422	4.46	618.79	1001.06	1.00
Reach-1	1.5	PF 2	2194.00	4442.64	4443.73	4443.73	4444.01	0.029065	4.25	515.66	936.39	1.01
Reach-1	1.4	PF 1	2762.00	4441.00	4442.98	4442.42	4443.08	0.004024	2.57	1073.82	941.55	0.42
Reach-1	1.4	PF 2	2194.00	4441.00	4442.81	4442.30	4442.90	0.004071	2.39	918.88	908.69	0.42
Reach-1	1	PF 1	2762.00	4440.00	4442.80		4442.86	0.001627	1.90	1453.62	1017.19	0.28
Reach-1	1	PF 2	2194.00	4440.00	4442.65		4442.70	0.001412	1.68	1302.42	981.53	0.26
Reach-1	0.5	PF 1	2762.00	4439.82	4442.79	4441.31	4442.82	0.000337	1.27	2333.43	1610.98	0.16
Reach-1	0.5	PF 2	2194.00	4439.82	4442.64	4441.23	4442.66	0.000281	1.11	2106.22	1531.67	0.14
Reach-1	0.35	PF 1	2762.00	4441.47	4442.61	4442.28	4442.73	0.004210	2.14	1034.93	1222.13	0.46
Reach-1	0.35	PF 2	2194.00	4441.47	4442.48	4442.17	4442.58	0.004307	1.93	874.73	1156.15	0.45
Reach-1	.2	PF 1	2762.00	4439.84	4441.17	4441.17	4441.55	0.034325	4.94	559.24	770.97	1.02
Reach-1	.2	PF 2	2194.00	4439.84	4441.05	4441.05	4441.39	0.034333	4.66	471.16	709.59	1.01

HEC-RAS Plan: DamVStm River: RIVER-1 Reach: Reach-1

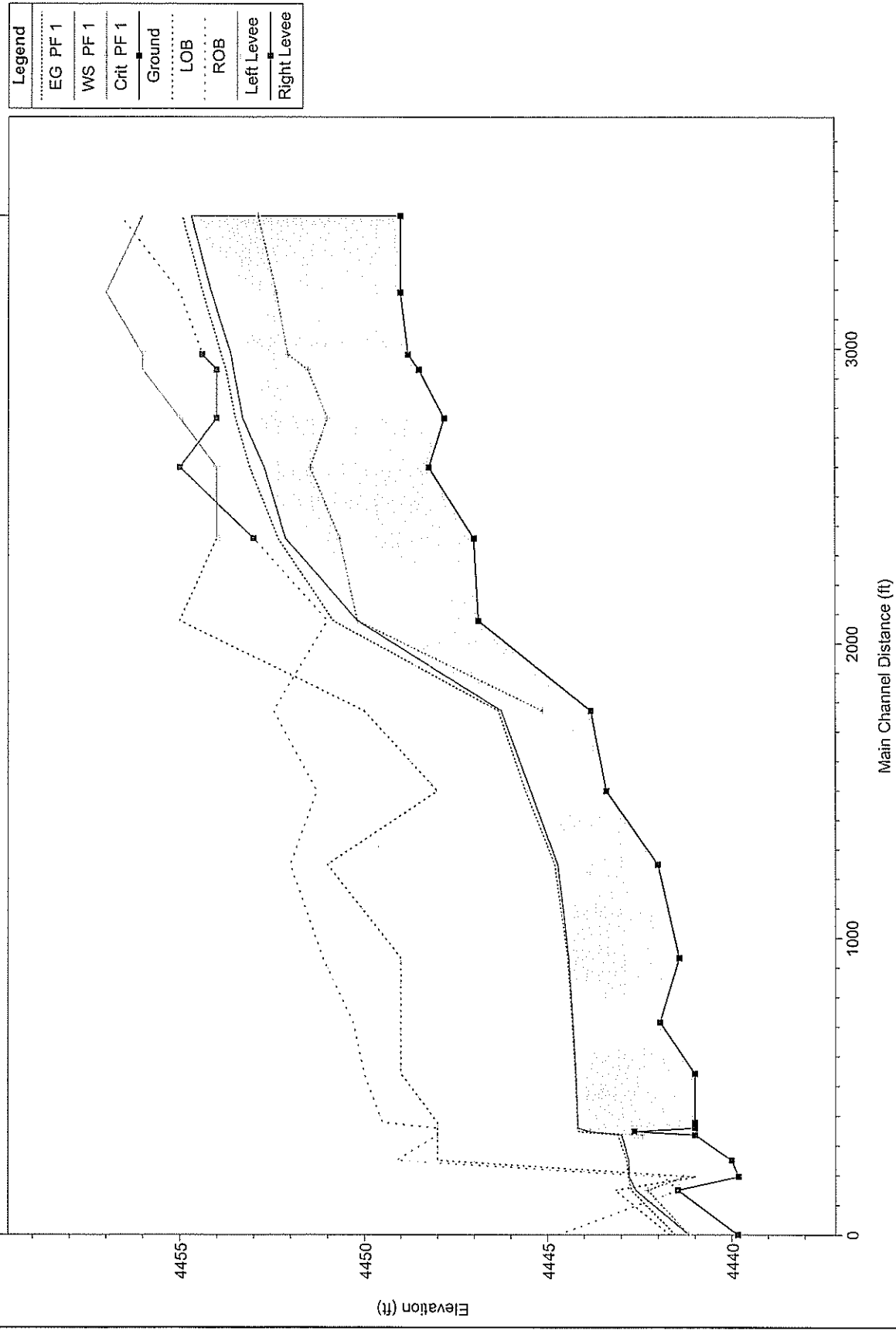
Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frctn Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Reach-1	16	PF 1	4454.94	4454.69	0.24	0.56	0.00		2762.00		199.13
Reach-1	16	PF 2	4454.43	4454.22	0.21	0.55	0.00		2194.00		195.34
Reach-1	15	PF 1	4454.38	4454.14	0.23	0.50	0.00		2762.00		212.09
Reach-1	15	PF 2	4453.88	4453.68	0.20	0.49	0.00		2194.00		204.14
Reach-1	14	PF 1	4453.88	4453.61	0.27	0.11	0.02		2762.00		204.12
Reach-1	14	PF 2	4453.38	4453.15	0.23	0.11	0.02		2194.00		200.45
Reach-1	13	PF 1	4453.75	4453.54	0.21	0.25	0.00		2762.00		204.92
Reach-1	13	PF 2	4453.26	4453.09	0.17	0.24	0.01		2194.00		201.25
Reach-1	12	PF 1	4453.49	4453.30	0.19	0.37	0.02		2762.00		198.95
Reach-1	12	PF 2	4453.02	4452.87	0.15	0.33	0.02		2194.00		195.46
Reach-1	11	PF 1	4453.10	4452.72	0.38	0.71	0.05		2762.00		175.55
Reach-1	11	PF 2	4452.67	4452.36	0.31	0.65	0.04		2194.00		172.68
Reach-1	10	PF 1	4452.34	4452.14	0.21	1.46	0.05		2762.00		257.89
Reach-1	10	PF 2	4451.98	4451.81	0.16	1.38	0.05		2194.00		255.41
Reach-1	9	PF 1	4450.84	4450.17	0.67	1.32	0.18		2762.00		315.73
Reach-1	9	PF 2	4450.55	4449.93	0.62	1.29	0.17		2194.00		286.73
Reach-1	8	PF 1	4446.34	4446.25	0.08	0.74	0.01		2762.00		674.57
Reach-1	8	PF 2	4446.11	4446.04	0.07	0.72	0.01		2194.00		666.63
Reach-1	7	PF 1	4445.60	4445.45	0.14	0.78	0.02		2762.00		688.12
Reach-1	7	PF 2	4445.38	4445.26	0.12	0.79	0.02		2194.00		663.84
Reach-1	6	PF 1	4444.80	4444.72	0.08	0.33	0.02		2762.00		874.95
Reach-1	6	PF 2	4444.58	4444.51	0.07	0.31	0.01		2194.00		850.00
Reach-1	5	PF 1	4444.45	4444.42	0.03	0.12	0.00		2762.00		1191.85
Reach-1	5	PF 2	4444.26	4444.24	0.02	0.10	0.00		2194.00		1161.57

HEC-RAS Plan: DamVStm River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Profile	E.G. Elev (ft)	W.S. Elev (ft)	Vel Head (ft)	Frctn Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Reach-1	4	PF 1	4444.33	4444.31	0.02	0.08	0.00		2762.00		1182.00
Reach-1	4	PF 2	4444.16	4444.14	0.02	0.06	0.00		2194.00		1139.28
Reach-1	3	PF 1	4444.25	4444.23	0.02	0.05	0.00		2762.00		1304.56
Reach-1	3	PF 2	4444.10	4444.08	0.02	0.04	0.00		2194.00		1299.05
Reach-1	2	PF 1	4444.19	4444.18	0.02	0.00	0.00		2762.00		1304.58
Reach-1	2	PF 2	4444.05	4444.04	0.01	0.00	0.00		2194.00		1286.27
Reach-1	1.6	PF 1	4444.19	4444.17	0.02	0.01	0.03		2762.00		1286.59
Reach-1	1.6	PF 2	4444.05	4444.04	0.01	0.01	0.03		2194.00		1269.75
Reach-1	1.5	PF 1	4444.15	4443.84	0.31	0.09	0.06		2762.00		1001.06
Reach-1	1.5	PF 2	4444.01	4443.73	0.28	0.09	0.06		2194.00		936.39
Reach-1	1.4	PF 1	4443.08	4442.98	0.10	0.21	0.01		2762.00		941.55
Reach-1	1.4	PF 2	4442.90	4442.81	0.09	0.19	0.01		2194.00		908.69
Reach-1	1	PF 1	4442.86	4442.80	0.06	0.04	0.01		2762.00		1017.19
Reach-1	1	PF 2	4442.70	4442.65	0.04	0.03	0.01		2194.00		981.53
Reach-1	0.5	PF 1	4442.82	4442.79	0.02	0.08	0.01		2636.33	125.67	1610.98
Reach-1	0.5	PF 2	4442.66	4442.64	0.02	0.07	0.01		2122.93	71.07	1531.67
Reach-1	0.35	PF 1	4442.73	4442.61	0.12	1.16	0.03		839.95	1922.05	1222.13
Reach-1	0.35	PF 2	4442.58	4442.48	0.11	1.17	0.02		609.47	1584.53	1156.15
Reach-1	.2	PF 1	4441.55	4441.17	0.38				2762.00		770.97
Reach-1	.2	PF 2	4441.39	4441.05	0.34				2194.00		709.59

Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

RIVER-1 Reach-1

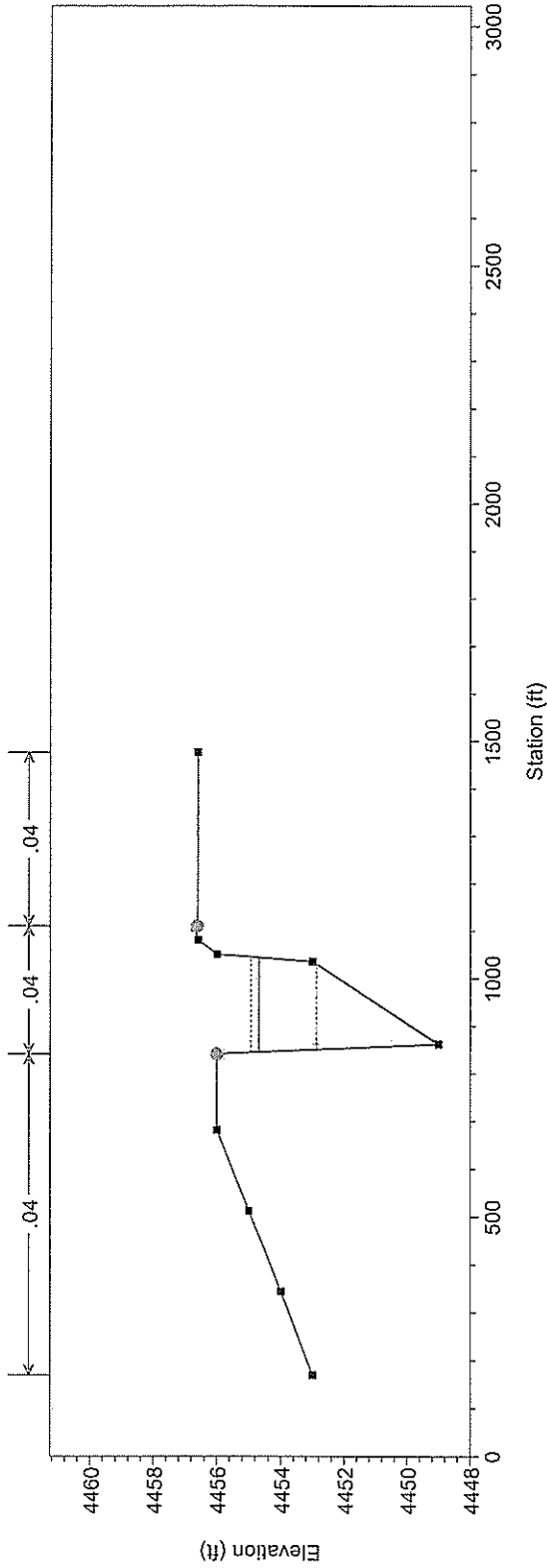


Legend	
EG PF 1	(Dotted line)
WS PF 1	(Dashed line)
Crit PF 1	(Dash-dot line)
Ground	(Solid line with square markers)
LOB	(Long-dashed line)
ROB	(Short-dashed line)
Left Levee	(Solid line)
Right Levee	(Solid line)

1 in Horiz. = 500 ft 1 in Vert. = 4 ft

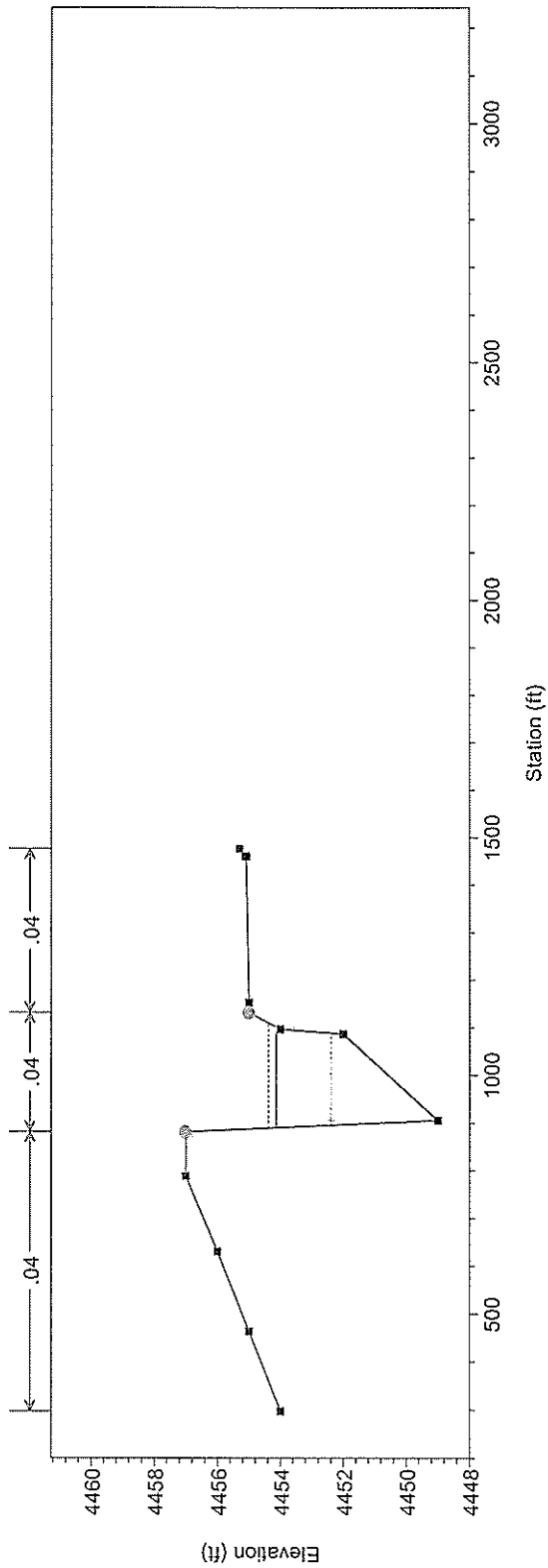
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 16



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

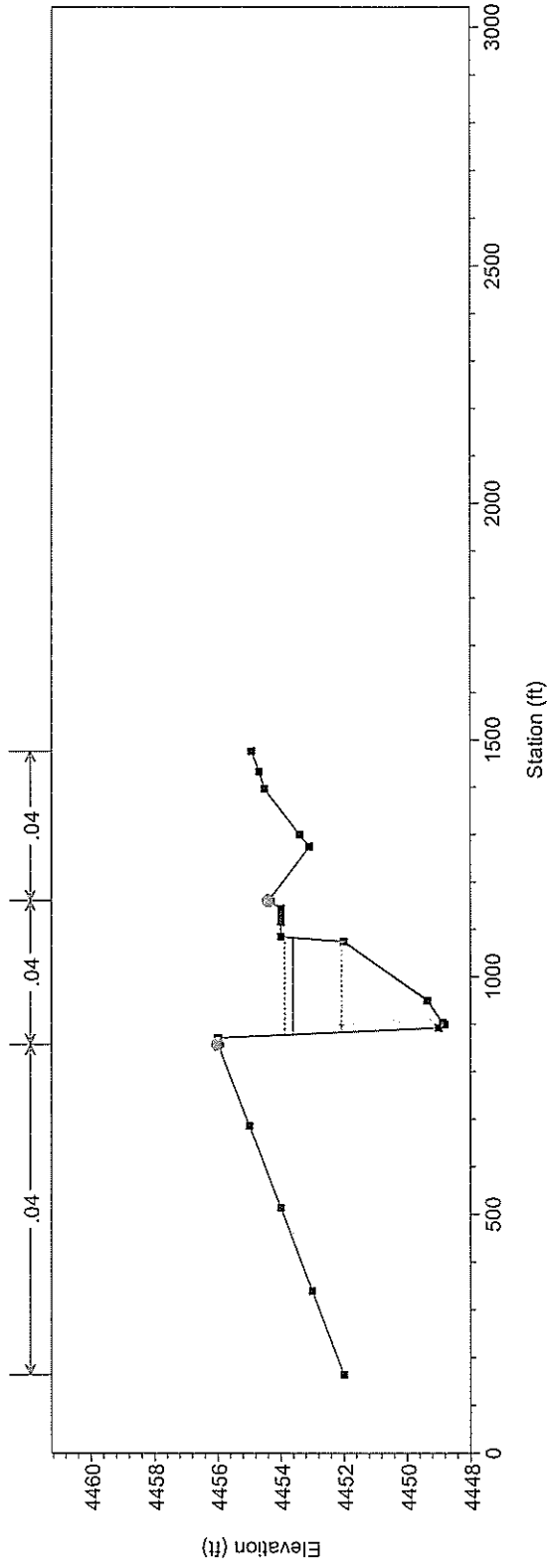
River = RIVER-1 Reach = Reach-1 RS = 15



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

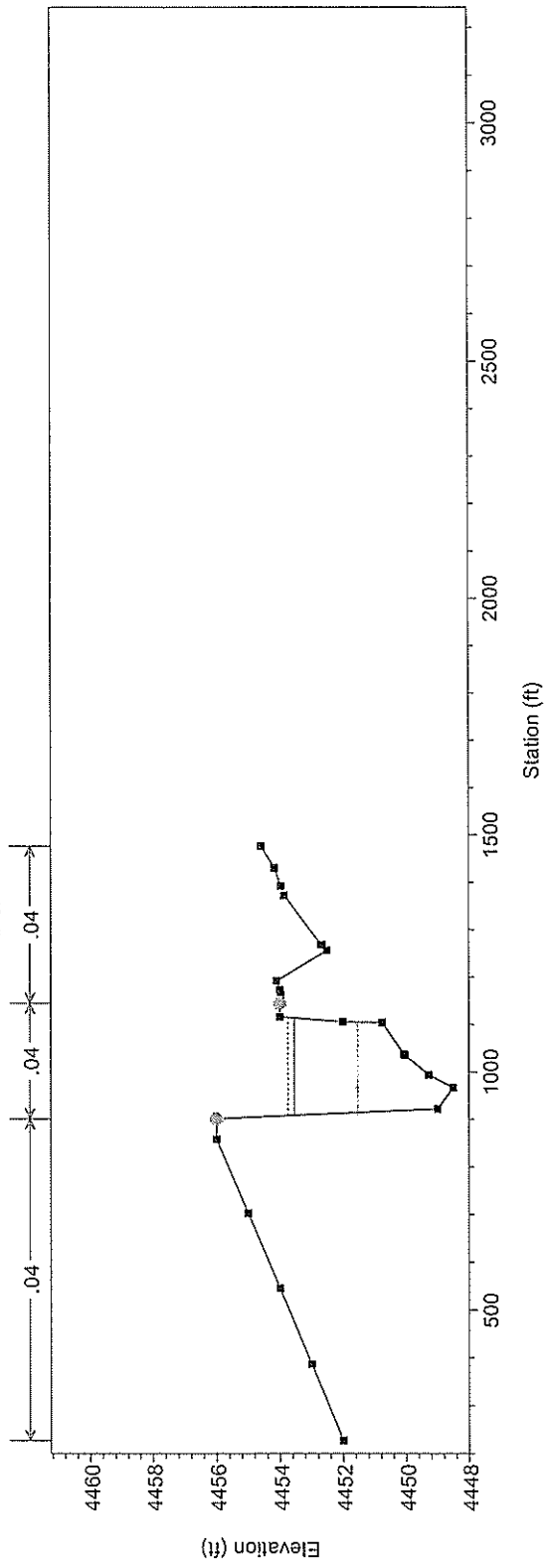
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 14



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

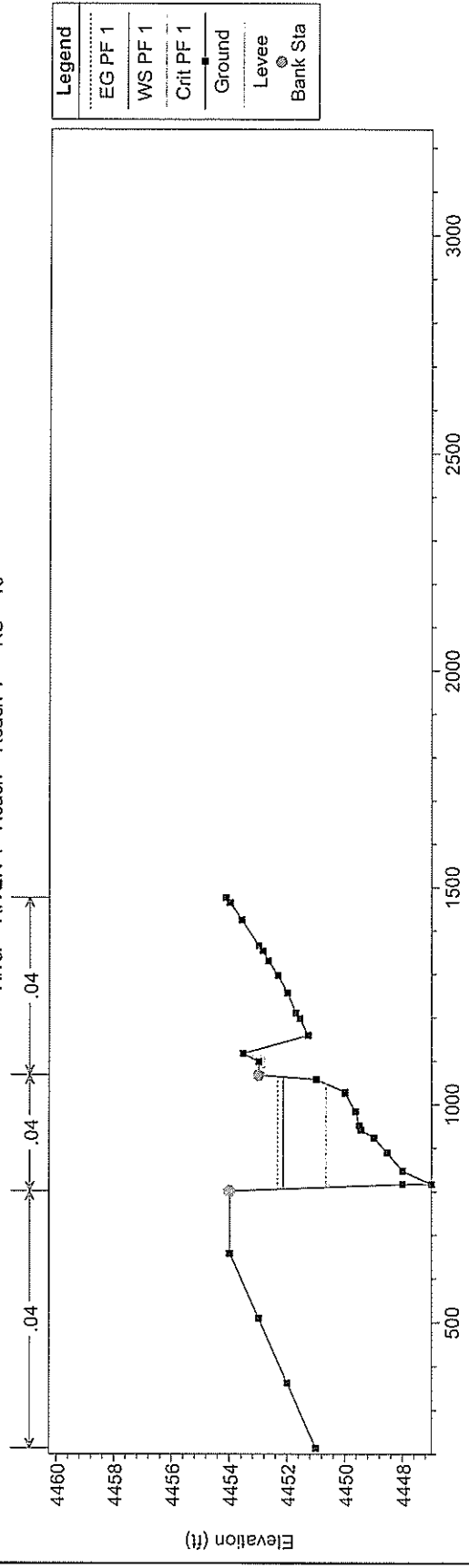
River = RIVER-1 Reach = Reach-1 RS = 13



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

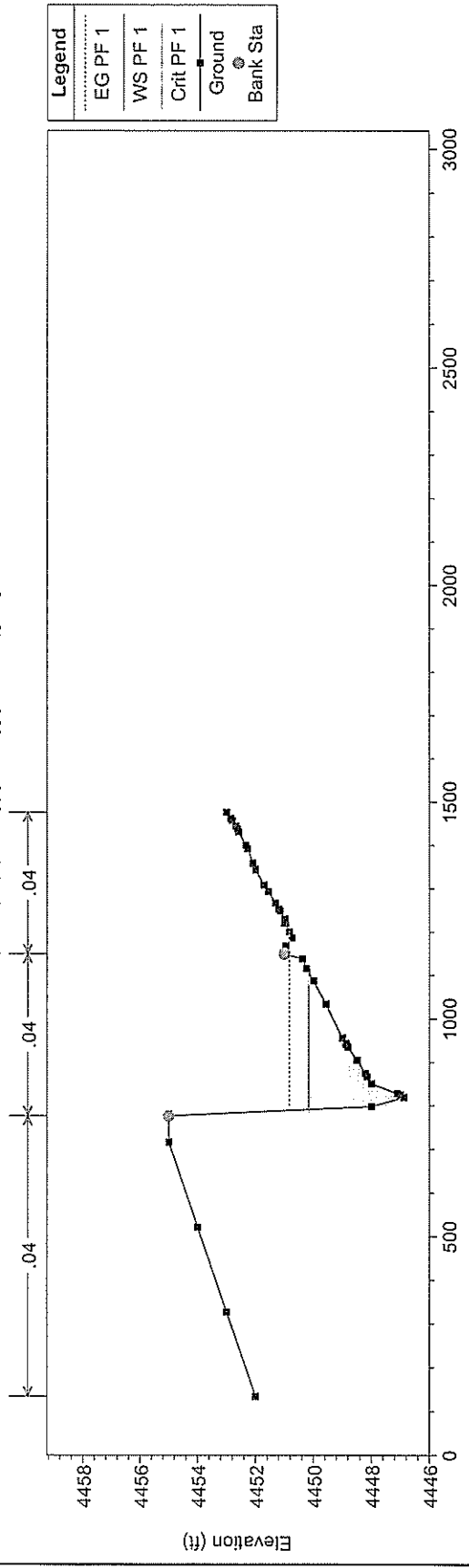
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 10



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

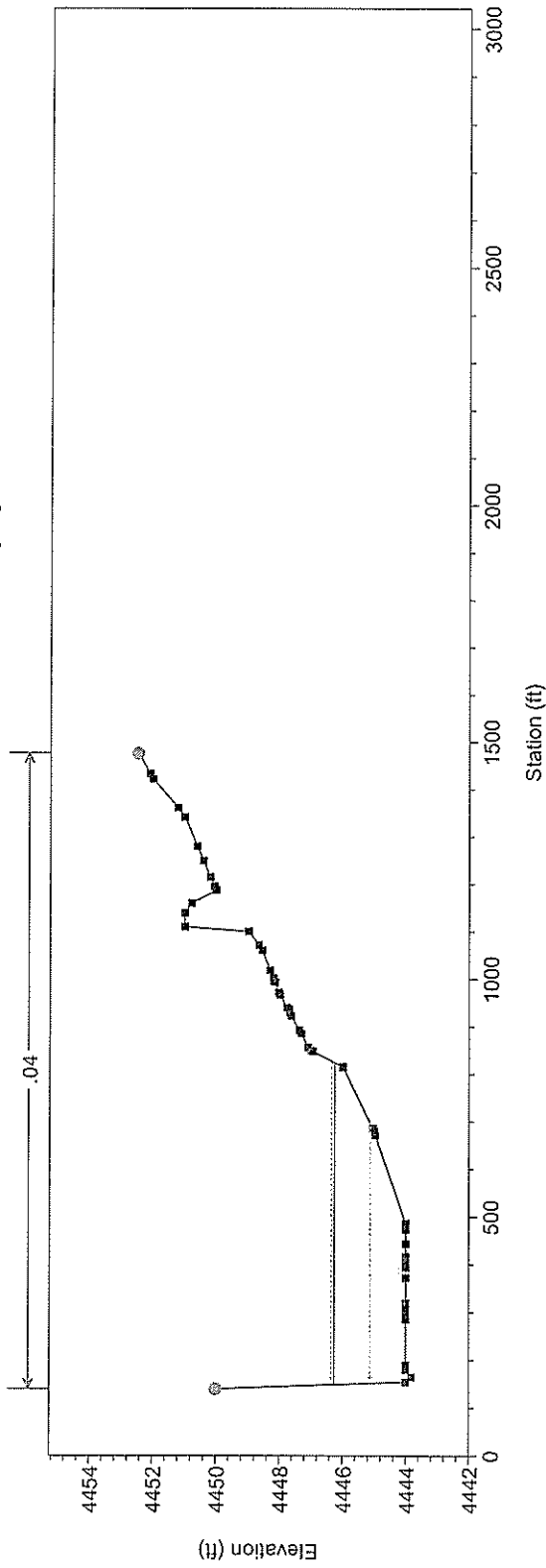
River = RIVER-1 Reach = Reach-1 RS = 9



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

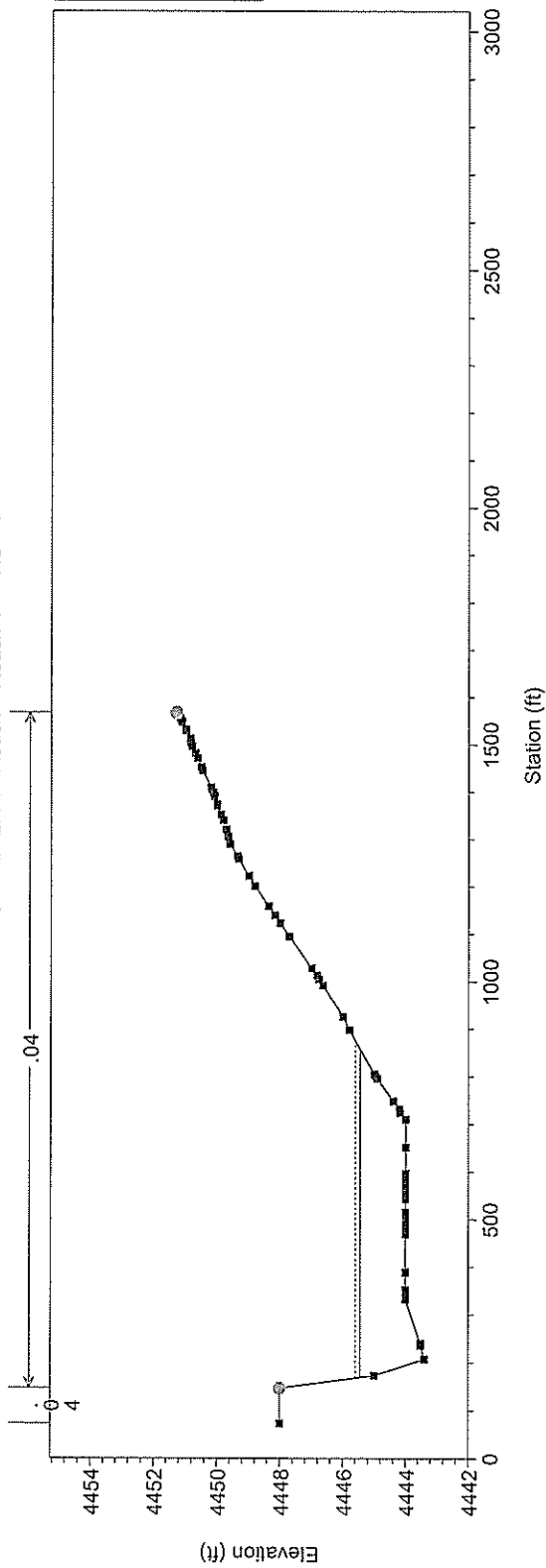
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 8



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

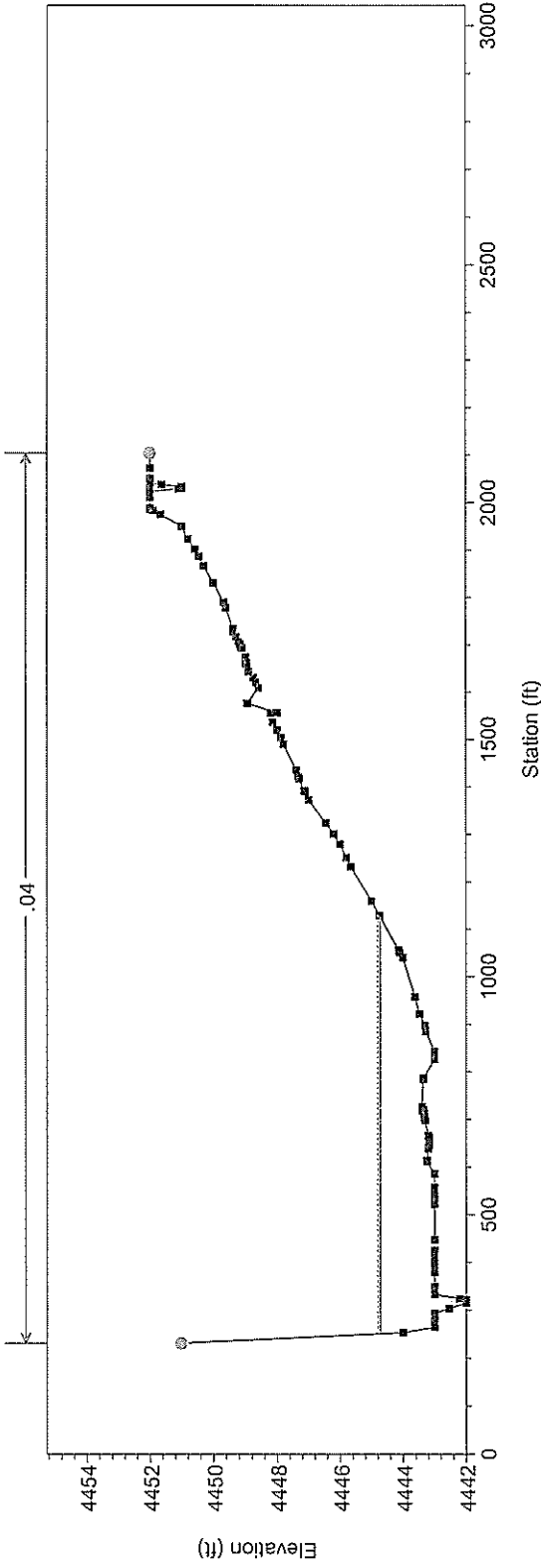
River = RIVER-1 Reach = Reach-1 RS = 7



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

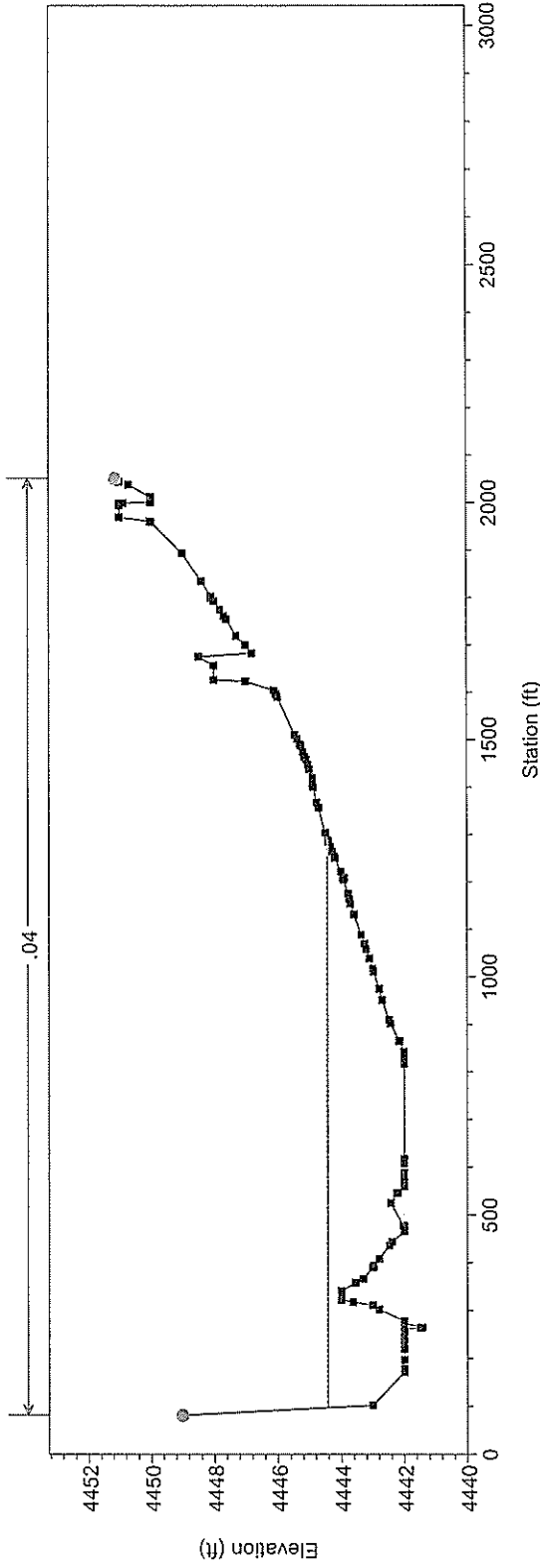
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 6



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

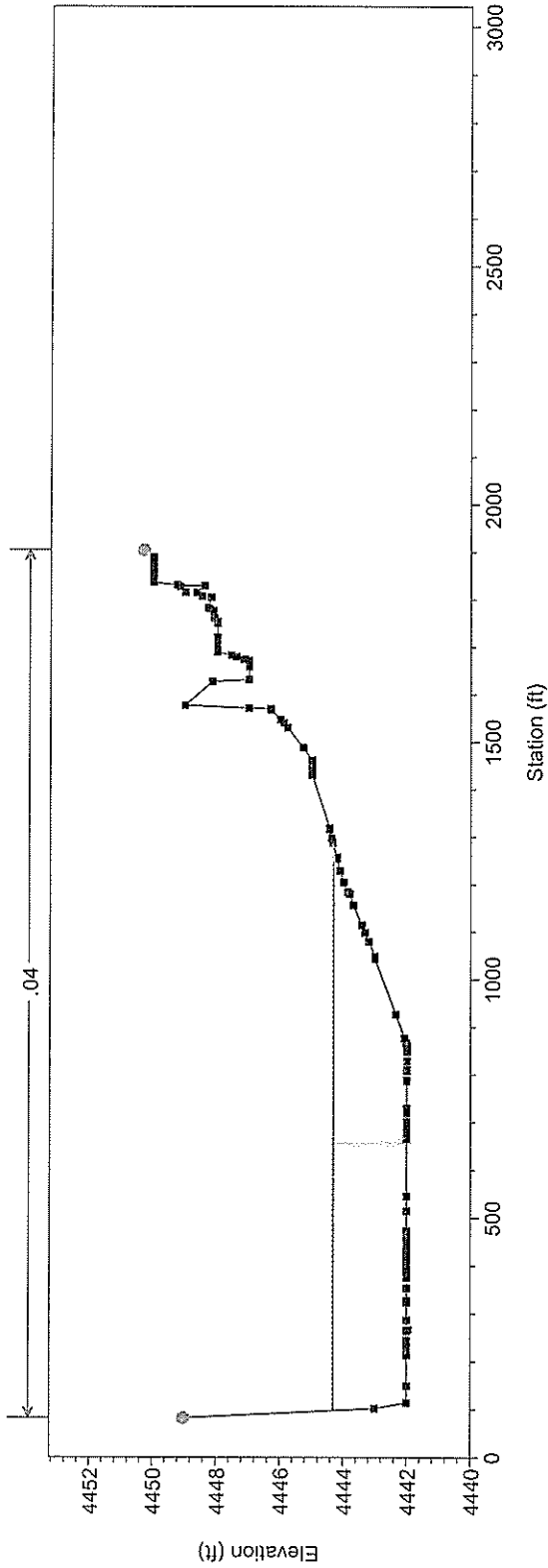
River = RIVER-1 Reach = Reach-1 RS = 5



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

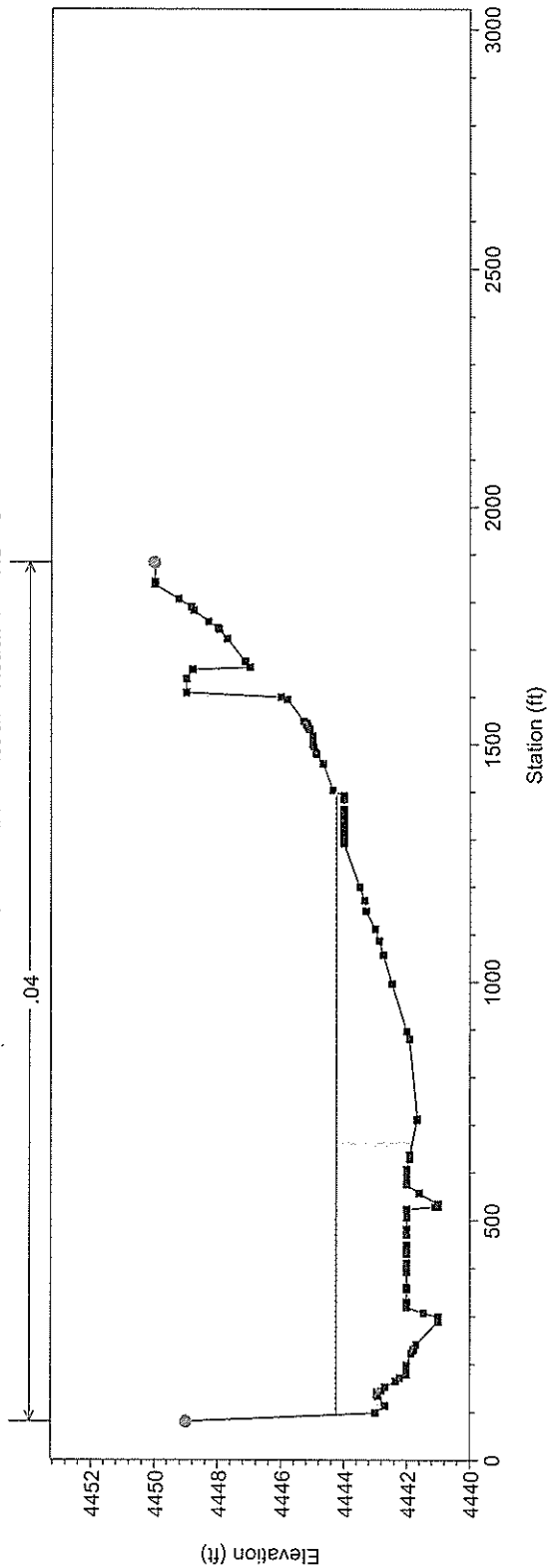
River = RIVER-1 Reach = Reach-1 RS = 4



Legend	
.....	EG PF 1
.....	WS PF 1
—■—	Ground
⊙	Bank Sta

Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 3

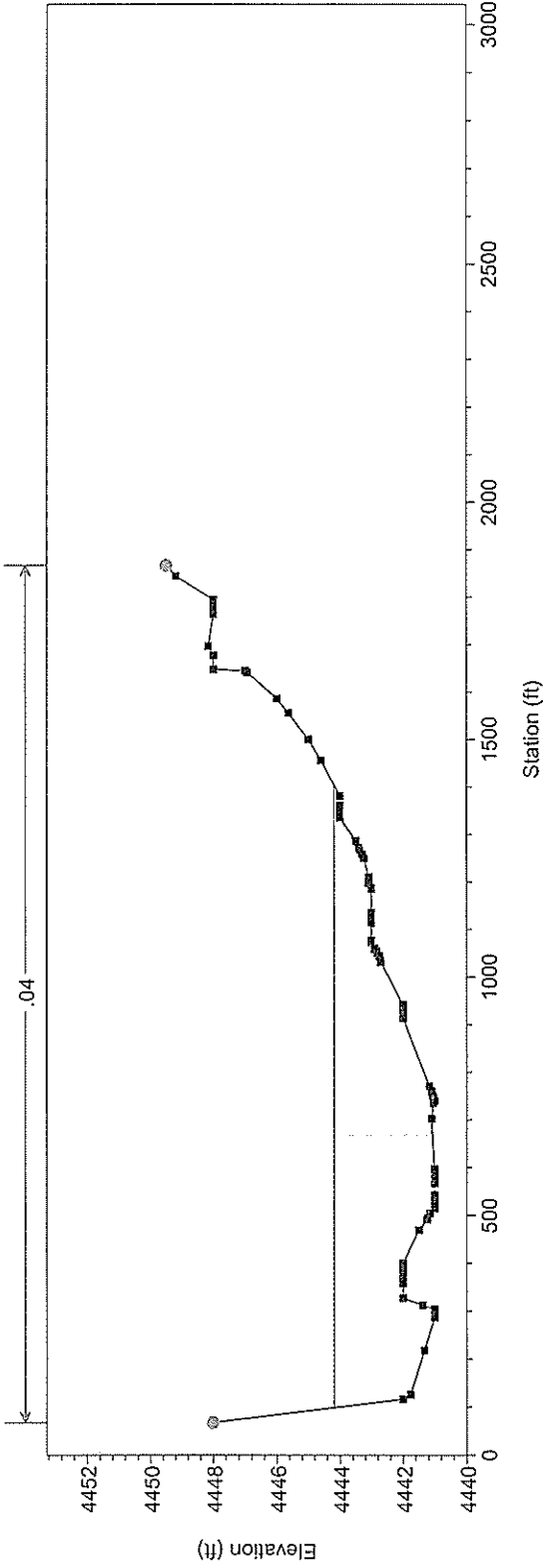


Legend	
.....	EG PF 1
.....	WS PF 1
—■—	Ground
⊙	Bank Sta

1 in Horiz. = 400 ft 1 in Vert. = 6 ft

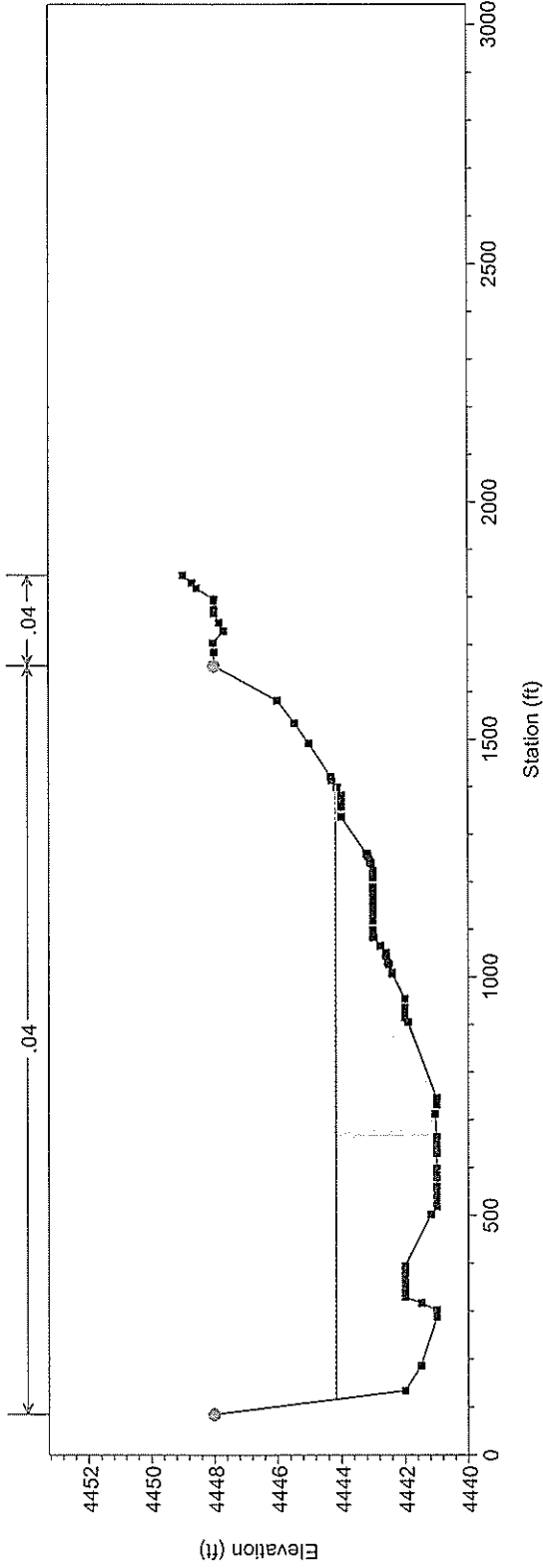
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 2



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

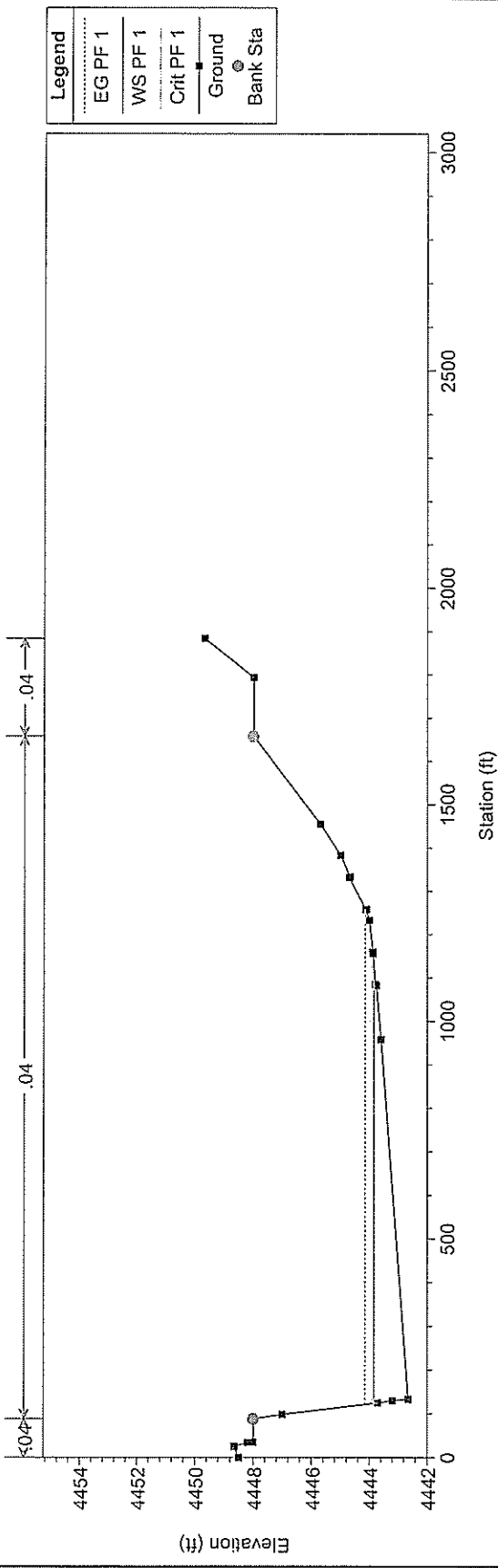
River = RIVER-1 Reach = Reach-1 RS = 1.6



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

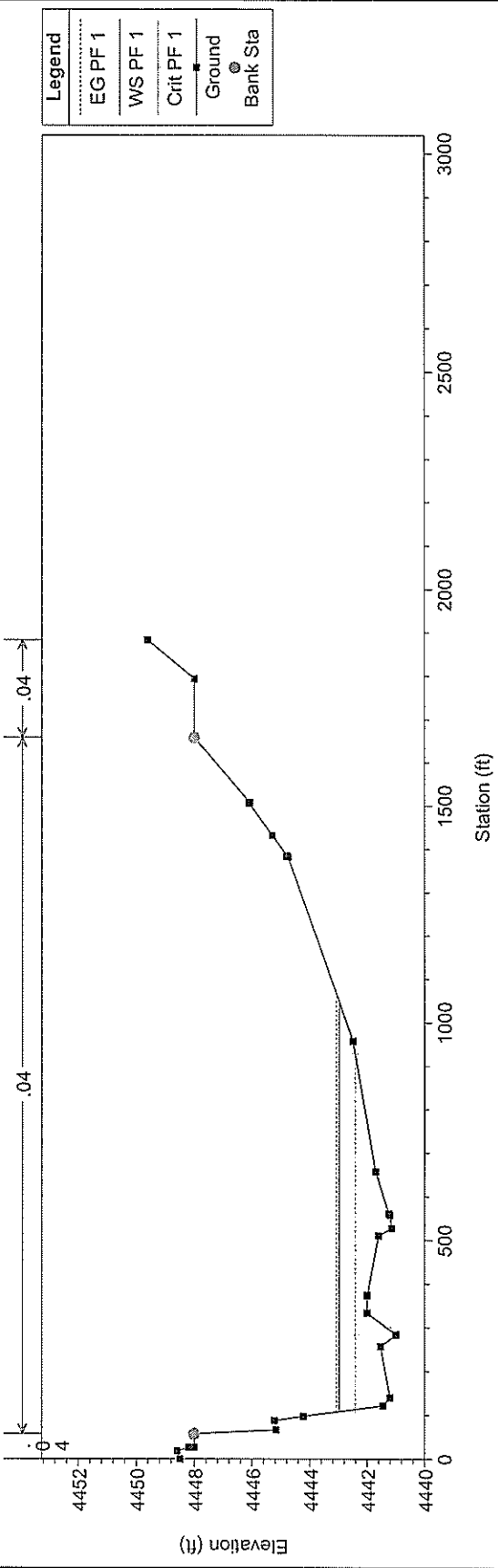
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 1.5



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

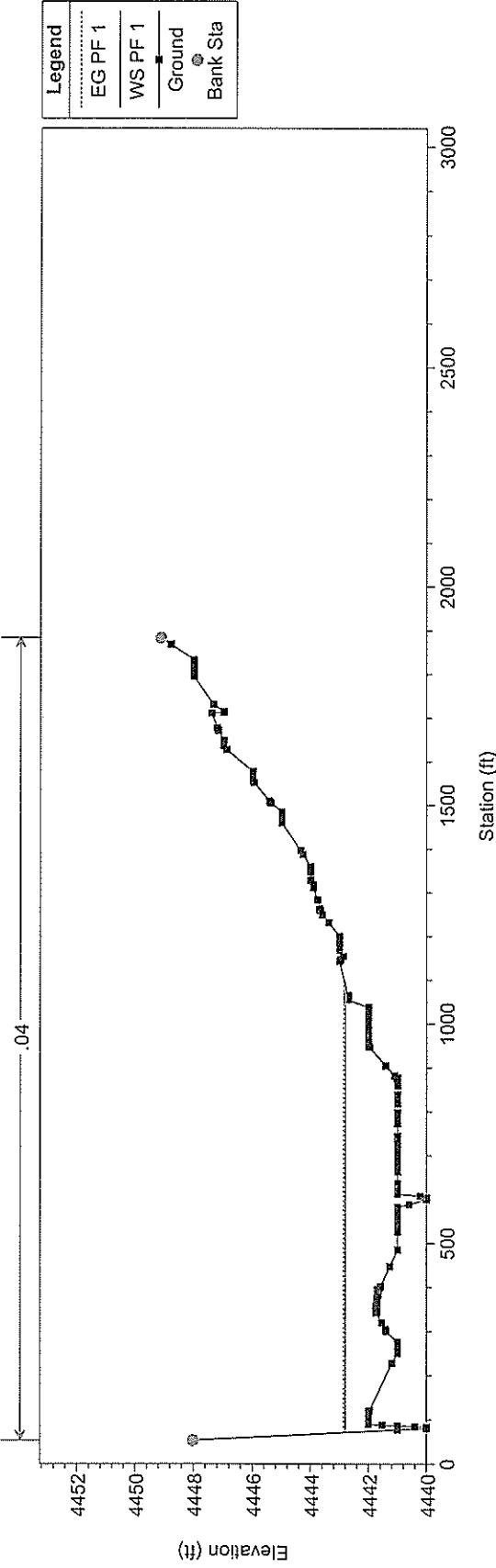
River = RIVER-1 Reach = Reach-1 RS = 1.4



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

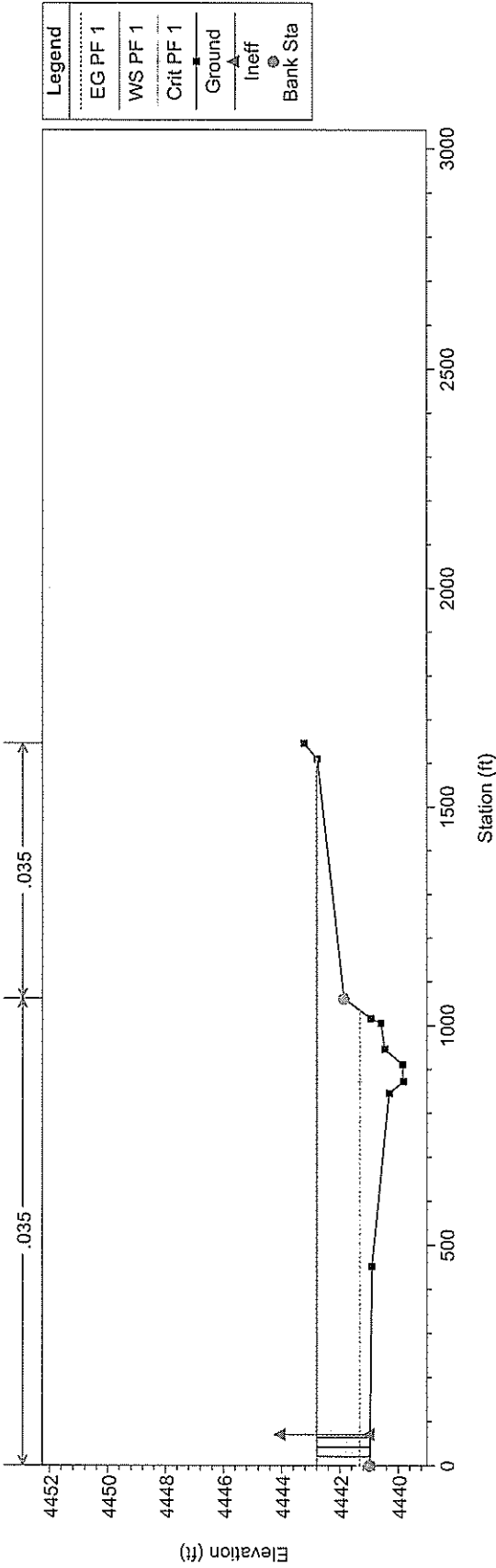
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 1



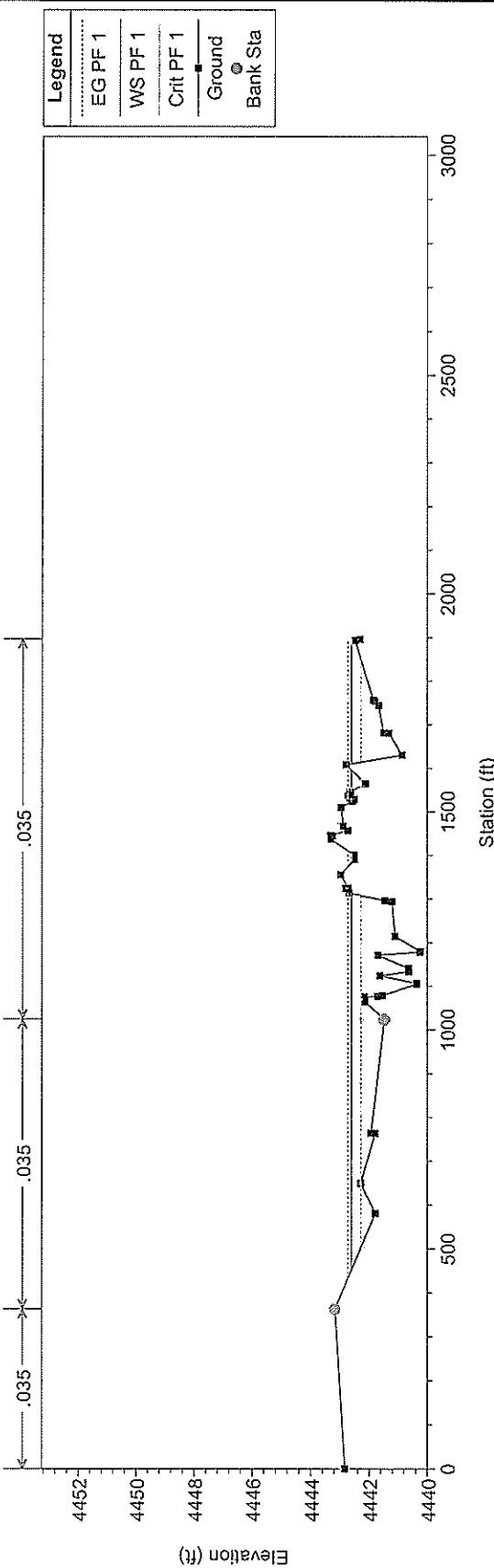
Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007

River = RIVER-1 Reach = Reach-1 RS = 0.5 Top of Bella Vista Riprap and Channel - 3.33 feet subtracted fro

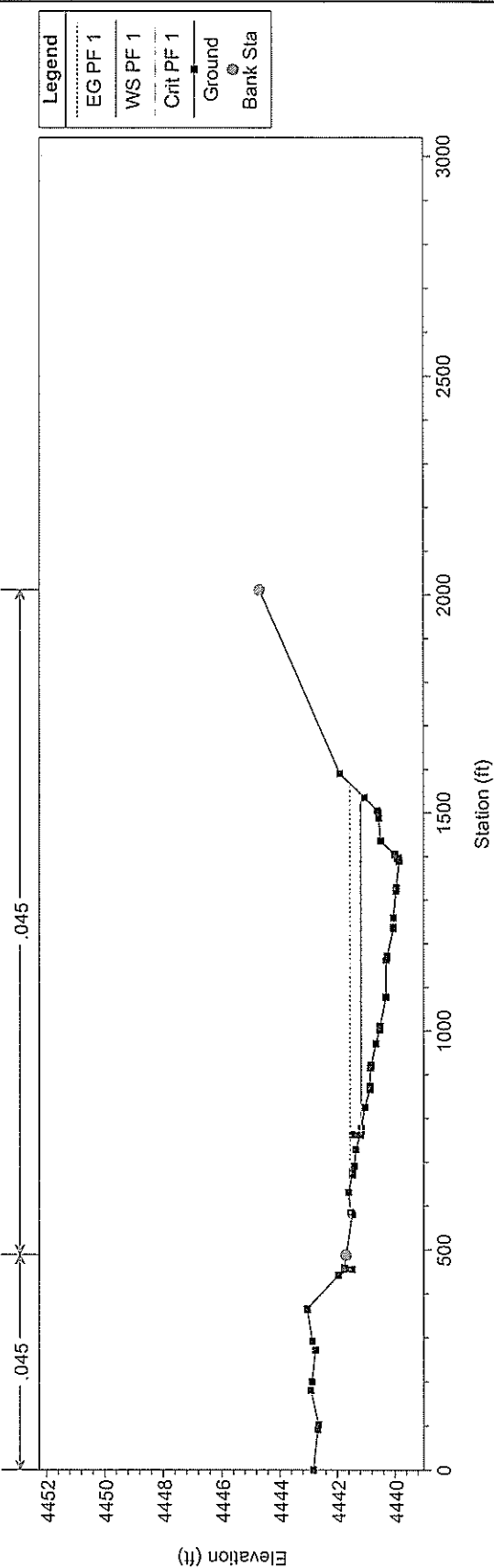


1 in Horiz. = 400 ft 1 in Vert. = 6 ft

Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007
 River = RIVER-1 Reach = Reach-1 RS = 0.35 Top of Steamboat Creek Riprap and Channel - 3.33 feet subtracted



Damonte Phase V - Wetlands Plan: Damonte Phase V - Wetlands/Steamboat 12/28/2007
 River = RIVER-1 Reach = Reach-1 RS = .2 Top of Steamboat Creek Channel - 3.33 Subtracted from Bella Vist



1 in Horiz. = 400 ft 1 in Vert. = 6 ft

HYDROGRAPH AT STATION EST-WS
 SUM OF 2 HYDROGRAPHS
 PLAN 1, RATIO = .94

This is the hydrograph of the East West Channel at the Steamboat Confluence

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW
27	JUL	0005	1	0.	*	27	JUL	0605	73	0.	*	27	JUL	1205	145	56.
27	JUL	0010	2	0.	*	27	JUL	0610	74	0.	*	27	JUL	1210	146	76.
27	JUL	0015	3	0.	*	27	JUL	0615	75	0.	*	27	JUL	1215	147	84.
27	JUL	0020	4	0.	*	27	JUL	0620	76	0.	*	27	JUL	1220	148	83.
27	JUL	0025	5	0.	*	27	JUL	0625	77	0.	*	27	JUL	1225	149	80.
27	JUL	0030	6	0.	*	27	JUL	0630	78	0.	*	27	JUL	1230	150	76.
27	JUL	0035	7	0.	*	27	JUL	0635	79	0.	*	27	JUL	1235	151	71.
27	JUL	0040	8	0.	*	27	JUL	0640	80	0.	*	27	JUL	1240	152	67.
27	JUL	0045	9	0.	*	27	JUL	0645	81	0.	*	27	JUL	1245	153	65.
27	JUL	0050	10	0.	*	27	JUL	0650	82	0.	*	27	JUL	1250	154	64.
27	JUL	0055	11	0.	*	27	JUL	0655	83	0.	*	27	JUL	1255	155	64.
27	JUL	0100	12	0.	*	27	JUL	0700	84	0.	*	27	JUL	1300	156	63.
27	JUL	0105	13	0.	*	27	JUL	0705	85	0.	*	27	JUL	1305	157	63.
27	JUL	0110	14	0.	*	27	JUL	0710	86	0.	*	27	JUL	1310	158	62.
27	JUL	0115	15	0.	*	27	JUL	0715	87	0.	*	27	JUL	1315	159	62.
27	JUL	0120	16	0.	*	27	JUL	0720	88	0.	*	27	JUL	1320	160	61.
27	JUL	0125	17	0.	*	27	JUL	0725	89	0.	*	27	JUL	1325	161	61.
27	JUL	0130	18	0.	*	27	JUL	0730	90	0.	*	27	JUL	1330	162	60.
27	JUL	0135	19	0.	*	27	JUL	0735	91	0.	*	27	JUL	1335	163	60.
27	JUL	0140	20	0.	*	27	JUL	0740	92	0.	*	27	JUL	1340	164	59.
27	JUL	0145	21	0.	*	27	JUL	0745	93	0.	*	27	JUL	1345	165	59.
27	JUL	0150	22	0.	*	27	JUL	0750	94	0.	*	27	JUL	1350	166	58.
27	JUL	0155	23	0.	*	27	JUL	0755	95	0.	*	27	JUL	1355	167	58.
27	JUL	0200	24	0.	*	27	JUL	0800	96	0.	*	27	JUL	1400	168	57.
27	JUL	0205	25	0.	*	27	JUL	0805	97	0.	*	27	JUL	1405	169	57.
27	JUL	0210	26	0.	*	27	JUL	0810	98	0.	*	27	JUL	1410	170	56.
27	JUL	0215	27	0.	*	27	JUL	0815	99	0.	*	27	JUL	1415	171	56.

East-West Confluence
with Steamboat Creek

27 JUL 0220	28	0.	*	27 JUL 0820	100	0.	*	27 JUL 1420	172	56.	*	27 JUL 2020	244	31.
27 JUL 0225	29	0.	*	27 JUL 0825	101	0.	*	27 JUL 1425	173	55.	*	27 JUL 2025	245	31.
27 JUL 0230	30	0.	*	27 JUL 0830	102	0.	*	27 JUL 1430	174	55.	*	27 JUL 2030	246	31.
27 JUL 0235	31	0.	*	27 JUL 0835	103	0.	*	27 JUL 1435	175	54.	*	27 JUL 2035	247	31.
27 JUL 0240	32	0.	*	27 JUL 0840	104	0.	*	27 JUL 1440	176	54.	*	27 JUL 2040	248	30.
27 JUL 0245	33	0.	*	27 JUL 0845	105	0.	*	27 JUL 1445	177	53.	*	27 JUL 2045	249	30.
27 JUL 0250	34	0.	*	27 JUL 0850	106	0.	*	27 JUL 1450	178	53.	*	27 JUL 2050	250	30.
27 JUL 0255	35	0.	*	27 JUL 0855	107	0.	*	27 JUL 1455	179	53.	*	27 JUL 2055	251	30.
27 JUL 0300	36	0.	*	27 JUL 0900	108	0.	*	27 JUL 1500	180	52.	*	27 JUL 2100	252	29.
27 JUL 0305	37	0.	*	27 JUL 0905	109	0.	*	27 JUL 1505	181	52.	*	27 JUL 2105	253	29.
27 JUL 0310	38	0.	*	27 JUL 0910	110	0.	*	27 JUL 1510	182	51.	*	27 JUL 2110	254	29.
27 JUL 0315	39	0.	*	27 JUL 0915	111	0.	*	27 JUL 1515	183	51.	*	27 JUL 2115	255	29.
27 JUL 0320	40	0.	*	27 JUL 0920	112	0.	*	27 JUL 1520	184	51.	*	27 JUL 2120	256	29.
27 JUL 0325	41	0.	*	27 JUL 0925	113	0.	*	27 JUL 1525	185	50.	*	27 JUL 2125	257	28.
27 JUL 0330	42	0.	*	27 JUL 0930	114	0.	*	27 JUL 1530	186	50.	*	27 JUL 2130	258	28.
27 JUL 0335	43	0.	*	27 JUL 0935	115	0.	*	27 JUL 1535	187	49.	*	27 JUL 2135	259	28.
27 JUL 0340	44	0.	*	27 JUL 0940	116	0.	*	27 JUL 1540	188	49.	*	27 JUL 2140	260	28.
27 JUL 0345	45	0.	*	27 JUL 0945	117	0.	*	27 JUL 1545	189	49.	*	27 JUL 2145	261	27.
27 JUL 0350	46	0.	*	27 JUL 0950	118	0.	*	27 JUL 1550	190	48.	*	27 JUL 2150	262	27.
27 JUL 0355	47	0.	*	27 JUL 0955	119	0.	*	27 JUL 1555	191	48.	*	27 JUL 2155	263	27.
27 JUL 0400	48	0.	*	27 JUL 1000	120	0.	*	27 JUL 1600	192	47.	*	27 JUL 2200	264	27.
27 JUL 0405	49	0.	*	27 JUL 1005	121	0.	*	27 JUL 1605	193	47.	*	27 JUL 2205	265	27.
27 JUL 0410	50	0.	*	27 JUL 1010	122	0.	*	27 JUL 1610	194	47.	*	27 JUL 2210	266	26.
27 JUL 0415	51	0.	*	27 JUL 1015	123	0.	*	27 JUL 1615	195	46.	*	27 JUL 2215	267	26.
27 JUL 0420	52	0.	*	27 JUL 1020	124	0.	*	27 JUL 1620	196	46.	*	27 JUL 2220	268	26.
27 JUL 0425	53	0.	*	27 JUL 1025	125	0.	*	27 JUL 1625	197	46.	*	27 JUL 2225	269	26.
27 JUL 0430	54	0.	*	27 JUL 1030	126	0.	*	27 JUL 1630	198	45.	*	27 JUL 2230	270	26.
27 JUL 0435	55	0.	*	27 JUL 1035	127	1.	*	27 JUL 1635	199	45.	*	27 JUL 2235	271	25.
27 JUL 0440	56	0.	*	27 JUL 1040	128	1.	*	27 JUL 1640	200	45.	*	27 JUL 2240	272	25.
27 JUL 0445	57	0.	*	27 JUL 1045	129	1.	*	27 JUL 1645	201	44.	*	27 JUL 2245	273	25.
27 JUL 0450	58	0.	*	27 JUL 1050	130	1.	*	27 JUL 1650	202	44.	*	27 JUL 2250	274	25.
27 JUL 0455	59	0.	*	27 JUL 1055	131	1.	*	27 JUL 1655	203	43.	*	27 JUL 2255	275	25.
27 JUL 0500	60	0.	*	27 JUL 1100	132	1.	*	27 JUL 1700	204	43.	*	27 JUL 2300	276	24.
27 JUL 0505	61	0.	*	27 JUL 1105	133	1.	*	27 JUL 1705	205	43.	*	27 JUL 2305	277	24.
27 JUL 0510	62	0.	*	27 JUL 1110	134	2.	*	27 JUL 1710	206	42.	*	27 JUL 2310	278	24.

TIME	PEAK FLOW (CFS)	6-HR	24-HR	72-HR	23.92-HR	DEPTH (INCHES)	DEPTH (AC-FT)	DATE	DEPTH		
27 JUL 0515	63	0.	27 JUL 1115	135	2.	27 JUL 1715	207	42.	27 JUL 2315	279	24.
27 JUL 0520	64	0.	27 JUL 1120	136	2.	27 JUL 1720	208	42.	27 JUL 2320	280	24.
27 JUL 0525	65	0.	27 JUL 1125	137	3.	27 JUL 1725	209	41.	27 JUL 2325	281	23.
27 JUL 0530	66	0.	27 JUL 1130	138	3.	27 JUL 1730	210	41.	27 JUL 2330	282	23.
27 JUL 0535	67	0.	27 JUL 1135	139	3.	27 JUL 1735	211	41.	27 JUL 2335	283	23.
27 JUL 0540	68	0.	27 JUL 1140	140	4.	27 JUL 1740	212	40.	27 JUL 2340	284	23.
27 JUL 0545	69	0.	27 JUL 1145	141	6.	27 JUL 1745	213	40.	27 JUL 2345	285	23.
27 JUL 0550	70	0.	27 JUL 1150	142	10.	27 JUL 1750	214	40.	27 JUL 2350	286	23.
27 JUL 0555	71	0.	27 JUL 1155	143	17.	27 JUL 1755	215	40.	27 JUL 2355	287	22.
27 JUL 0600	72	0.	27 JUL 1200	144	32.	27 JUL 1800	216	39.	28 JUL 0000	288	22.

PEAK FLOW (CFS)	TIME (HR)	6-HR	24-HR	72-HR	23.92-HR
84.	12.17	53.	21.	21.	21.
(INCHES)		3.105	4.909	4.909	4.909
(AC-FT)		26.	42.	42.	42.

CUMULATIVE AREA = .16 SQ MI

Peak flow is listed at 12:17 hours and 84 cfs at confluence with Steamboat Creek.

HYDROGRAPH AT STATION RT 12
PLAN 1, RATIO = .94

[This is the routed hydrograph from STMBv3 Downstream to the East-West Channel Confluence]

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
27	JUL	0005	1	0.	27	JUL	0605	73	518.	27	JUL	1205	145	604.
27	JUL	0010	2	0.	27	JUL	0610	74	519.	27	JUL	1210	146	621.
27	JUL	0015	3	0.	27	JUL	0615	75	520.	27	JUL	1215	147	651.
27	JUL	0020	4	0.	27	JUL	0620	76	522.	27	JUL	1220	148	704.
27	JUL	0025	5	0.	27	JUL	0625	77	527.	27	JUL	1225	149	784.
27	JUL	0030	6	0.	27	JUL	0630	78	534.	27	JUL	1230	150	871.
27	JUL	0035	7	0.	27	JUL	0635	79	543.	27	JUL	1235	151	939.
27	JUL	0040	8	0.	27	JUL	0640	80	553.	27	JUL	1240	152	977.
27	JUL	0045	9	0.	27	JUL	0645	81	560.	27	JUL	1245	153	998.
27	JUL	0050	10	0.	27	JUL	0650	82	565.	27	JUL	1250	154	1017.
27	JUL	0055	11	1.	27	JUL	0655	83	566.	27	JUL	1255	155	1046.
27	JUL	0100	12	3.	27	JUL	0700	84	563.	27	JUL	1300	156	1086.
27	JUL	0105	13	10.	27	JUL	0705	85	559.	27	JUL	1305	157	1139.
27	JUL	0110	14	32.	27	JUL	0710	86	556.	27	JUL	1310	158	1216.
27	JUL	0115	15	73.	27	JUL	0715	87	556.	27	JUL	1315	159	1325.
27	JUL	0120	16	130.	27	JUL	0720	88	561.	27	JUL	1320	160	1476.
27	JUL	0125	17	192.	27	JUL	0725	89	571.	27	JUL	1325	161	1672.
27	JUL	0130	18	251.	27	JUL	0730	90	586.	27	JUL	1330	162	1911.
27	JUL	0135	19	302.	27	JUL	0735	91	599.	27	JUL	1335	163	2180.
27	JUL	0140	20	345.	27	JUL	0740	92	608.	27	JUL	1340	164	2464.
27	JUL	0145	21	382.	27	JUL	0745	93	610.	27	JUL	1345	165	2751.
27	JUL	0150	22	412.	27	JUL	0750	94	608.	27	JUL	1350	166	3037.
27	JUL	0155	23	437.	27	JUL	0755	95	604.	27	JUL	1355	167	3317.
27	JUL	0200	24	456.	27	JUL	0800	96	601.	27	JUL	1400	168	3593.
27	JUL	0205	25	470.	27	JUL	0805	97	600.	27	JUL	1405	169	3866.
27	JUL	0210	26	481.	27	JUL	0810	98	603.	27	JUL	1410	170	4137.
27	JUL	0215	27	488.	27	JUL	0815	99	609.	27	JUL	1415	171	4402.
27	JUL	0220	28	493.	27	JUL	0820	100	615.	27	JUL	1420	172	4648.
27	JUL	0225	29	497.	27	JUL	0825	101	620.	27	JUL	1425	173	4860.
27	JUL	0230	30	500.	27	JUL	0830	102	622.	27	JUL	1430	174	5026.
27	JUL	0235	31	502.	27	JUL	0835	103	620.	27	JUL	1435	175	5140.
27	JUL	1805	217	6263.	27	JUL	1810	218	6247.	27	JUL	1815	219	6226.
27	JUL	1820	220	6201.	27	JUL	1825	221	6171.	27	JUL	1830	222	6137.
27	JUL	1835	223	6099.	27	JUL	1840	224	6056.	27	JUL	1845	225	6006.
27	JUL	1850	226	5948.	27	JUL	1855	227	5882.	27	JUL	1900	228	5807.
27	JUL	1905	229	5724.	27	JUL	1910	230	5630.	27	JUL	1915	231	5528.
27	JUL	1920	232	5417.	27	JUL	1925	233	5299.	27	JUL	1930	234	5171.
27	JUL	1935	235	5034.	27	JUL	1940	236	4894.	27	JUL	1945	237	4757.
27	JUL	1950	238	4628.	27	JUL	1955	239	4507.	27	JUL	2000	240	4393.
27	JUL	2005	241	4282.	27	JUL	2010	242	4174.	27	JUL	2015	243	4067.
27	JUL	2020	244	3964.	27	JUL	2025	245	3866.	27	JUL	2030	246	3771.
27	JUL	2035	247	3680.										

East-West Confluence
with Steamboat Creek

27 JUL 0240	32	503.	*	27 JUL 0840	104	615.	*	27 JUL 1440	176	5210.	*	27 JUL 2040	248	3591.
27 JUL 0245	33	504.	*	27 JUL 0845	105	608.	*	27 JUL 1445	177	5244.	*	27 JUL 2045	249	3503.
27 JUL 0250	34	505.	*	27 JUL 0850	106	601.	*	27 JUL 1450	178	5253.	*	27 JUL 2050	250	3417.
27 JUL 0255	35	505.	*	27 JUL 0855	107	595.	*	27 JUL 1455	179	5246.	*	27 JUL 2055	251	3336.
27 JUL 0300	36	506.	*	27 JUL 0900	108	590.	*	27 JUL 1500	180	5230.	*	27 JUL 2100	252	3259.
27 JUL 0305	37	506.	*	27 JUL 0905	109	587.	*	27 JUL 1505	181	5213.	*	27 JUL 2105	253	3188.
27 JUL 0310	38	507.	*	27 JUL 0910	110	584.	*	27 JUL 1510	182	5198.	*	27 JUL 2110	254	3121.
27 JUL 0315	39	507.	*	27 JUL 0915	111	582.	*	27 JUL 1515	183	5187.	*	27 JUL 2115	255	3058.
27 JUL 0320	40	507.	*	27 JUL 0920	112	580.	*	27 JUL 1520	184	5184.	*	27 JUL 2120	256	2999.
27 JUL 0325	41	508.	*	27 JUL 0925	113	579.	*	27 JUL 1525	185	5190.	*	27 JUL 2125	257	2942.
27 JUL 0330	42	508.	*	27 JUL 0930	114	578.	*	27 JUL 1530	186	5205.	*	27 JUL 2130	258	2888.
27 JUL 0335	43	508.	*	27 JUL 0935	115	578.	*	27 JUL 1535	187	5230.	*	27 JUL 2135	259	2837.
27 JUL 0340	44	509.	*	27 JUL 0940	116	577.	*	27 JUL 1540	188	5264.	*	27 JUL 2140	260	2786.
27 JUL 0345	45	509.	*	27 JUL 0945	117	577.	*	27 JUL 1545	189	5308.	*	27 JUL 2145	261	2737.
27 JUL 0350	46	509.	*	27 JUL 0950	118	576.	*	27 JUL 1550	190	5358.	*	27 JUL 2150	262	2689.
27 JUL 0355	47	509.	*	27 JUL 0955	119	576.	*	27 JUL 1555	191	5411.	*	27 JUL 2155	263	2645.
27 JUL 0400	48	509.	*	27 JUL 1000	120	576.	*	27 JUL 1600	192	5466.	*	27 JUL 2200	264	2604.
27 JUL 0405	49	510.	*	27 JUL 1005	121	576.	*	27 JUL 1605	193	5524.	*	27 JUL 2205	265	2565.
27 JUL 0410	50	510.	*	27 JUL 1010	122	575.	*	27 JUL 1610	194	5585.	*	27 JUL 2210	266	2529.
27 JUL 0415	51	510.	*	27 JUL 1015	123	575.	*	27 JUL 1615	195	5650.	*	27 JUL 2215	267	2495.
27 JUL 0420	52	510.	*	27 JUL 1020	124	575.	*	27 JUL 1620	196	5714.	*	27 JUL 2220	268	2462.
27 JUL 0425	53	510.	*	27 JUL 1025	125	575.	*	27 JUL 1625	197	5775.	*	27 JUL 2225	269	2431.
27 JUL 0430	54	511.	*	27 JUL 1030	126	575.	*	27 JUL 1630	198	5831.	*	27 JUL 2230	270	2400.
27 JUL 0435	55	511.	*	27 JUL 1035	127	575.	*	27 JUL 1635	199	5886.	*	27 JUL 2235	271	2370.
27 JUL 0440	56	511.	*	27 JUL 1040	128	575.	*	27 JUL 1640	200	5940.	*	27 JUL 2240	272	2341.
27 JUL 0445	57	512.	*	27 JUL 1045	129	575.	*	27 JUL 1645	201	5994.	*	27 JUL 2245	273	2313.
27 JUL 0450	58	512.	*	27 JUL 1050	130	575.	*	27 JUL 1650	202	6046.	*	27 JUL 2250	274	2286.
27 JUL 0455	59	513.	*	27 JUL 1055	131	575.	*	27 JUL 1655	203	6092.	*	27 JUL 2255	275	2259.
27 JUL 0500	60	513.	*	27 JUL 1100	132	576.	*	27 JUL 1700	204	6130.	*	27 JUL 2300	276	2233.
27 JUL 0505	61	513.	*	27 JUL 1105	133	576.	*	27 JUL 1705	205	6159.	*	27 JUL 2305	277	2208.
27 JUL 0510	62	514.	*	27 JUL 1110	134	577.	*	27 JUL 1710	206	6184.	*	27 JUL 2310	278	2184.
27 JUL 0515	63	514.	*	27 JUL 1115	135	578.	*	27 JUL 1715	207	6207.	*	27 JUL 2315	279	2160.
27 JUL 0520	64	515.	*	27 JUL 1120	136	579.	*	27 JUL 1720	208	6227.	*	27 JUL 2320	280	2137.
27 JUL 0525	65	515.	*	27 JUL 1125	137	580.	*	27 JUL 1725	209	6246.	*	27 JUL 2325	281	2115.
27 JUL 0530	66	516.	*	27 JUL 1130	138	581.	*	27 JUL 1730	210	6262.	*	27 JUL 2330	282	2093.
27 JUL 0535	67	516.	*	27 JUL 1135	139	583.	*	27 JUL 1735	211	6276.	*	27 JUL 2335	283	2072.
27 JUL 0540	68	516.	*	27 JUL 1140	140	584.	*	27 JUL 1740	212	6287.	*	27 JUL 2340	284	2052.
27 JUL 0545	69	517.	*	27 JUL 1145	141	586.	*	27 JUL 1745	213	6292.	*	27 JUL 2345	285	2033.
27 JUL 0550	70	517.	*	27 JUL 1150	142	588.	*	27 JUL 1750	214	6292.	*	27 JUL 2350	286	2015.
27 JUL 0555	71	518.	*	27 JUL 1155	143	591.	*	27 JUL 1755	215	6286.	*	27 JUL 2355	287	1996.
27 JUL 0600	72	518.	*	27 JUL 1200	144	595.	*	27 JUL 1800	216	6276.	*	28 JUL 0000	288	1977.

Depth upstream of confluence should be similar to depth at Station 46 which is downstream of Basin No. 3.
 Computed formula for depth is:

Equation for Depth vs Channel Flow at Basin 3 Outlet		
C3	C2	C1
0	-7.16E-08	1.20E-03
0.0000E+00	-7.159DE-08	1.2043E-03
		C0
		3.58E+00
		3.5826E+00

At flow = 621 cfs computed depth equals 4.30 feet. Flowline of Steamboat Creek at Confluence is 4425.81
 therefore water surface in Steamboat Creek at Time = 12.17 equals 4430.1.

Depth upstream of confluence should be similar to depth at Station 46 which is downstream of Basin No. 3.
Computed formula for depth is:

Equation for Depth vs Channel Flow at Basin 3 Outlet			
C3	C2	C1	C0
0.0000E+00	-7.16E-08	1.20E-03	3.58E+00
0.0000E+00	-7.1591E-08	1.2043E-03	3.5826E+00

At flow = 621 cfs computed depth equals 4.30 feet. Flowline of Steamboat Creek at Confluence is 4425.81
therefore water surface in Steamboat Creek at Time = 12.17 equals 4430.1.

HEC-RAS Plan: asblt River: RIVER-1 Reach: Reach-1

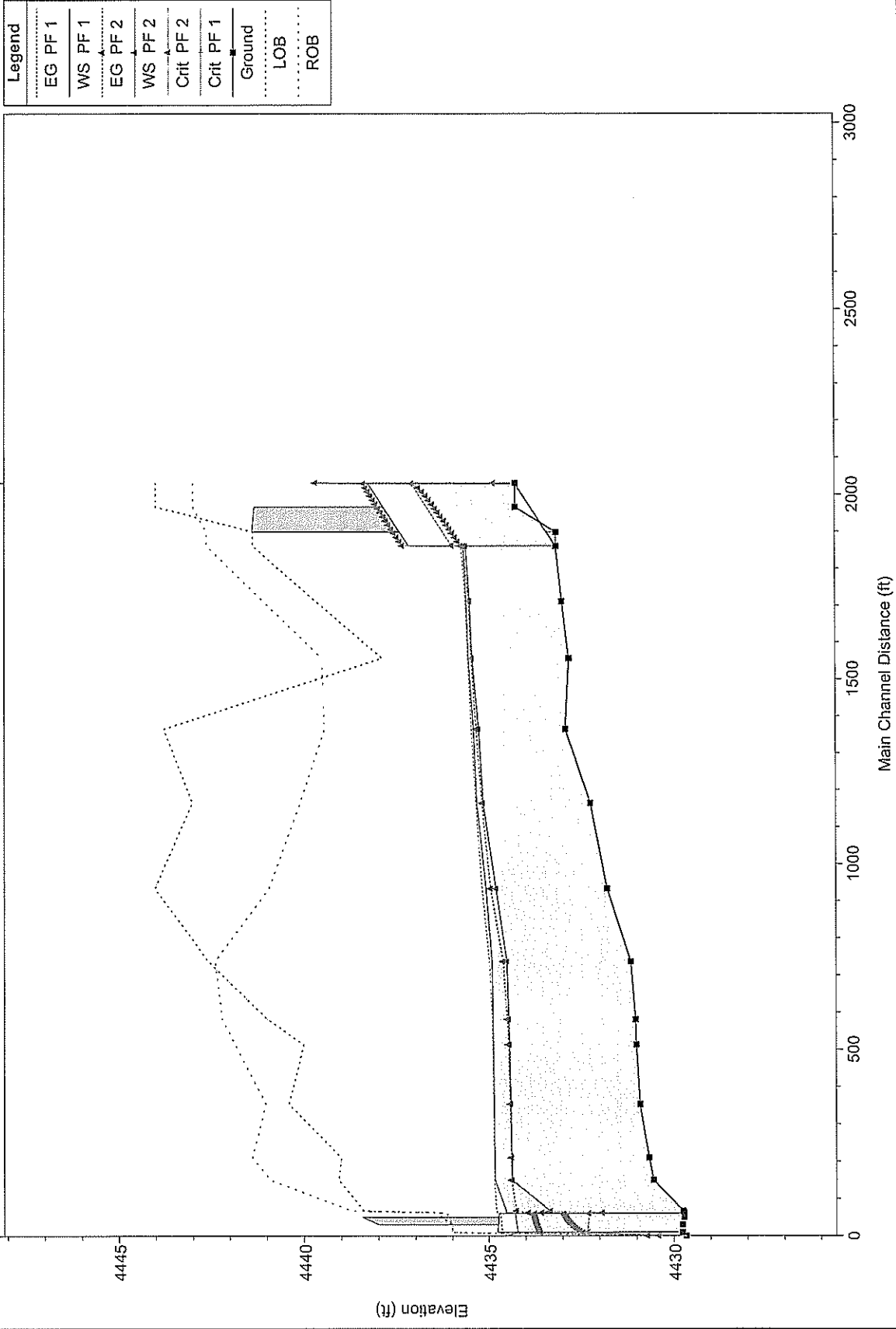
Reach	River Sta	Profile	Q Total (cfs)	Min Chl El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach-1	21.2	PF 1	86.72	4434.25	4439.67	4434.84	4439.67	0.000000	0.06	1366.56	372.73	0.01
Reach-1	21.2	PF 2	86.72	4434.25	4439.67	4434.84	4439.67	0.000000	0.06	1366.56	372.73	0.01
Reach-1	20	Culvert										
Reach-1	19.5	PF 1	86.72	4433.15	4435.67		4435.72	0.001683	1.86	46.51	52.33	0.35
Reach-1	19.5	PF 2	86.72	4433.15	4435.60		4435.66	0.002158	2.02	43.03	51.91	0.39
Reach-1	18	PF 1	99.82	4432.99	4435.58		4435.61	0.000412	1.24	80.22	57.87	0.19
Reach-1	18	PF 2	99.82	4432.99	4435.50		4435.52	0.000506	1.33	75.13	57.32	0.20
Reach-1	16.4	PF 1	99.82	4432.80	4435.53		4435.55	0.000338	1.16	86.25	59.94	0.17
Reach-1	16.4	PF 2	99.82	4432.80	4435.43		4435.45	0.000418	1.24	80.23	58.64	0.19
Reach-1	14.5	PF 1	103.63	4432.90	4435.39		4435.44	0.000888	1.83	56.69	40.76	0.27
Reach-1	14.5	PF 2	103.63	4432.90	4435.25		4435.32	0.001188	2.03	51.15	39.23	0.31
Reach-1	12.5	PF 1	106.99	4432.23	4435.31		4435.33	0.000353	1.31	81.54	48.19	0.18
Reach-1	12.5	PF 2	106.99	4432.23	4435.13		4435.17	0.000475	1.46	73.45	46.44	0.20
Reach-1	10.2	PF 1	131.65	4431.78	4435.06		4435.17	0.001376	2.63	50.07	28.45	0.35
Reach-1	10.2	PF 2	131.65	4431.78	4434.79		4434.94	0.002148	3.10	42.53	26.46	0.43
Reach-1	8.2	PF 1	137.62	4431.15	4434.90		4434.96	0.000742	2.09	65.99	33.47	0.26
Reach-1	8.2	PF 2	137.62	4431.15	4434.49		4434.60	0.001331	2.59	53.12	30.15	0.34
Reach-1	6.7	PF 1	137.62	4431.02	4434.88		4434.90	0.000201	1.20	114.72	50.58	0.14
Reach-1	6.7	PF 2	137.62	4431.02	4434.45		4434.48	0.000351	1.47	93.89	46.70	0.18
Reach-1	6	PF 1	137.62	4431.00	4434.87		4434.88	0.000170	1.06	129.92	61.33	0.13
Reach-1	6	PF 2	137.62	4431.00	4434.43		4434.46	0.000327	1.32	103.97	57.31	0.17
Reach-1	4.4	PF 1	137.62	4430.90	4434.85		4434.86	0.000117	0.85	161.20	79.82	0.11
Reach-1	4.4	PF 2	137.62	4430.90	4434.39		4434.41	0.000232	1.09	126.31	72.38	0.15
Reach-1	3	PF 1	139.55	4430.66	4434.84		4434.85	0.000079	0.79	177.46	74.04	0.09
Reach-1	3	PF 2	139.55	4430.66	4434.37		4434.38	0.000143	0.97	144.11	68.58	0.12

HEC-RAS Plan: asblt River: RIVER-1 Reach: Reach-1

Reach	River Sta	Profile	E.G. US (ft)	W.S. US (ft)	E.G. IC (ft)	E.G. OC (ft)	Min El Weir Flow (ft)	Q Culv Group (cfs)	Q Weir (cfs)	Delta WS (ft)	Culv Vel US (ft/s)	Culv Vel DS (ft/s)
Reach-1	20 Culvert #1	PF-1	4439.67	4439.67	4438.83	4439.67	4441.39	86.72		4.00	9.15	10.10
Reach-1	20 Culvert #1	PF-2	4439.67	4439.67	4438.83	4439.67	4441.39	86.72		4.07	9.15	10.10
Reach-1	1:3 Culvert #1	PF-1	4434.77	4434.53	4433.83	4434.77	4438.45	139.55		0.32	5.10	5.23
Reach-1	1:3 Culvert #1	PF-2	4433.92	4433.56	4433.83	4433.92	4438.45	139.55		1.25	7.17	8.68

East West Channel Plan: As Built November 2007 12/27/2007

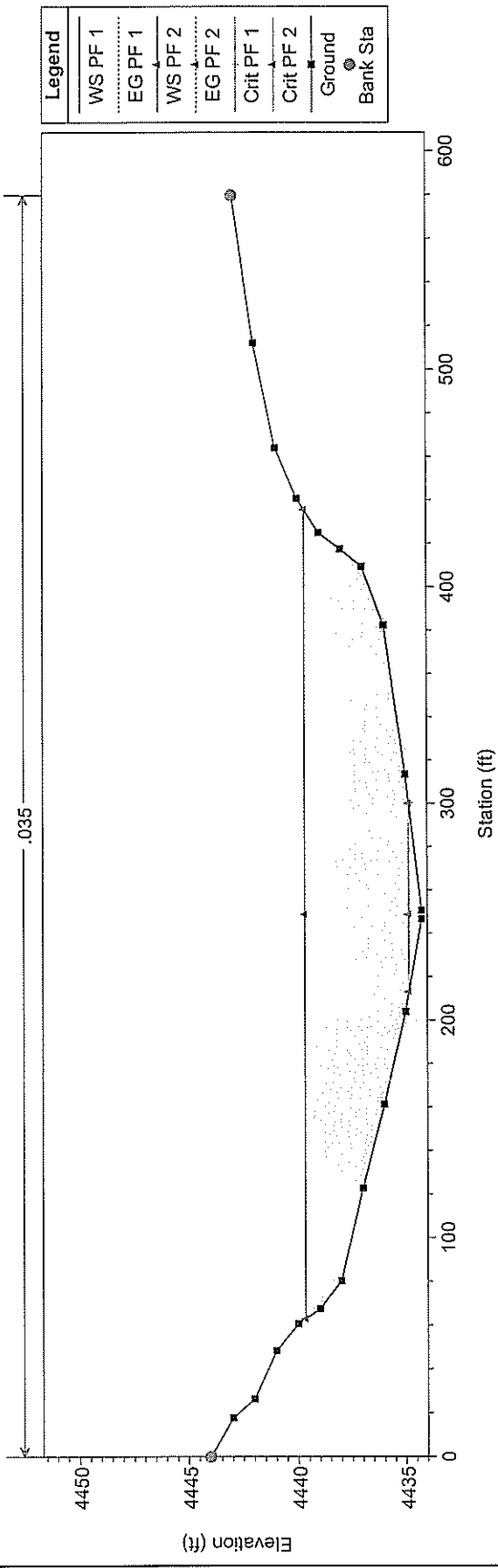
RIVER-1 Reach-1



1 in Horiz. = 400 ft 1 in Vert. = 4 ft

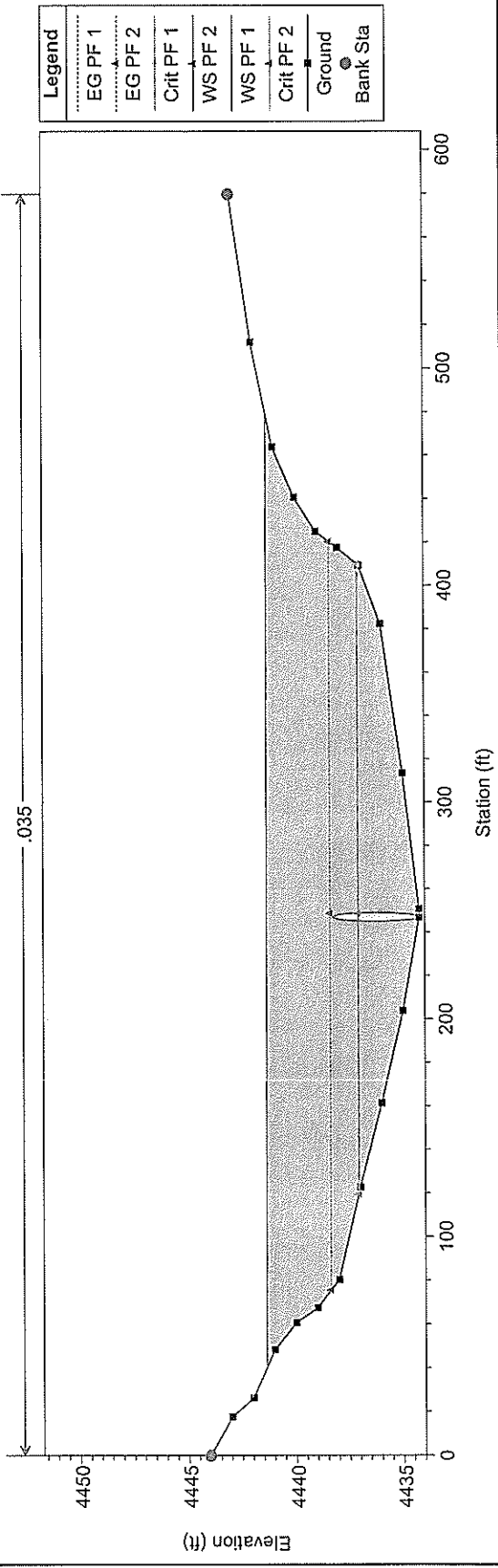
East West Channel Plan: As Built November 2007 12/27/2007

River = RIVER-1 Reach = Reach-1 RS = 21.2



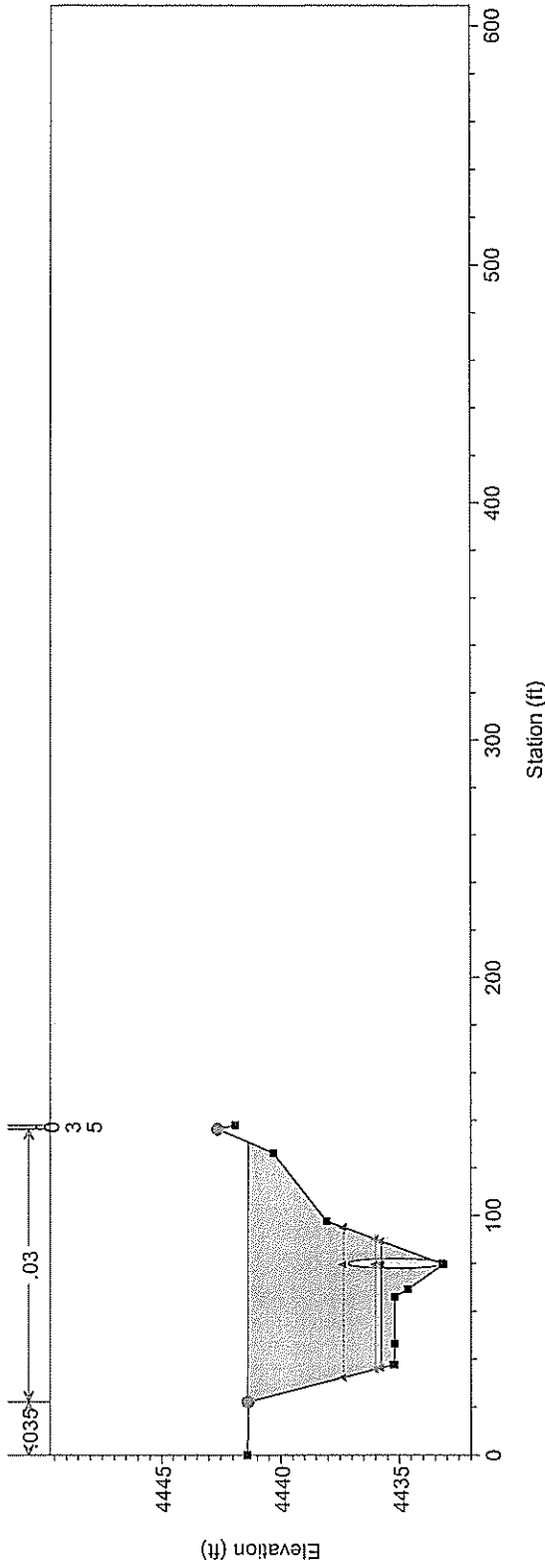
East West Channel Plan: As Built November 2007 12/27/2007

River = RIVER-1 Reach = Reach-1 RS = 20 Culiv

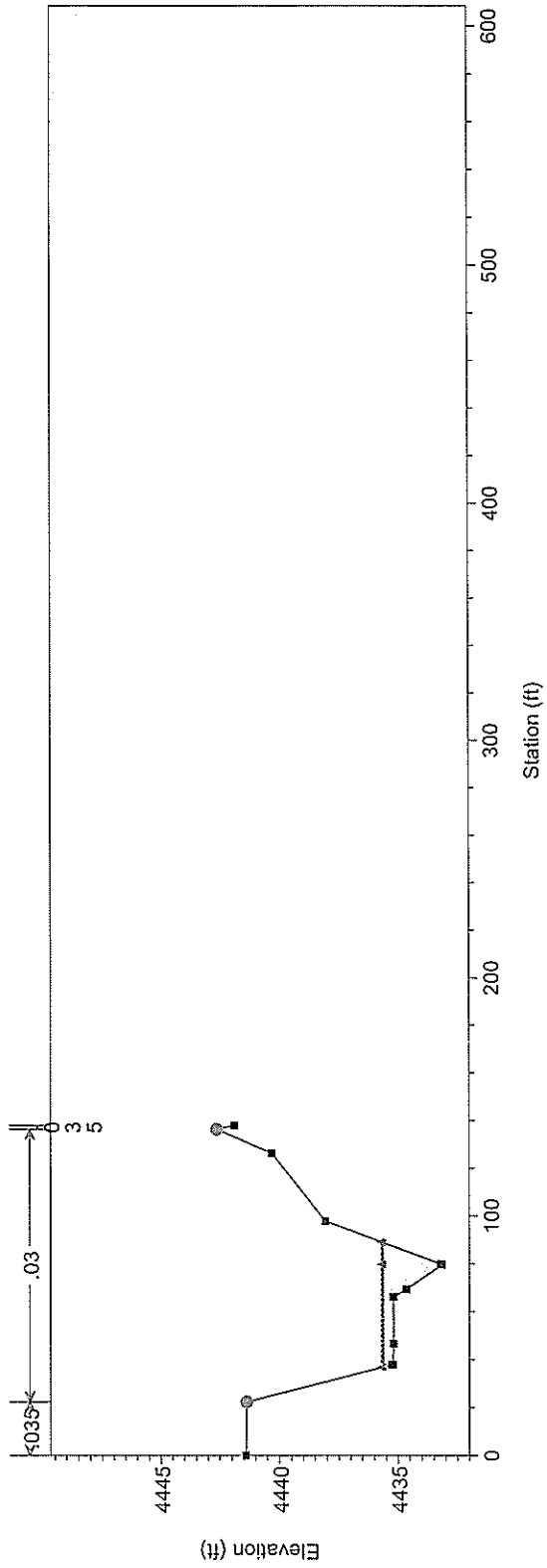


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 20 Culv

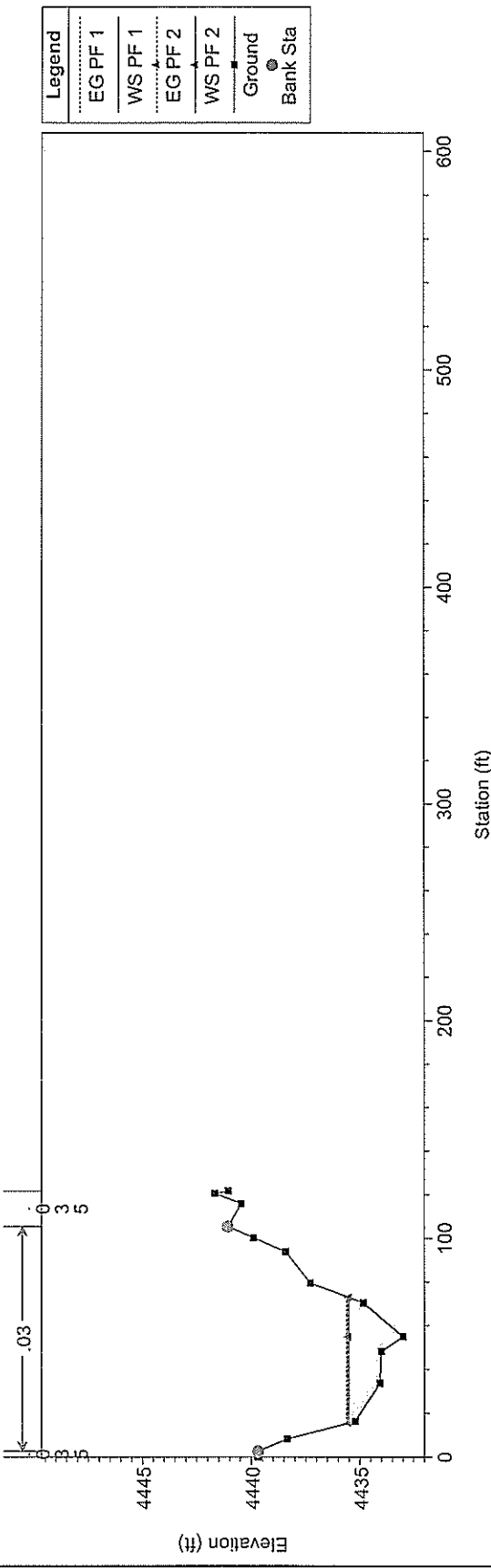


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 19.5

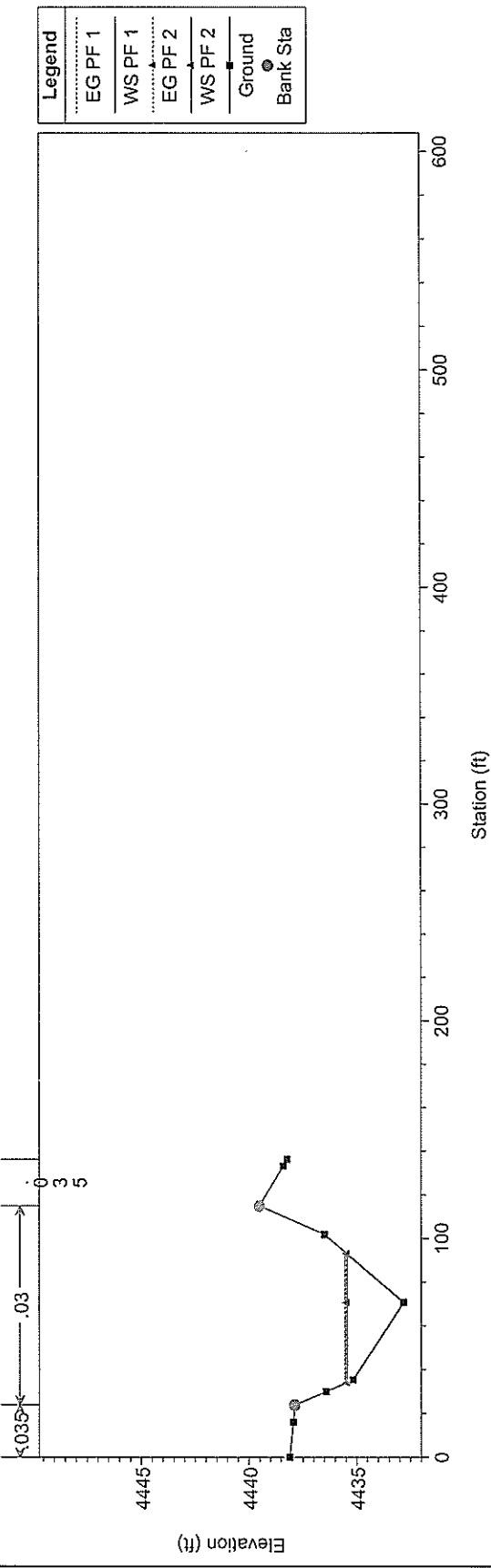


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 18

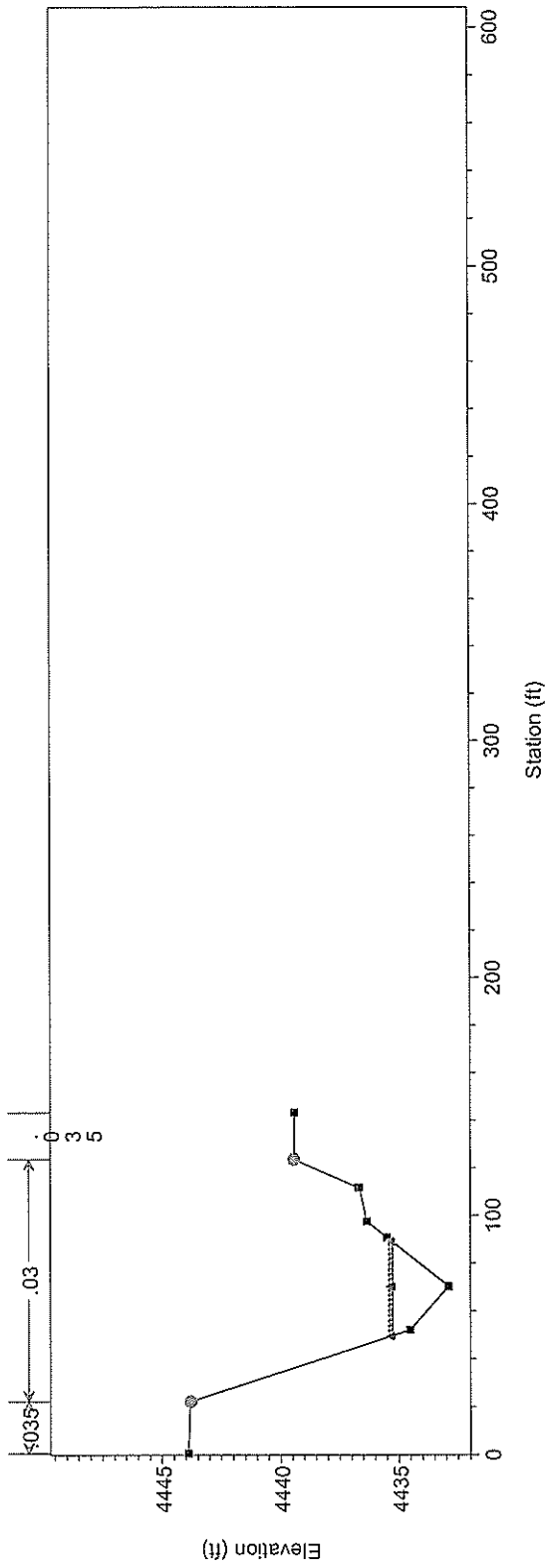


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 16.4

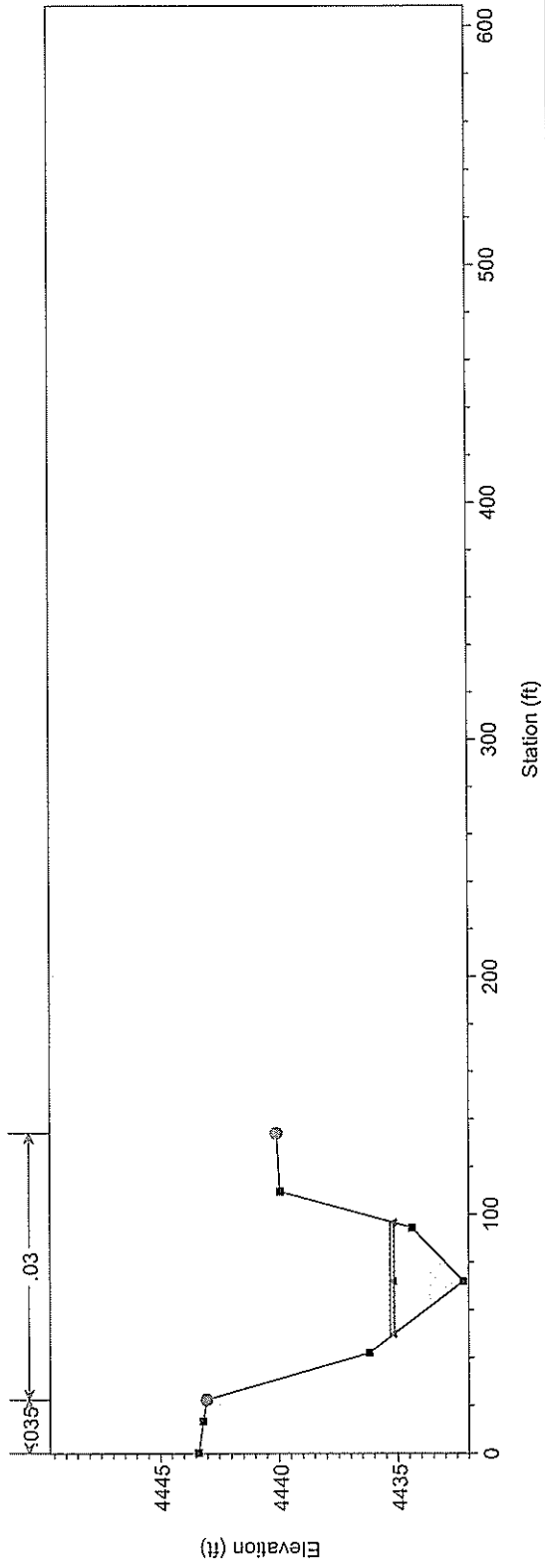


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 14.5

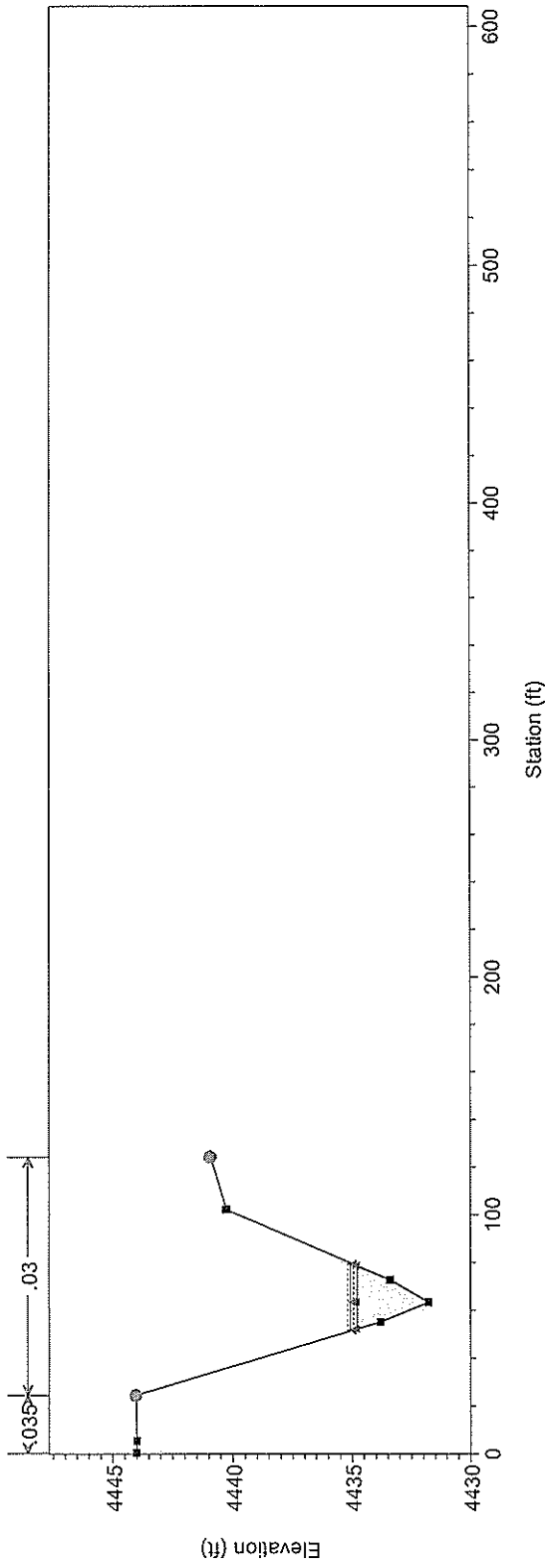


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 12.5

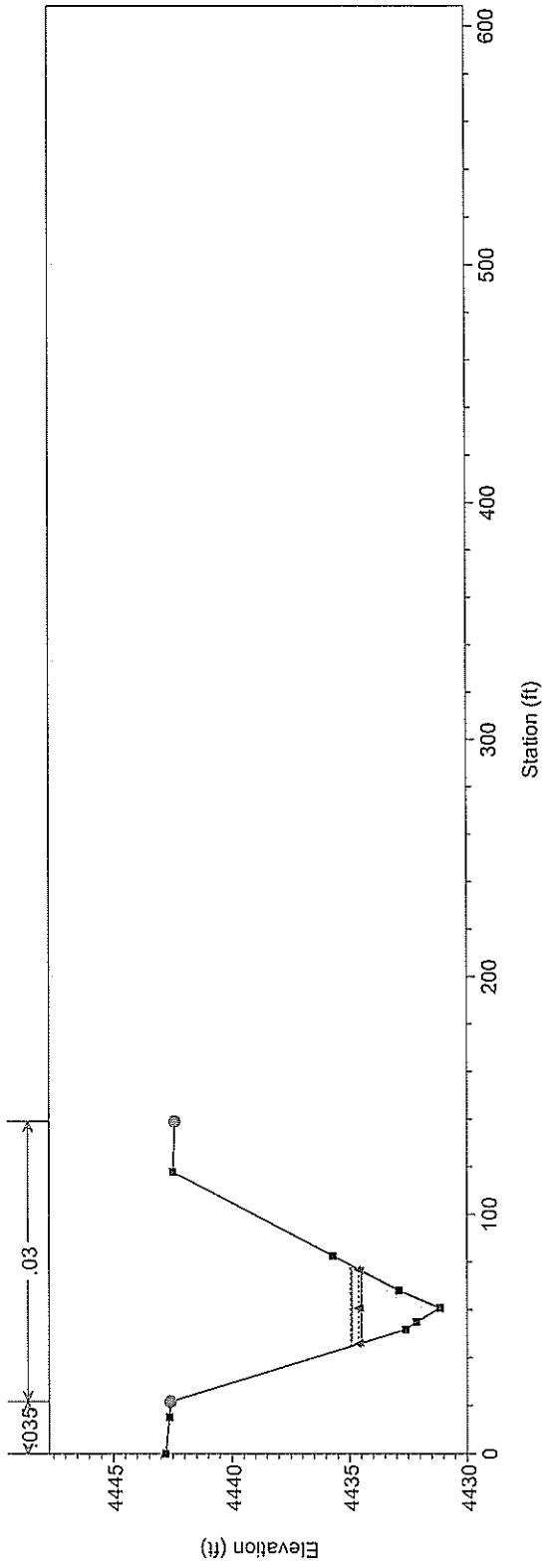


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 10.2

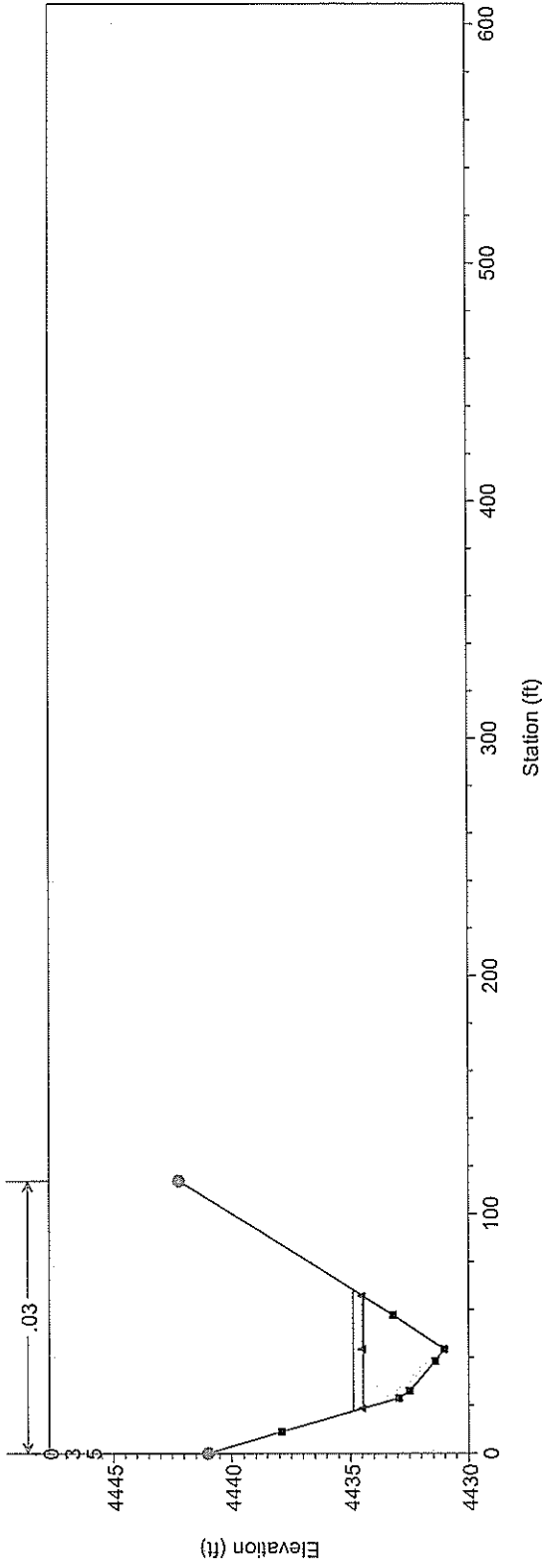


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 8.2

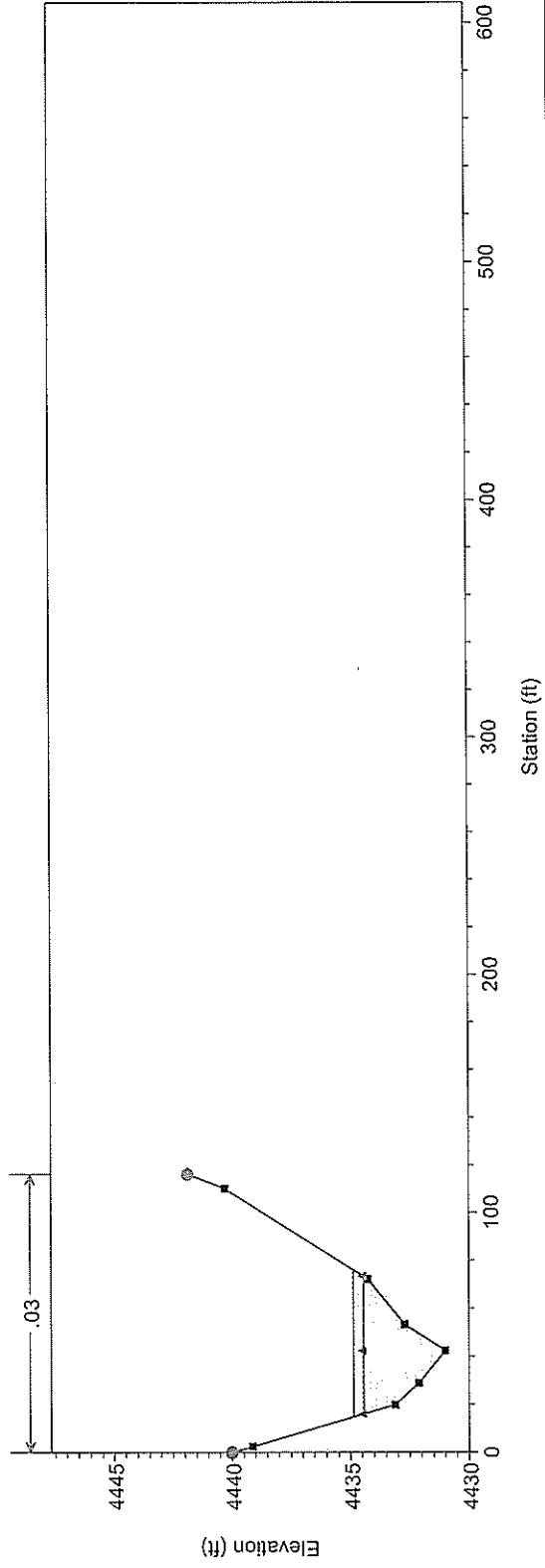


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 6.7



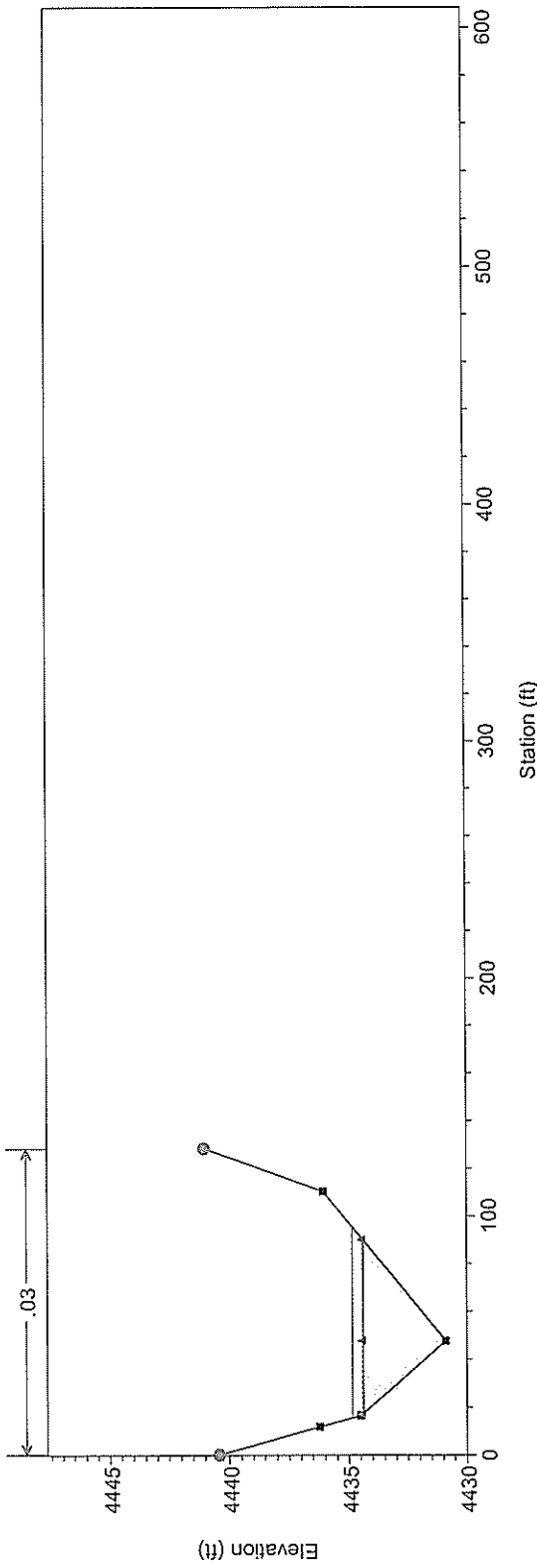
East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 6



1 in Horiz. = 80 ft 1 in Vert. = 8 ft

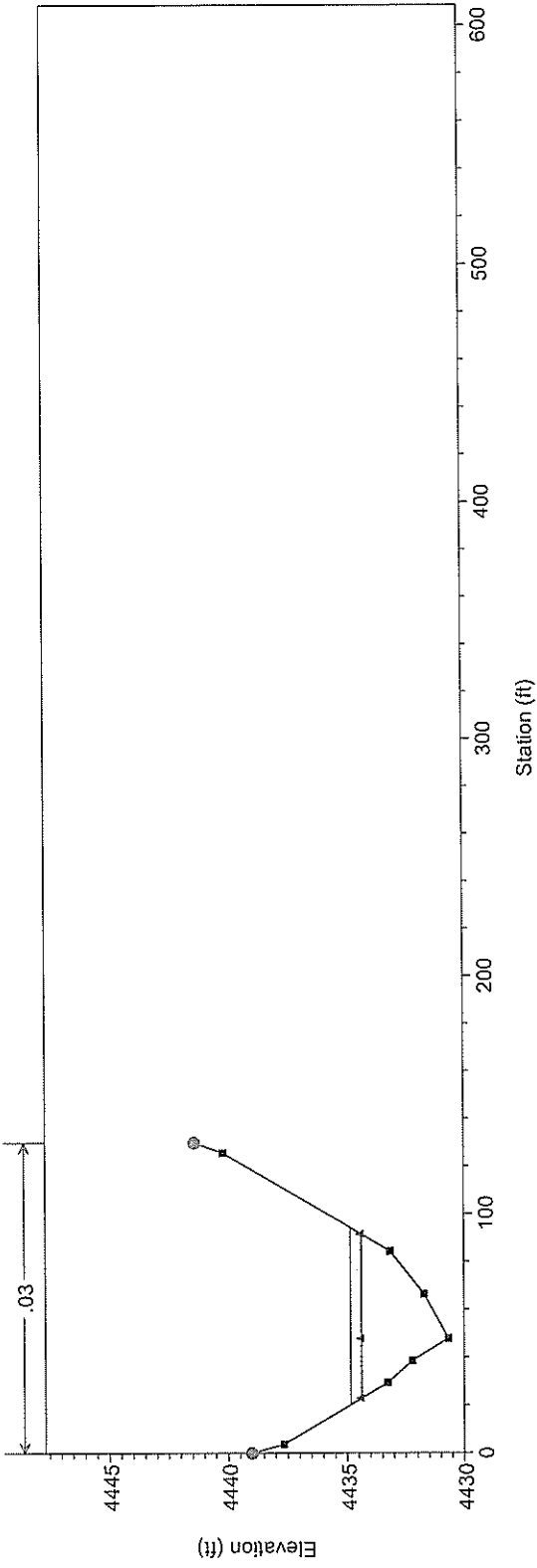
East West Channel Plan: As Built November 2007 12/27/2007

River = RIVER-1 Reach = Reach-1 RS = 4.4



East West Channel Plan: As Built November 2007 12/27/2007

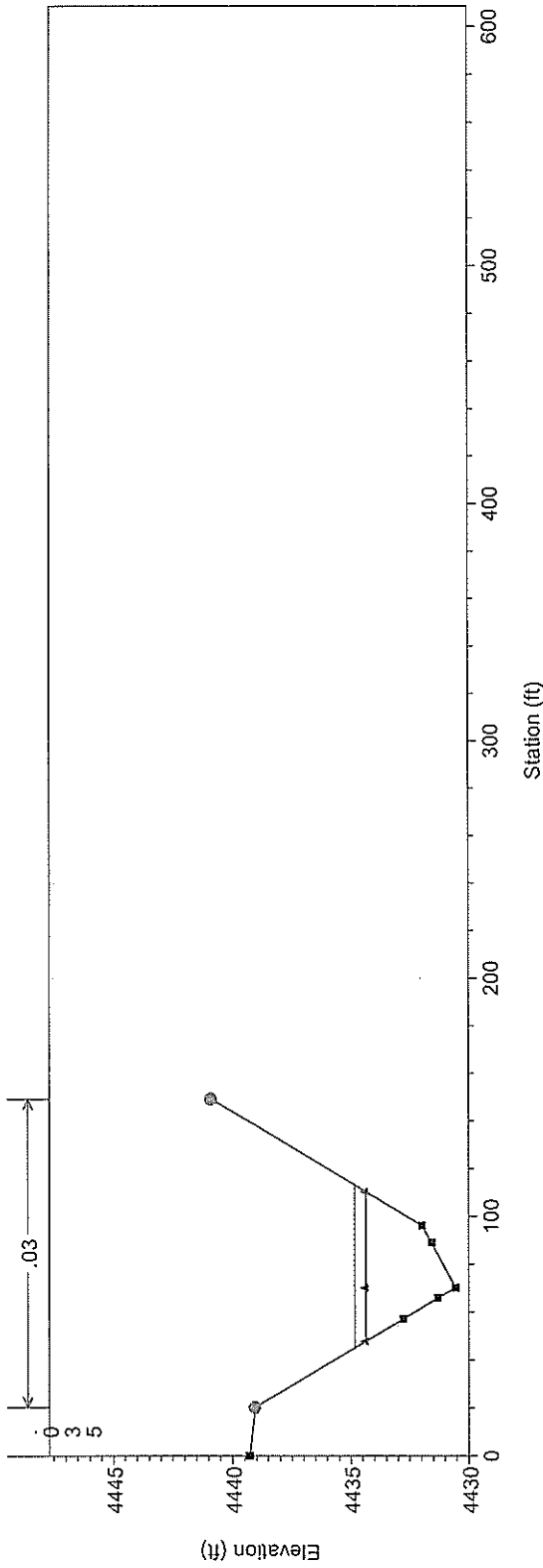
River = RIVER-1 Reach = Reach-1 RS = 3



1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007

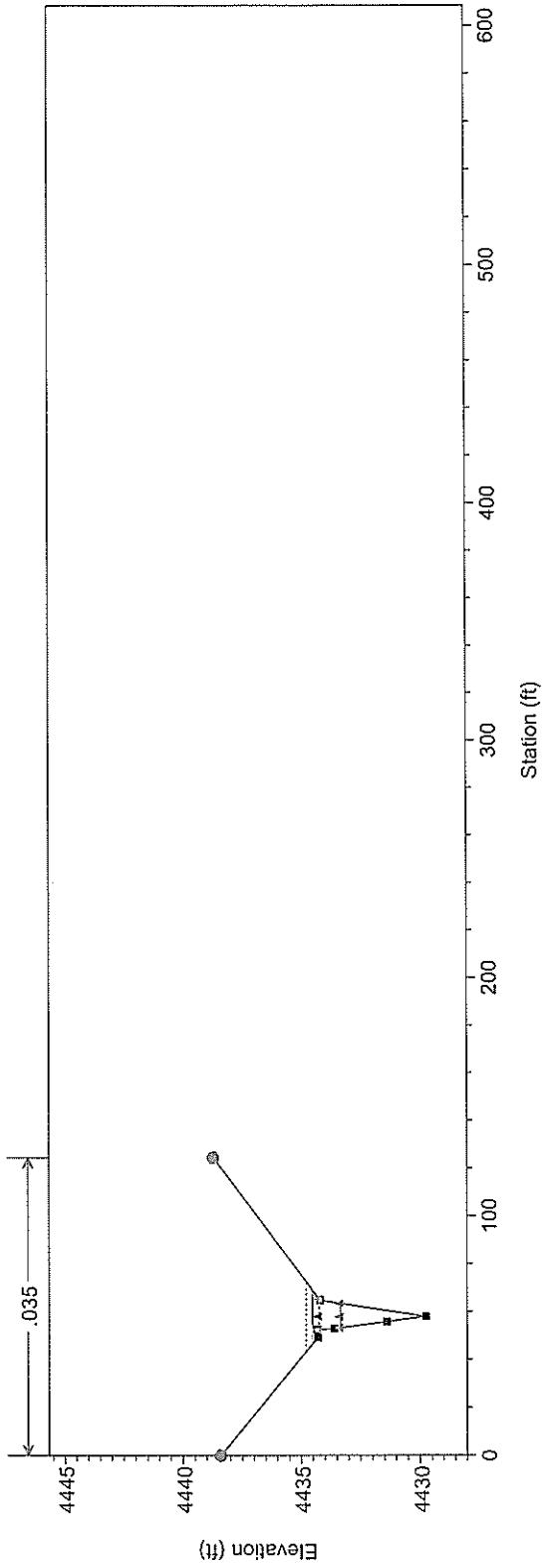
River = RIVER-1 Reach = Reach-1 RS = 2.4



Legend	
.....	EG PF 1
.....	WS PF 1
.....	EG PF 2
.....	WS PF 2
—	Ground
●	Bank Sta

East West Channel Plan: As Built November 2007 12/27/2007

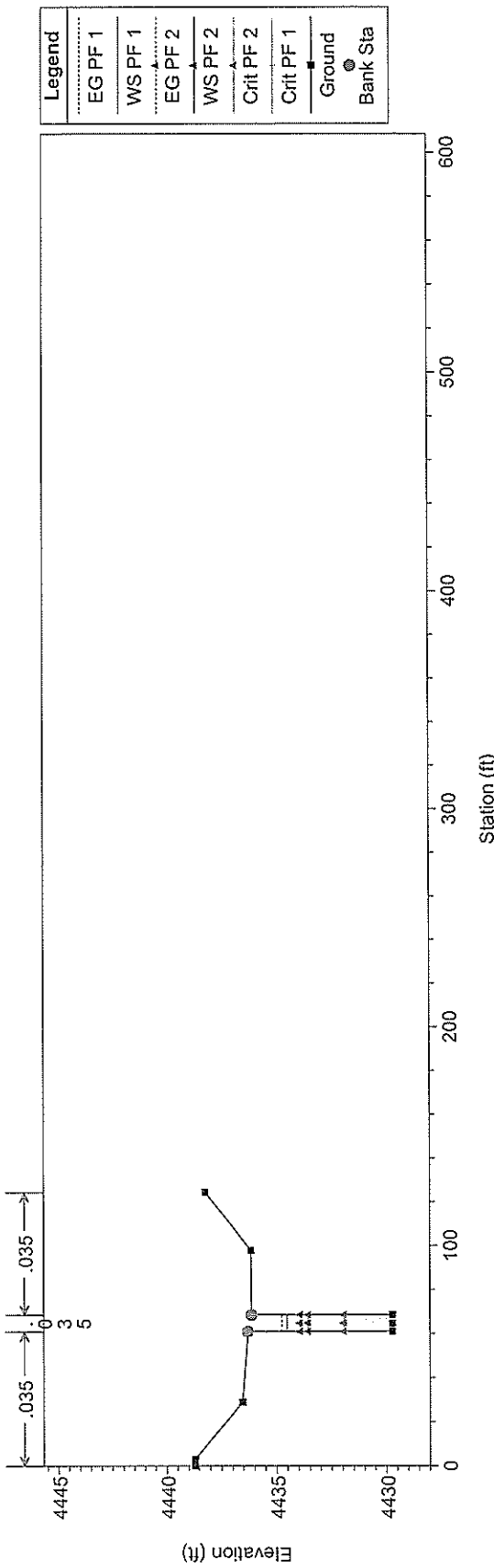
River = RIVER-1 Reach = Reach-1 RS = 1.6



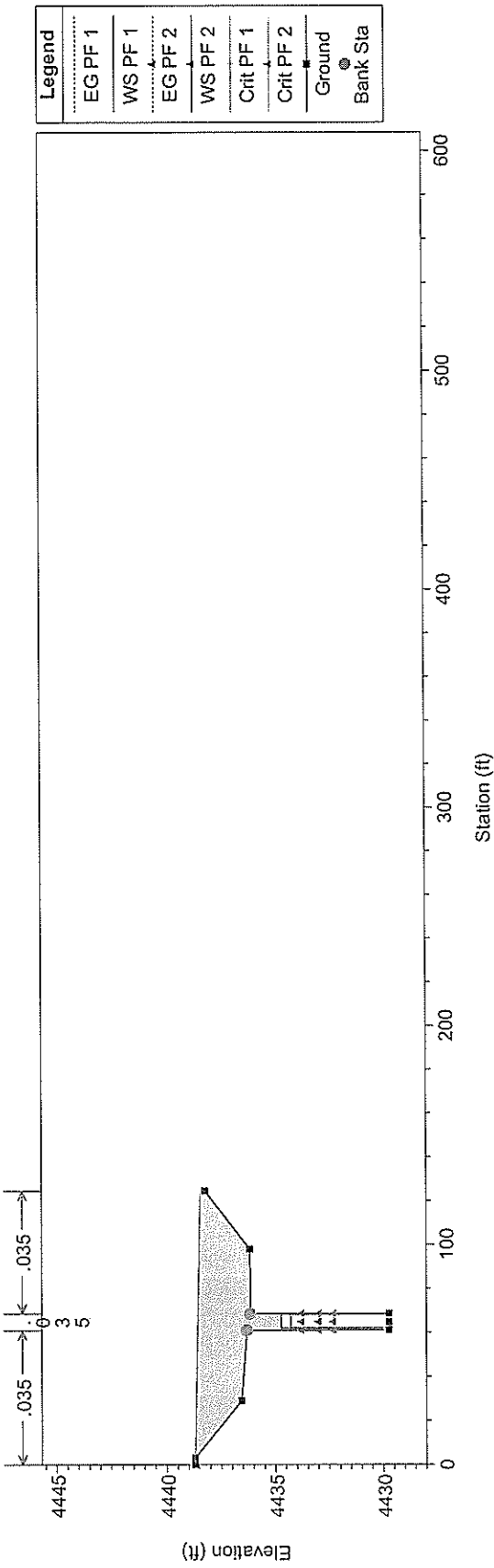
Legend	
.....	EG PF 1
.....	WS PF 1
.....	EG PF 2
.....	WS PF 2
.....	Crit PF 2
—	Ground
●	Bank Sta

1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 1.5

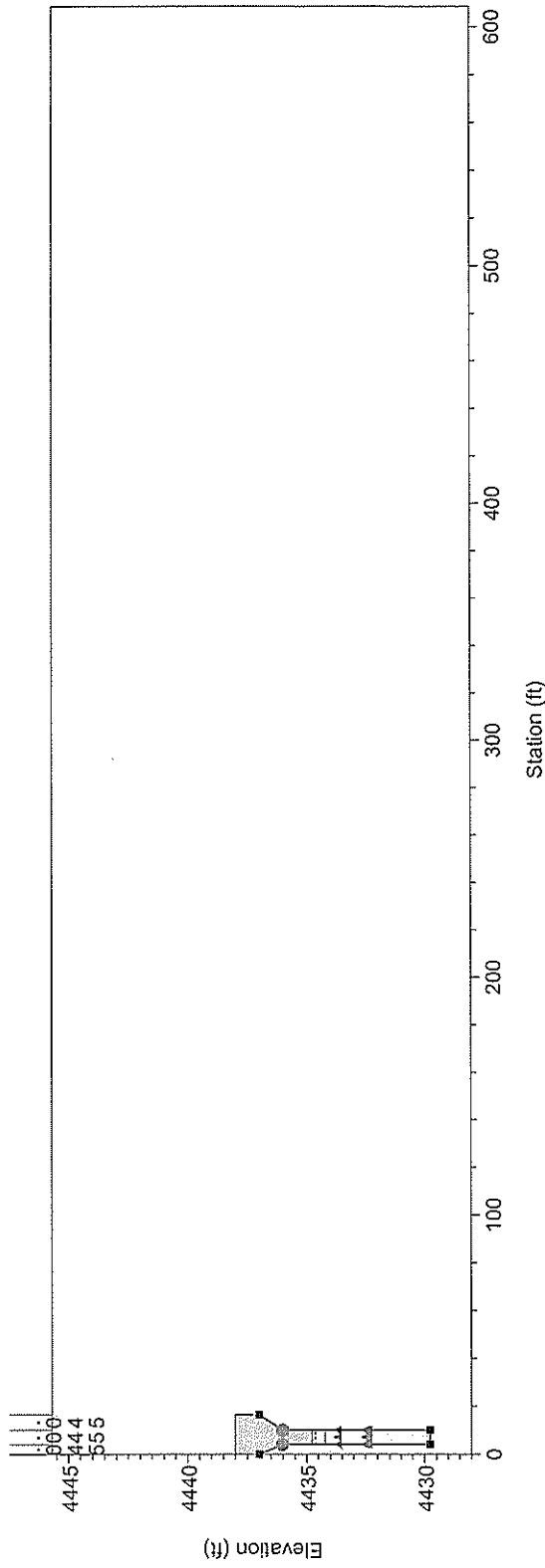


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 1.3 Cuiv

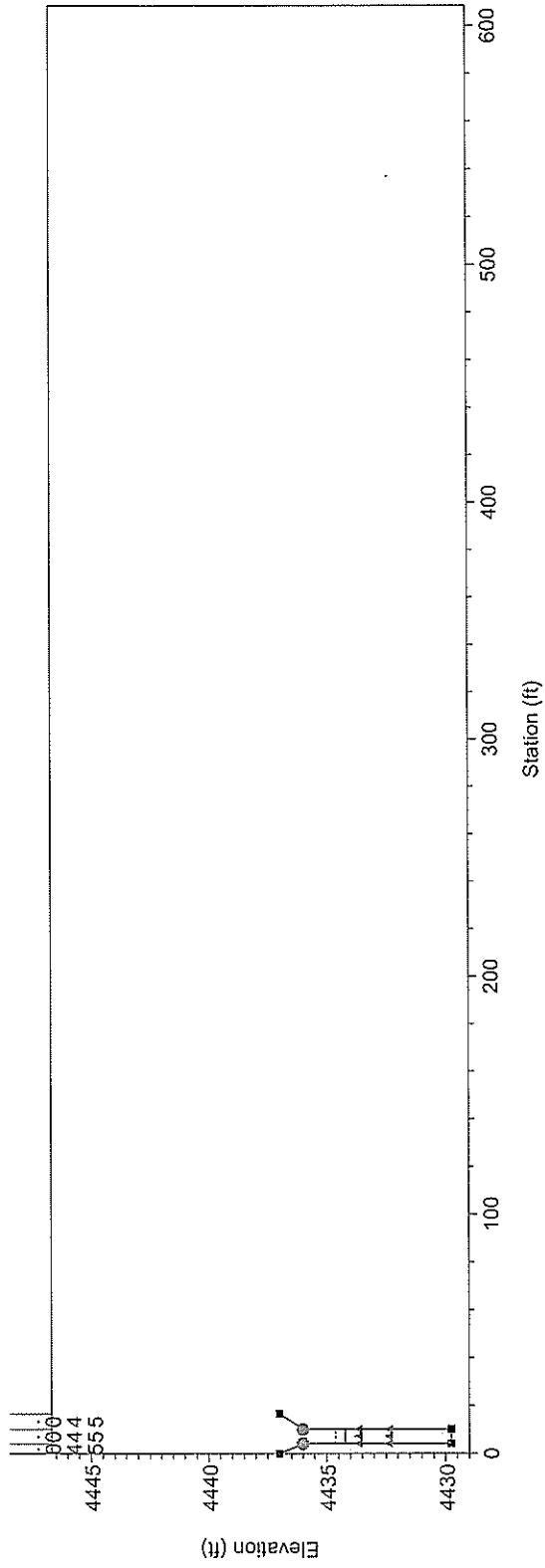


1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 1.3 Culv

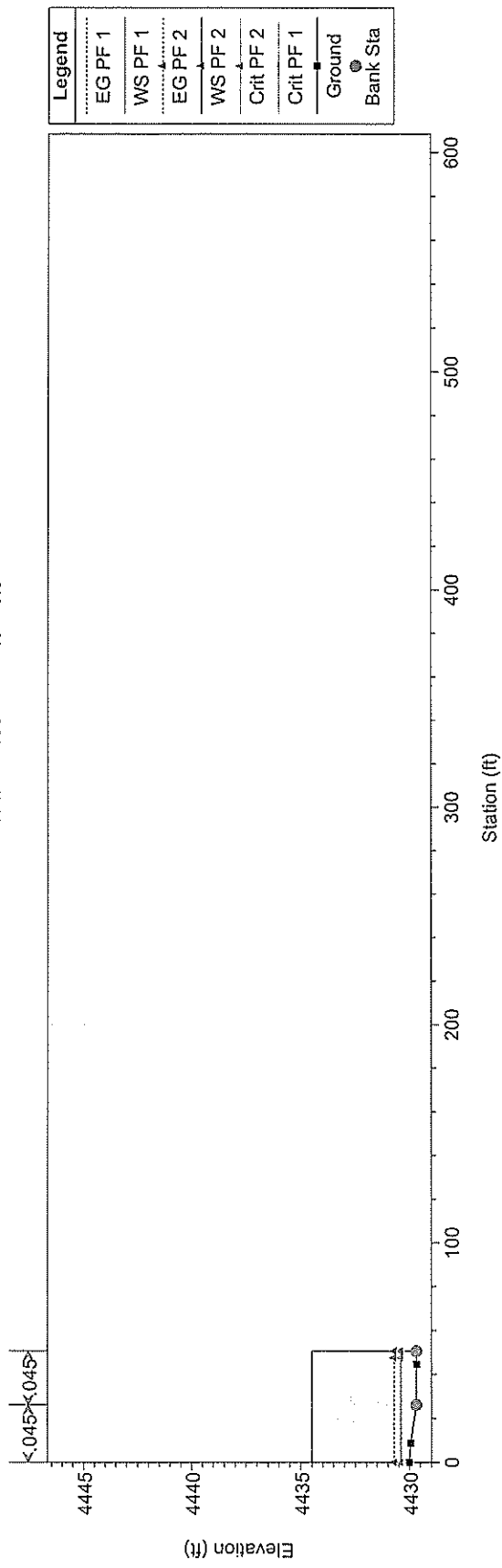


East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 1



1 in Horiz. = 80 ft 1 in Vert. = 8 ft

East West Channel Plan: As Built November 2007 12/27/2007
 River = RIVER-1 Reach = Reach-1 RS = 0.9



1 in Horiz. = 80 ft 1 in Vert. = 8 ft